# TELEMETRY FM/FM BASEBAND STRUCTURE STUDY

VOLUME II
FINAL REPORT FOR:
WHITE SANDS MISSILE RANGE
NEW MEXICO
CONTRACT DA-29-040-AMC-746 (R)

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### SECTION 1

### INTRODUCTION

### 1.1 GENERAL

This volume contains the procedures used and data measured as part of a base-band expansion study sponsored by the IRIG Telemetry Working Group (TWG), funded by White Sands Missile Range (WSMR) and the Electronic Systems Division of the USAF, and undertaken by E'ectro-Mechanical Research, Inc. of Sarasota, Florida, on 17 June 1964 under contract DA-29-040-AMC-746(R). In essence, the program consisted of an evaluation of equipment, a study to determine a feasible baseband expansion, and a program of experimentation to evaluate expansion and provide recommendations for systems application.

Telemetry equipment representative of that typical in field use was gathered and evaluated to determine if there were any characteristics which would prohibit its use in an FM/FM baseband expanded in frequency to 200 kc. Those parameters which were thought to contribute to total system error were also evaluated. Parameters such as receiver IF-envelope delay variation, transmitter dynamic linearity, tape-recorder harmonic distortion, etc., were measured. Where possible similar units from different manufacturers were obtained.

In order to determine the feasibility of the recommended expansions of the FM/-FM basebands, a complete laboratory telemeter was constructed and several basebands were evaluted using specific system tests. The system tests included experimental optimization of the transmitter pre-emphasis, intermodulation, signal-to-noise and system error tests. Determination of the effect of post detection recording, system accuracy, and applicability for pulse modulation were considered as well.

### 1.2 FORMAT DESCRIPTION

The format of this report includes two volumes. Volume I contains the summarizations of the data obtained and interpretations and conclusions based upon this data. This volume, Volume II, as an appendix to Volume I, contains the detailed procedures used and the actual data measured. Both volumes are subdivided into similar sections. A description of the program objectives, the overall approach, and the design of the recommended basebands are contained in Section 1 of Volume I. Section 2 in both volumes discuss the equipment evaluation. The individual systems tests are included in Section 3 of each volume. Volume I alone contains a fourth section where the program conclusions and recommendations appear.

Throughout this report, figures and tables have been sequentially numbered within each section with the volume number, in Roman numerals, as well as the section number appearing each time.

### 1.3 BASEBAND DESIGN AND DESCRIPTION

### 1.3.1 Proportional-Bandwidth Basebands

The design of the expanded proportional-bandwidth baseband is a direct expansion of the present IRIG configuration. The center frequencies of the high frequency channels are approximately 1.3 times the previous upper channel. Thus, channels are located at 93 kc, 124 kc, 165 kc, 220 kc, etc. Like the present IRIG channels, it is desirable to operate all channels at  $\pm 7.5\%$  deviation or by deleting alternate channels when operation at  $\pm 15\%$  deviation is desirable.

Although the spacing of the new proportional-bandwidth channels was straightforward, the number of additional channels that can be added under the constraint of the 500 kc receiver IF bandwidth and the transmitter-radiated-spectrum limitation needed to be determined. Using a technique proposed by H. O. Jeske<sup>(1)</sup>, the higher subcarrier channels can be compared to the present 70-kc channel:

"From a study of the sideband structure of a frequency modulated ? signal it is found that for a given deviation the envelope formed by the sidebands have steeper skirts for the lower modulating frequencies. Since this is the case, only the highest modulation frequency is important unless a pre-emphasis taper is used opposite to the normally used tapers. Also from the theory of FM sideband structure, when multiple modulating frequencies are employed, additional modulation components are produced over the components produced by the superposition of the simple components due to the individual modulation frequencies. additional frequencies are the sums and difference of the simple sidebands removed from the carrier. Fortunately, their amplitudes are equal to the products of the Bessel function amplitudes producing the original simple sidebands and are therefore relatively small. It therefore appears to be safe to assume that for a normal pre-emphasis taper or even no taper the bandwidth occupied by an FM/FM telemetry system is dependent on the modulation level of the highest frequency subcarrier only. "

A sideband study of the higher frequency channels was made using the radiated spectrum limit: The 40 db bandwidth of the modulated carrier, referenced to the unmodulated carrier, shall not exceed  $\pm 320$  kc. Carrier components appearing outside a  $\pm 500$  kc bandwidth shall not exceed -25 dbm.

<sup>(1)</sup> Jeske, H. O., Extension of Proportional Bandwidth FM Subcarrier Channels, Unpublished paper.

The sideband calculation for  $\pm 7.5\%$  and  $\pm 15\%$  subcarrier deviations are shown in Tables II-1.3-1 and II-1.3-2 respectively.

Note that a 0.01% allowance is made for drift and the -25 dbm specification is converted to -75 db relative to a 100-watt unmodulated carrier. Since IRIG document 106-60 limits transmitter power to 100 watts, this is a worst case condition.

The procedure used for the calculation of Tables II-1.3-1 and II-1.3-2 is to first determine the sideband which lies just outside the bandwidth limit. Next, using a table of Bessel functions, choose the maximum modulation index (MI) that does not cause the sideband outside the particular bandwidth to exceed the radiated spectrum level. From the modulation index, the maximum transmitter deviation allotted to that particular channel can be determined. This procedure is repeated at center frequency and at the bandedges to determine the limiting case. The limiting case then determines the maximum allowable transmitter deviation for that channel.

Table II-1. 3-3 shows a comparison of the signal-to-noise performance of the high-frequency channels relative to the 70-kc channel, based upon the maximum allowable transmitter deviation derived in Tables II-1. 3-1 and II-1. 3-2.

To define further the number of channels to be added to the proportional-band-width baseband, the minimum transmitter deviation allotted to each subcarrier was determined. This minimum is based on the criteria that the receiver should threshold at a carrier-to-noise ratio higher than that for the subcarriers to threshold, i.e., the receiver should threshold first. For this condition to be maintained, the subcarrier-to-noise ratio must exceed the receiver IF carrier-to-noise. The minimum transmitter deviation allotted to each subcarrier is thus the deviation sufficient to cause the subcarrier-to-noise ratio to equal the IF carrier-to-noise ratio. Figure II-1.3-4 shows the minimum deviation as a function of the subcarrier center frequency. The straight line which defines the minimum deviation is the classical 3/2-power curve and is based upon the following calculation:

Assumptions:

Triangular noise in passband.

Subcarrier-to-noise ratio equal to IF carrier-to-noise ratio

IF bandwidth = 500 kc

BPIF bandwidth = 15% of center frequency

Carrier-to-noise above threshold.

$$(S/N)_s = (S/N)_c$$
  $\left[\frac{B_c}{2B_s}\right]^{1/2} \frac{f_{dc}}{f_s}$ 

where,

(S/N) = subcarrier-to-noise ratio

(S/N) = IF carrier-to-noise ratio

B = IF bandwidth

B = Subcarrier filter bandwidth

f = Peak carrier deviation allotted to particular subcarrier channel

f = Subcarrier center frequency

But, 
$$(S/N)_s$$
 =  $(S/N)_c$ , therefore
$$f_{dc} = f_s \begin{bmatrix} 2B_s \\ B_c \end{bmatrix}^{1/2}$$

As an example, consider the 40 kc ±15% channel:

$$f_{dc}$$
 = 40,000  $\left[\frac{2(12,000)}{500,000}\right]^{1/2}$   
 $f_{dc}$  = 8.76 kc

In addition to the minimum deviation line in Figure II-1.3-4, the maximum carrier deviation from the sideband study shown in Table II-1.3-2 is also plotted. The area of permissible operation, i.e., peak transmitter deviation allotted to each subcarrier, is thus the region bounded by the two curves in Figure II-1.3-4. The maximum subcarrier center frequency is also found to be 135 kc. The initial expanded proportional-bandwidth baseband considered thus contained channels at 93 kc and 124 kc; however, during the system test it was found that the 165 kc channel could be added while still maintaining the subcarrier threshold above the receiver threshold. This is discussed in more detail in Volume I. Table II-1.3-5 shows the channel allocations for the basebands evaluated using the laboratory telemeter.

### 1.3.2 Constant-Bandwidth Baseband

A similar calculation of maximum and minimum transmitter deviation allotted to each subcarrier channel as described for the proportional-bandwidth baseband was also made for the constant-bandwidth baseband. The sideband study calculations are shown in Table II-1.3-6 for binary channels spaced 8 kc apart

and with  $\pm 2$  kc. Calculations are also shown for each channel with  $\pm 4$  kc deviation; however, only alternate channels can be used with  $\pm 4$  kc deviation.

The minimum transmitter deviation to maintain the subcarrier-to-noise equal to the IF carrier-to-noise ratio was calculated for ±2 kc deviation in an identical manner as for the proportional-bandwidth baseband and is shown in Figure II-1.3-7. The maximum deviation based on the sideband study shown in Table II-1.3-6 is also plotted in Figure II-1.3-7. The area of permissible operation is then again the region bounded by the two curves. The maximum center frequency is approximately 180 kc. Thus, the constant-bandwidth-baseband configuration which most nearly meets the objectives of the baseband expansion outlined in Volume I and which was chosen for evaluation is the 21-channel system (Figure I-1.5-2) with the highest frequency channel at 176 kc. The channel allocations and implementation for this baseband are shown in Table II-1.3-8.

### 1.3.3 Combinational-Bandwidth Baseband

To meet the objective of a baseband providing both constant- and proportional-bandwidth channels, the combinational-bandwidth baseband was designed and evaluated. This baseband consists of taking the 21-channel constant-bandwidth baseband and filling the space between dc and the first constant-bandwidth channel at 16 kc with IRIG proportional-bandwidth channels.

With the  $\pm 2$  kc constant-bandwidth channels spaced 8 kc apart, the guard-band limit associated wit' each channel is 2 kc or  $\pm 4$  kc from band center. For the 16 kc channel, this buard band extends to 12 kc. The center of the guard band between IRIG channel 12 (10.5 kc  $\pm 7.5\%$ ) and channel 13 (14.5 kc  $\pm 7.5\%$ ) is 12.3 kc which is above the 12 kc guard band edge for the first constant-bandwidth-baseband channel.

Thus, the highest IRIG channel used in the combinational-bandwidth baseband is channel 11 (7.35 kc  $\pm$ 7.5%). The combinational-bandwidth baseband thus consists of IRIG channels 1 through 11, Table II-1.3-5, and constant-bandwidth channels 1 through 21, Table II-1.3-8.

### 1.4 DEFINITION OF SYMBOLS AND TERMS

The abbreviations and symbols below are used throughout the text.

BPIF Band-pass input filter of subcarrier discriminator

CBW Constant bandwidth

Crosstalk Interference in a given channel which has its origin in another channel, e.g., adjacent channels in a frequency

division multiplex system.

db Voltage or power levels referenced to unity in decibels

dbm Power level in db referenced to 1 milliwatt or voltage level in db referenced to the voltage into 600 ohms which

dissipates l milliwatt

DR Deviation ratio; in a frequency modulation system, the ratio of the maximum frequency deviation to the maximum

modulating frequency of the system.

Full bandwidth FRW

3-db cutoff frequency f

 $f_{\mathbf{m}}$ Maximum modulation frequency for a particular deviation

ratio

Intermediate frequency amplifier of receiver IF

The modulation of the components of a complex wave by Intermodulation each other, producing waves having frequencies equal to the sums and differences of integral multiples of the com-

ponent frequencies of the complex wave.

LPOF Low-pass output filter of subcarrier discriminator

Modulation index; for a sinusoidal modulating wave, the ratio MI

of the frequency deviation to the frequency of the modulating

wave.

PBW Proportional bandwidth

Transmitter deviation sensitivity (kc peak/voltage peak) rms transmitter

-6-

times rms voltage input. deviation

(S/N) <sub>c</sub>	Carrier-to-noise ratio
(S/N) <sub>d</sub>	Signal-to-noise ratio
(S/N) <sub>s</sub>	Subcarrier-to-noise ratio

\$ 5

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I

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Table II-1. 3-1

# ±7.5% HIGHER FREQUENCY PROPORTIONAL BANDWIDTH SUBCARIERS SIDEBAND CALCULATIONS FOR ADDITION OF

Conditions: Pt = 100 watts
Drift Allowances - 0.01%

Specification: -40db at ±320 KC -25dbm at ±500 KC

Channel Position (%)	Frequency (kc)	Sideband Outside ±294 kc	Actual Modulation Index	Sideband Amplitude (Limit 0.010)	Maximum Transmitter Deviation (* kc)	Sideband Outside	Sideband Amplitude (Limit 0.000178)
-7.5 0 +7.5	64. 75 70. 00 75. 25	សេសស	2. 16 2. 00 1. 86	*0.0100 0.0070 0.0050	140 140	80 ~ ~	0.00004 *0.000175 0.00011
-7.5 0 +7.5	86.02 93.00 99.98	ৰা হা ল	0.92 0.85 0.79	0.0018 0.0013 *0.00987	79 79 79	oo in	0. 000013 0. 000008 0. 00008
-7.5 0 17.5	114.7 124.0 133.3	#: # m m m	0.54 0.50 0.46	0.0032 0.0025 0.0020	62 62 62	ਮਨ ਵਾ ਵਾ	0.000012 *0.00016 0.00011
-7.5 0 +7.5	152. 6 165. 0 177. 38	~ ~ ~	0. 22 0. 20 0. 19	0.006 0.005 0.004	3333	<b>4</b> m m	0.000006 *0.00016 0.00014
-7.5 0 +7.5	203. 5 220. 0 236. 5	222	0. 20 0. 19 0. 17	0.005 0.004 0.0036	4 4 4	ммм	*0.00016 0.00014 0.00010

SIDEBAND CALCULATIONS FOR ADDITION OF ±15% HIGHER FREQUENCY PROPORTIONAL BANDWIDTH SUBCARRIERS

Conditions: P = 100 watt

Specification: -40 db at ±320 kc -25 dbm at ±500 kc

2
0
Ö
11
lowance
7
Drift

Channel Position	Frequency (kc)	Sideband Outside ±294 kc	Actual Modulation Index	Sideband Amplitude (Limit 0.010)	Maximum X-mtr. Deviation (* kc)	Sideband Outside ±474 kc	Sideband Amplitude (Limit 0.000178)
-15	59.50	5	1.93	0.0059	115	<b>&amp;</b>	0.000017
-7.5	64.75	<b>ا</b> کا	1.78	0.0041	511	co t	0.0000089
¥ 7 0	70.00	เก เก	1.65	0.0028	115	~ ~	0.000029
+15	80.50	*	1.43	0.0098	115	9	*0.000172
<u>د</u> د	79.05	*	1.00	0.0025	79		0.0000015
-7.5	86.02	*	0.92	0.0018	62	9	0.000013
0	93.00	*	0.85	0.0013	79	9	0.000008
+7.5	96.66	6	0.79	*0.00987	79	'n	0.00008
+15	106.95	€ .	0.74	0.0081	62	ហ	0.00006
<b>.</b>	105.4	<b>C</b>	0.59	0.0042	29	<b>1</b> 50	0.000018
-7.5	114.7	8	0.54	0.0032	29	ĸ	0.000012
0	124.0	3	0.50	0.0025	29	4	*0.00016
+7.5	133.3		0.46	0.0020	29	4	0.00011
+15	142.6	m	0.43	0.0016	29	4	0.00008
-15	140.2	8	0.24	0.00028	33	4.	0.000008
-7.5	152.6	7	0.22	900.0	33	4	900000.0
0	165.0	2	0.20	0.005	33	~	*0.00016
+7.5	177.38	2	0.19	0.004	33	٣	0.00014
+15	189.75	2	0.17	0.0036	33	<b>m</b>	0.00010
				· .			

# SIDEBAND CALCULATIONS FOR ADDITION OF ±15% HIGHER FREQUENCY PROPORTIONAL BANDWIDTH SUBCARRIERS

Conditions: P<sub>t</sub> = 100 watt

Specification: -40 db at ±320 kc

Drift Allowance.= 0.01%

-25 dbm at ±500 kc

Sideband Amplitude (Limit 0.000178)	0.000001 0.0000009 0.0000008 0.0000006 *0.00011	
Sideband Outside ±474 kc		ı
Maximum X-mtr. Deviation (± kc)	7.6 7.6 7.6 7.6	
Sideband Amplitude (Limit 0.010)	0.0002 0.00018 0.00016 0.00012 0.00011	
Actual Modulation Index	0.041 0.037 0.035 0.031 0.030	
Sideband Outside ±294 kc	~ ~ ~ ~ ~	
Frequency (kc)	187.0 203.5 220.0 236.5 253.0	
Channel Position (%)	-15 -7.5 0 +7.5 +15	

\* Indicates Limiting Case

SUMMARY OF SIGNAL-TO-NOISE PERFORMANCE OF HIGHER FREQUENCY PROPORTIONAL BANDWIDTH CHANNELS RELATIVE TO THE 70 KC IRIG CHANNEL TABLE II-1.3-3

 $P_t = 100 \text{ watt}$ 

Subcarrier (kc)	Channel Deviation (%)	Modulation	X-mtr. Deviation (± kc)	Relative X-mtr. Deviation	Relative Deviation (db)	Noise 3/2 Taper (db)	Overall Performance (db)
70	15	1.65	115	1.00	0	0	0
93	15	0.85	46	0.686	-3.27	-3.8	-7.1
124	15	0.50	29	0.538	-5.38	-7.4	-12.8
165	15	0.20	33	0.287	-10.9	-11.2	-22.1
220	15	0.035	7.6	990.0	-23.6	-14.9	-38.5
70	7.5	2.00	140	1.00	0	0	0
93	7.5	0.65	79	0.564	-5.0	-3.8	-8.8
124	7.5	05.0	29	0.443	-7.1	-7.4	-14.5
165	7.5	0.20	33	0.236	-12.6	-11.2	-23.8
220	7.5	0.19	4	0.292	-10.8	-14.9	-25.7

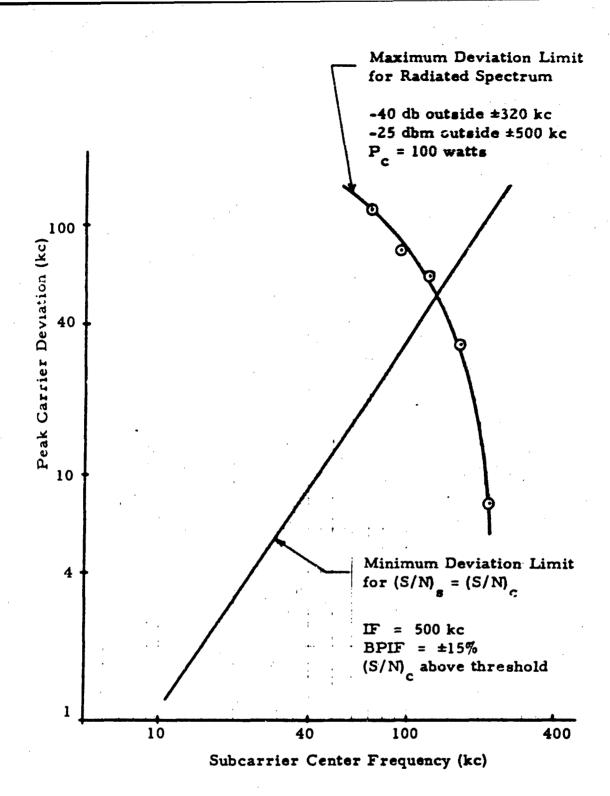


FIGURE II-1.3-4
FM/FM CARRIER DEVIATION LIMIT FOR WIDEBAND
PROPORTIONAL BANDWIDTH CHANNELS

# CHANNEL ALLOCATIONS FOR PROPORTIONAL BANDWIDTH BASEBANDS

Center Frequency (kc)		RIG seband	Ba W	IRIG seband vith ideband Channel	Prop Ba	panded portional ndwidth isoband	Prop Ba Ba V W	cpanded cortional ndwidth seband vith ideband hannel
0.40	l	±7.5%	!	±7.5%	l	±7.5%	1	±7.5%
0.56	2	±7.5%	2	±7.5%	2	±7.5%	2	±7.5%
0.73	3	±7.5%	3	±7.5%	3	±7.5%	3	±7.5%
0.96	4	±7.5%	4	±7.5%	- 4	±7.5%	4	±7.5%
1.30	5	±7.5%	5	±7.5%	5	±7.5%	5	±7.5%
1.70	6	± 7.5%	6	±7.5%	6	±7.5%	6	±7.5%
2.30	7	±7.5%	7	±7.5%	7	±7.5%	7	±7.5%
3.00	8	±7.5%	8	±7.5%	8	±7.5%	8	±7.5%
3.90	9	±7.5%	9	±7.5%	9	±7.5%	9	± 7.5%
5.40	10	±7.5%	10	±7.5%	10	±7.5%	10	±7.5%
7.35	11	±7.5%	11	±7.5%	11	±7.5%	11	±7.5%
10.5	12	±7.5%	12	±7.5%	12	±7.5%	12	±7.5%
14.5	1 3	±7.5%	13	±7.5%	13	±7.5%	13	±7.5%
22.0	1'4	±7.5%	14	±7.5%	14	±7.5%	i 4	±7.5%
30.0	15	±7.5%	15	±7.5%	15	±7.5%	15	±7.5%
40.0	16	±7.5%	16	±7.5%	16	±7.5%	16	±7.5%
52.5	17	±7.5%			17	±7.5%	i 7	±7.5%
70.0	18	±7.5%	E	±15%	18	±7.5%	18	±7.5%
93.0					19	±7.5%	19	±7.5%
124.0					20	±7.5%	_	
165.0					21	±7.5%	H	±15%

SIDEBAND CALCULATIONS FOR CONSTANT BANDWIDTH CHANNELS

Conditions: P = 100 watts

Specifications: -40 db at #320 kc

Drift Allowance = 0.01%

-25 dbm at ±500 kc

Subcarrier (kc)	Channel Position (kc)	Sideband Outside ±294 kc	Actual M.I.	Sideband Amplitude (Limit 0.010)	Maximum X-mtr. Deviation (±kc)	Sideband Outside ±474 kc	Sideband Amplitude (Limit 0.000178)
94 96 98	2- 0 +5	च च च	0.92	0.0017	88.4 88.4 88.4	<b>ዕ</b> የአ	*0,000166
95 96 100	404	44 44 W	0.82	*0.0098	79.0 79.0 79.0	ວທະດ	0.00009
102 104 106	2- 0 7-	m m.m	0.79	*6.0098	80.5 80.5 80.5	տտտ	0.000078
100	404	m m m	0.79	*0.0098	79.0 79.0 79.0	மமை	0.000078
110	-5 0 +2	<b></b>	0.79	*0.0098	86.8 86.8 86.8	முல்	0.000078
108 112 116	404	m m m	0.79	*0.0098	85.3 85.3 85.3	ທີ່ດາ	0.000078

T.#

# SIDEBAND CALCULATIONS FOR CONSTANT BANDWIDTH CHANNELS TABLE II-1.3-6 (CONT'D.)

Conditions: Pt = 100 watts

Specifications: -40 db at ±320 kc

Drift Allowance = 0.01%

-25 dbm at ±500 kc

Subcarrier (kc)	Channel Position (kc)	Sideband Outside ±294 kc	Actual M.I.	Sideband Amplitude (Limit 0.010)	Maximum X-mtr. Deviation (±kc)	Sideband Outside	Sideband Amplitude (Limit 0.000178)
118 120 122	2- 0 +2		0.52 0.51	0.0029	61.1 61.1 61.1	<b>ጥ</b> 4 4	*0.000174
116 120 124	404	m m m	0.53	0.0029	61.1 61.1 61.1	rv 44	*0.000174
126 128 130	-2 0 +2	m m m	0.51 0.50	0.0027	64.2 64.2 64.2	4 4 4	*0.000174
124 128 132	404	m m m	0.50	0.0027	63.3 63.3 63.3	िय य य	*0.000174
134 136 138	7-0 7	m m m	0.51	0.0027	68.3 68.3 68.3	4 4 4	*0.000174
132 136 140	4- 0 4+	<b></b>	0.51	0.0027	67.3 67.3 67.3	क क क	*0.000174

\*Indicates Limiting Case

Specifications: -40 db at ±320 kc

-25 dbm at ±500 kc

Conditions:  $P_t = 100$  watts Specification Drift Allowance = 0.01%

Sideband Amplitude (Limit 0.000178)	*0.000174	0.000016	0.000016	0.000016	*0.000166	0.000004 *0.000166
Sideband Outside ±474 kc	4 4 4	444	4 4 4	ਚਾ ਚਾ ਚਾ	<b>.</b>	44 W W
Maximum X-mtr. Deviation (±kc)	72.4 72.4 72.4	41.5 41.5 41.5	42.42	41.5	31.6 31.6 31.6	32.0 32.0 32.6
Sideband Amplitude (Limit 0.010)	0.0027	*0.0097	*0.0097	*0.0097	0.005	0.005
Actual M.I.	0.51	0.288	0.28 0.276 0.273	0.28 0.273 0.266	0.20 0.198 0.195	0.205 0.20 0.195
Sideband Outside ±294 kc		r r 2	2 2 2	777	7 7 7	2 2 2
Channel Position (kc)	-2 0 +2	4- 0 4-	-2 0 +2	4 0 4	-2 0 +2	4-0+
Subcarrier (kc)	142 144 146	140 144 148	150 152 154	148 152 156	158 160 162	156 160 164

\* Indicates Limiting Case

SIDEBAND CALCULATIONS FOR CONSTANT BANDWIDTH CHANNELS

Conditions: P = 100 watts

Specifications: -40 db at #320 kc

Drift Allowance = 0.01%

-25 dbm at ±500 kc

Sideband Amplitude (Limit 0.000178)	*0.000166 *0.000166	*0.000166
Sideband Outside ±474 kc	<b></b>	mmm 222
Maximum X-mtr. Deviation (±kc)	33.2 33.2 32.8 32.8 32.8	46.0 46.0 46.0 7.14 7.14
Sideband Amplitude (Limit 0.010)	0.005	0.005
Actual M.I.	0.20 0.198 0.195 0.20 0.195 0.191	0.20
Sideband Outside ±294 kc	222 222	222 222
Channel Position (kc)	207 404	2- 2- 2- 2- 2- 2- 2- 2- 2- 2- 2- 2- 2- 2
Subcarrier (kc)		

# SIDEBAND CALCULATIONS FOR CONSTANT BANDWIDTH CHANNELS

Conditions: P = 100 watts

Specifications: -40 db at ±320 kc

Drift Allowance = 0.01%

-25 dbm at ±500 kc

Sideband Amplitude (Limit 0.000178)	0.00016 *0.00011	*0.00011	*0.00011	
Sideband Outside ±474 kc	m 72 72	~ ~ ~	8 8 8	
Maximum X-mtr. Deviation (±kc)	7.2 7.2 7.2	7.38 7.38 7.38	7.32 7.32 7.32	
Sideband Amplitude (Limit 0.010)	0,00011	0.00011	0.00011	
Actual M.I.	0.03	0.03	0.03	
Sideband Outside ±294 kc	~ ~ ~	~ ~ ~	2 2 2	
Channel Position (kc)	404	-5 0 14 7	404	
Subcarrier (kc)	236 240 244	246 248 250	244 248 252	

\*Indicates Limiting Case

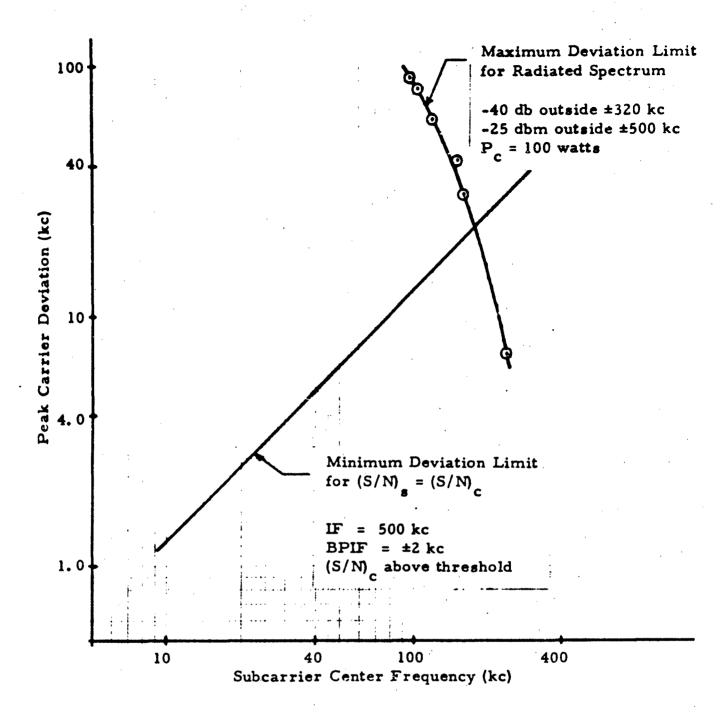


FIGURE II-1.3-7
FM/FM CARRIER DEVIATION LIMIT FOR
±2 KC CONSTANT BANDWIDTH CHANNELS

TABLE II-1. 3-8

CHANNEL ALLOCATIONS FOR

CONSTANT BANDWIDTH BASEBAND

Channel Number	Group	VCO Frequency (kc)	Translation Frequency (kc)	Channel Frequency (kc)
1		16		16
2		24		24
3	A	32	None	32
4	1	40		40
5		48		48
6		56		56
7		56	·	64
8		48		72
9	В	40	120	80
10		32		88
11		24	į	96
12		56		104
- 13		48	·	112
14	С	40	160	120
15	•	32		128
16		24		136
17		56	·	144
18		48	:	152
19	D	40	200	160
20		32	!	168
21	,	24		176

### SECTION 2

### **EQUIPMENT EVALUATION**

### 2.1 GENERAL

This section contains block diagrams, procedures, and measured data for the equipment-evaluation portion of the baseband-expansion study. The equipment evaluation was undertaken to measure characteristics of the equipments used which would affect the accuracy of the telemeter or the ability to add additional higher-frequency channels to the baseband.

### 2.2 VOLTAGE-CONTROLLED OSCILLATORS

Of the 36 standard IRIG  $\pm 7.5\%$  VCOs and two 93.5 kc  $\pm 15\%$  VCOs received as GFE for the study contract, five units were selected for evaluation:

Manufacturer	Model	Frequency	Serial No.
Tele-Dynamics	1270A	3.0 kc ±7.5%	21-404
Tele-Dynamics	1270A	70.0 kc ±7.5%	27 -565
Vector	TS-41	3.0 kc ±7.5%	3742-25
Vector	TS-41	70.0 kc ±7.5%	5683-25
Vector	TS-41HF	93.5 kc ±15%	8485-5

An EMR 307A, 32 kc ±2 kc VCO was also subjected to the same evaluation tosts of static and dynamic linearity, modulation feedthrough, total harmonic distortion, and crosstalk.

Block diagrams and measured data for these tests are contained in Tables II-2.2-1 through 2.2-4.

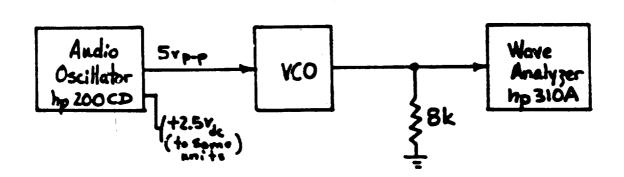
WO STATIC AND DYNAMIC LINEARITY

		Free	- Frequency, cos			•	
Chit	HBE	186	. y	2	387	Static Non-Lin.	Dymamic Now-Lin.
7D1 1270 A 30k ± 75%	3 224.0	3111.8	2 999.2	2886.0	2 772.2	± 0122%	± a122% ≈ ±a05%
TD1 1270A 70.0k±7.5%	75.275	72645.	70 018.	67.386.	64.743.	±0.048%	+0.018% x±a05%
Vector 75-41 304c ± 7.5%	3 225 8	3112.7	2 999.9	2.887.4	2 775.1	±0029% < ±0.05%	150.07
Vector 73-41 70.06. ± 7.5%	15.17.	72625.	69,989. 67.358.	67 358.	64 735.	64 735. ±a069%	z+a057,
Verby 75-41 4F 93.5 to ± 15%	107564	100 6 06.	33 600.	86561	79 495.	79 495. ± a1287.	
EMR 3074 32.0kr ± 2.0kc	34 <b>66.</b>	33 005.	32 003.	31003	30 83.	30003. ±0.0197. x±a017.	ztao17.

### VCO MODULATION FEEDTHROUGH

	Modulation Freq. fm (cps)	Mod. Feed through (% of annodalated VCO output voltage)
TDI 1270A 70.0kc±7.5%	5250 (MI=1)	0.0048%
Vector 75-41 70.0kc ± 7.5%	5250 (M:=1)	0.374%
Vector 75-41 HF 93.5 kc ± 15%	14,000 (MI=1)	0.87%
••	2800 (MI=5)	0.17%
EMR 307A 32.0k ± 2.0k	2000 (MI=1)	0.032%

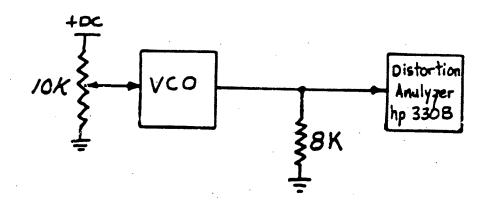
With the audio ascillator at for measure the for, component at the VCO output referenced to the unmodulated VCO output voltage.



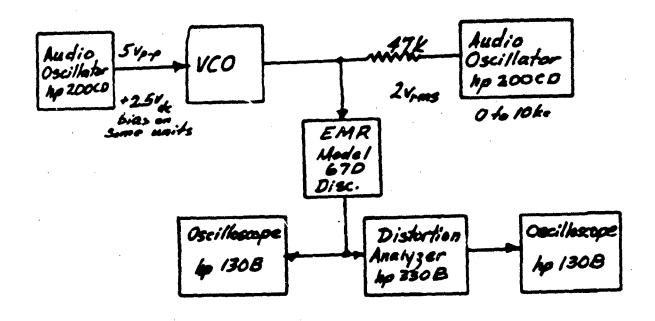
### VCO TOTAL HARMONIC DISTORTION

## Total Harmonic Distortion (Percent of Unmodulated VCO Output Votage)

TD1-1270A 3.04c ± 7.5%	HBE 0.26%	CF Q.42%	LBE a64%
TD1-1270A 70.0k ± 7.5%	0.14%	* .	022%
Vector T5-41 3.0 kt 7.5%	0.40%	0.36%	0.44%
Vector TS-41 70.0 kt 7.5%	0.19%	0.24%	029%
Vector 73-41 HF 93.5kc ±15%	0.45%	0.31%	0.17%
EMR 307A 32.0k ± 2.0k	0.07%	0.07%	0.08%



### VCO CROSSTALK



VCO's were tested as above with a modulating frequency corresponding to an M1=2 and a discriminator output filter (constant amplitude) catoff frequency corresponding to an MI of 1. No crosstalk greater than ±0.1% of bandwidth was observed outside the passband of the discriminator input filter. The experiment was repeated with a 47k resistor substituted for the VCO, with identical results; therefore, crosstalk due to the VCOs was judged to be negligible.

### 2.3 MIXER AMPLIFIER

The Sonex TEX-3210 Mixer Amplifier was evaluated for frequency response, harmonic content, and intermodulation characteristics. The respective results and block diagrams for the tests are included in Tables II-2.3-1 through II-2.3

# FREQUENCY RESPONSE SONEX TEX-3210 MIXER AMPLIFIER

Mixer Gain: +10 db

Frequency	Relative Level	
Cps	db	Voltage ter
50.0	-0.8	hp 400D
100.0	-0.3	
200.0	0.0	Generalis A.7k Sonex Mixer Wolfmeter
7	9	150A TEX-3210 J.Fluke 910A
200.0 kc	0.0	
500.0 kc	-1.2	
850.0k	-3.0	
1.0Mc	-3.8	
2.0 Mc	-8.8	
5.0Mc	-15.2	

HARMONIC CONTENT SONEX TEX-3210 MIXER AMPLIFIER

Fundamental Frequency		-59.5 -7 -59.0 -7 -58.5 -7 -58.0 -7 -58.0 -7 -54.5 -6 -60.5 -7	
	22		44
1 kc	-56.5	-59,5	- 73.0
2 kc	-56.0	-59.0	-72.5
5kc	-55.0	-58.5	-72.0
10 kc	-53.0	-58.0	- 72.0
20 k	-53.0	-58.0	-72.0
50k	-49.0	-54.5	-68.0
100kc	-46.0	-60.5	-72.0
150k	-44.0	-60.5	-73.5

Mixer Gain = + 10 db

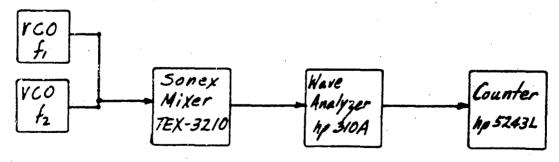
Output Level = Odbm into 600 se or 790 mv

Total Harmonic Distortion . 0.64%. for 150kc case. 13 within the specification for the hp 650A signal generator used. Measureing instrument: hp 3:0A wave Analyzer.

# INTERMODULATION TEST SONEX TEX-3210 MIXER AMPLIFIER

Frequency of the state of the s	ir	/2-	f, "	$f_{i}$	+ f2
f,	f2	Freq.	f, Level	Freq.	t fr Level
400cps	560cps		17 femilis	_	8 prosts
1.3k	1.7kc		8 jurolts		3 posts
14.5kc	22.0kc	7.5k.	77 proffs	36.5kc	24 µ16Hs
93.5kc	124.0kc	30.5kc	24 junits	-	_

Twenty-channel proportional multiplex pre-emphasized as used with output adjusted to 1.0 Vms with all channels operating.



### 2.4 GROUP TRANSLATOR

### 2.4.1 General

The EMR Model 316 Frequency Translator is used in constant-bandwidth FM/FM telemetry systems to generate stable high-frequency subcarrier channels by translating up in frequency the outputs of standard EMR subcarrier oscillators (VCOs) operating in the lower subcarrier frequency spectrum. The block diagram of a constant-bandwidth VHF FM/FM telemeter is shown in Section 1.5 of Volume I.

The outputs of the subcarrier oscillators for CBW channels 1 through 6, 16.0 kc through 56.0 kc, are linearily mixed in the Model 316A-01 for Group "A." The outputs of five subcarrier oscillators, whose center frequencies and frequency deviations are identical to those of the VCOs for CBW channels 2 (24.0 kc) through 6 (56.0 kc), are mixed in the Model 316X-01 Frequency Translator for Group "B. The outputs are frequency translated as a group to the multiplexed subcarrier channel frequencies for CBW channels 7 through 11, 64.0 kc through 96.0 kc. Multiplexed channels 12 (104.0 kc) through 16 (136.0 kc) are similarly obtained by the Model 316X-02 for Group "C," and channels 17 (144.0 kc) through 21 (176.0 kc) by the Model 316X-02 for Group "D." The subcarrier channels in Group "A" are mixed but not translated in frequency. The Group A, B, C, and D outputs are linearily mixed in a Model 311A Mixing Amplifier and the multiplex output signal, consisting of constant-bandwidth FM subcarrier channels 1 through 21, is applied as the modulating signal to the VHF FM transmitter.

The entire telemeter may contain only six different types of subcarrier oscillators. The frequency deviation of all VCOs is within the limits of  $\pm 3.57\%$  to  $\pm 12.5\%$  of center frequency, which makes it possible to generate accurate and stable subcarrier FM signals. A number of proportional-bandwidth channels may be added in the lower frequency spectrum of Group "A" below 16.0 kc if additional channels are required, as is shown in Section 1.5 of Volume I.

### 2.4.2 Specifications

A detailed evaluation program for the group translator was not undertaken as part of the baseband expansion study. The unit was, however, evaluated by other EMR personnel and its performance to the following specifications verified:

Subcarrier Frequencies: Standard constant-bandwidth FM subcarrier channels spaced 8.0 kc apart from 16 kc to 176 kc. Other constant-bandwidth FM systems are available with multiplexed subcarrier channel center frequencies in the range of the 4 kc to 750 kc.

Subcarrier Frequency Deviation: ±2 kc, ±4 kc, and ±8 kc are standard. Other constant-bandwidth FM systems are available with subcarrier frequency deviation in the range of ±1 kc to ±16 kc.

Subcarrier Deviation Polarity: Deviation polarity of subcarrier channels in Group "A" is maintained; deviation polarity of channels in other groups is inverted. Normally overall positive polarity from VCO input to subcarrier discriminator output is maintained due to reinversion of the inverted channels in ground frequency detranslation equipment such as the EMR Model 259.

Input Signal: Model 316A (Group "A"): Outputs of EMR Models 306A, 307A, or 309 A VCOs for channels 1 through 6. Outputs of VCOs for channel A and/or proportional-bandwidth channels may be added if additional channels are required.

Model 316X (Groups "B," "C," "D,"...): Outputs of EMR Models 306A, 307A, or 309A VCOs for channels 2 through 6. For standard constant-bandwidth systems a 46.4k ohm mixing resistor, contained in the VCOs, is used. The EMR VCOs for use in standard constant-bandwidth systems have a floating output ground connection to reduce inter-group crosstalk to a negligible level.

Output Signal: Adjustable to 5 volts peak-to-peak maximum open circuit (measured at output test point), referenced to ground. A series mixing resistor of 10k ohms minimum is installed at manufacture to provide the desired system emphasis.

Heterodyne Signal: A crystal-controlled reference signal is generated within all Model 316A Frequency Translators except the Model 316A for Group "A." A test point is provided for monitoring this signal.

Frequency Range:

50 kc to 800 kc

Frequency Accuracy:

±0.005% at 25°C

Frequency Stability:

±0.0025% from the frequency at 25°C over the range -20°C to +85°C

Subcarrier Gain: Overall subcarrier gain is measured from the input of the VCO mixing resistor (VCO test point) to the open circuit frequency translator output (Model 316A output test point). The subcarrier gain of a frequency at the center of the output passband of the Model 316A is adjusted in manufacture to 0.1 (-20 db). The subcarrier gain for frequencies in the passband from low band edge to the lowest frequency output channels to high band edge of the highest frequency output channel is within ±1 db of the gain measured at the center of the output passband.

Subcarrier Emphasis: Relative subcarrier levels are adjusted by "output" controls of the VCOs. Group level is adjusted by "output" control of Model 316A Frequency Translator. Multiplex level (modulation signal to the VHF FM transmitter) is adjusted by "output" control of the Model 311A Mixing Amplifier. The output mixing resistor of each Model 316A is adjusted in manufacture for approximate mid-setting of the "output" control of the Model 316A for the desired emphasis. Recommended emphasis schedules and list of nominal system levels for standard constant-bandwidth FM/FM systems are available on request.

Spurious Output Signals: Individual spurious output signals are -46 db or less referenced to the nominal individual subcarrier output level. This specification includes the following undesired output signals:

Undesired sideband

Input multiplex feedthrough

Hetrodyne signal (fundamental, harmonics, and sidebands about harmonics)

Input signal harmonics generated in the 316A

Input signal intermodulation products

Power supply ripple components

Based on 5 subcarriers per translation group, nominal levels are:

### Measured Level

	At Test Point of SCO	At Output Test Point of 315A
Subcarrier Level	1.5 rms	0.15 rms
Multiplex Level	•••	2.2 p-p

Power Supply Sensitivity: Operation is as specified with a steady-state supply voltage or a 4-volt peak-to-peak dynamic change in supply voltage (dc to 100 kc) anywhere in the range of +24 to +32 volts.

Power Requirements: Positive 28.0 volts dc nominal referenced to ground; ±4.0 volts; 30 ma at nominal voltage.

Operating Temperature: Operation is as specified with steady-state temperature in the range of -20°C to +85°C.

<u>Vibration</u>: Sinusoidal vibration along each of the three major axes of the reference oscillator at 0.06 inch double amplitude or a peak acceleration of 35g, whichever is less, up to a frequency of 2000 cycles per second, results in an offset change in output frequency of less than 0.005% and incidental FM, measured with a  $\pm 7.5\%$  discriminator at a deviation ratio of 1, of less than 0.1% rms of bandwidth.

Shock: Shock of up to 200g, 11 millisecond duration, causes an offset change in output frequency of less than 0.005% and peak incidental FM, measured with a  $\pm 7.5\%$  discriminator at a deviation ratio of 1, of less than 0.1% of bandwidth.

Continuous Acceleration: Continuous acceleration of up to 300g produces a change in output frequency of less than 0.005%.

Altitude: A change in altitude from sea level to 200,000 feet produces a change in output frequency of less than 0.005% provided the surface on which the unit is mounted is maintained at constant temperature.

Humidity: Operation is as specified over the humidity range of 0% to 95% relative.

### 2.5 TRANSMITTER

### 2.5.1 General

A Leach FM 200 Transmitter and an EMR 121D Transmitter were selected for evaluation as representative telemetry transmitters. The Leach FM 200 is a transistorized unit, while the EMR 121D is a vacuum tube design. Total harmonic distortion and deviation sensitivity were measured on each transmitter for deviations up to ±200 kc and modulation frequencies as high as 225 kc.

The EMR Model 270 Subcarrier Discriminator was calibrated for deviation sensitivity ( $\pm 20.0\pm 0.2\%$ ); linearity,  $\pm 0.1\%$  BSL; and total harmonic distortion data on the particular audio oscillator used was measured; the data is included as Table II-2.5-2.

### 2.5.2 Total Harmonic Distortion

Equipment outlined in Figure II-2.5-3 was used to measure transmitter total harmonic distortion. Each transmitter was evaluated by using frequency translation and the EMR 270 Subcarrier Discriminator as a precision receiver. Detailed procedure for the total harmonic distortion tests is as follows:

- 1. With equipment set up as in Figure II-2.5-3, set the audio oscillator to the desired fundamental frequency. Fundamental frequencies of 3.0 kc, 30 kc, 70 kc, and 225 kc were used.
- 2. Adjust the audio oscillator amplitude to yield the desired transmitter deviation as indicated by the discriminator output voltage measured on the HP 310A Wave Analyzer. Record the transmitter input voltage level required.
- 3. Tune the wave analyzer to harmonics of the fundamental and record their levels.
- 4. Compute the total harmonic distortion as follows:

%THD = 
$$\sqrt{\frac{\sigma_2^2 + \sigma_3^2 + ... + \sigma_n^2}{\sigma_1}} \times 100$$

where,

Harmonic distortion data obtained for the EMR 121D and the Leach FM 200 are given in Tables II-2.5-4 through II-2.5-8 and Tables II-2.5-9 through II-2.5-13, respectively. This data is presented graphically in Figures I-2.5-1 and I-2.5-2 of Volume I.

### 2.5.3 Deviation Sensitivity

By measuring the transmitter input signal level as part of the total harmonic distortion test, data on deviation sensitivity is obtained without a separate test. Data measured on transmitter input level as a function of deviation and modulation frequency is presented in the same Tables II-2.5-8 through II-2.5-13. Graphical presentation of the data is included in Volume I, Figures I-2.5-3 through I-2.5-6.

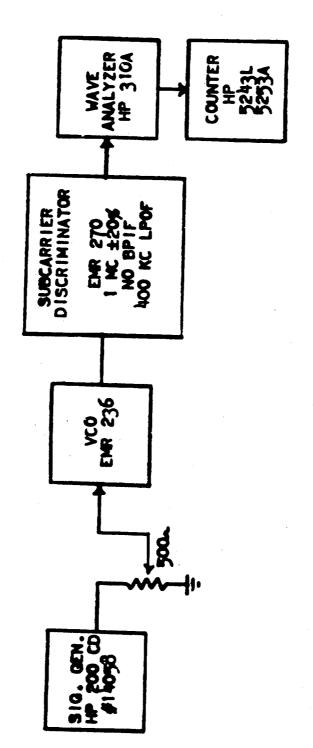


FIGURE II-2, 5-1 OSCILLATOR/DISCRIMINATOR TOTAL HARMONIC DISTORTION

TABLE II-2, 5-2 OSCILLATOR TEST RECORD

MFR L	6/	MODEL	MODEL 200CD	8/N 14	14053	ORIGINA	OPICINATOR (US &	DATE 9.464	4.67
Deviation	Transmitter Input Level rms volts		Fund.	Second Harmonic	Third	Fourth Hærmonic	Fifth Hermonic	Square Root Sum me	Total Harmonic Distortion
±25 kc		Frequency rms output ms output	3.0 ×	6 KC 5.0mv 25.10-6	9 KC 6.5mv 42.35.10-6	12Kc	15-KC 0.2 m.v	15-KC 0.3 mv 0.04.10-6, 8.2 x10-3 V 0.372 %	0.274%
£50 kc		Frequency rms output ms output	30 KC 3.0 V	60 KC 5.7m 32.49.10 tv	90KC 6.800	120 KC	1,50KC 0,3 mt	150kc 0.3 mv 0.09.10-6 V: 8.91-10-3V: 0.297 %	287 %
±75 kc		Frequency rms output ms output	70 %C 3.0 v	140 KC 50 mu 250.10-64	2.10 KC 3.4mi	28046	35.04c 35.04c 35.1 my	6.79.10° V 0.321. %	231. %
±100 kc		Frequency rms output	100 AC 3.0 V		300 KC 2.5mv	40015	500 AC 2.7" / 7.39.10.6v	5004c 2.7~ 7.39.10-6v.6.31.10-3v.0.207.0/	0 207 %
. ±125 kc		Frequency rms output ms output	225'4C 3.01		675'KC 5.3 mu 28.05.10-14	900 40	1,23.4c 1.7 mv 2,89.10.6v	1,25.4c 1.7 mv 2.89.10 6 V 6 91.10 3 x 0.3 x 0.9%	2000
±150 kc		Frequency rms output ms output							
±175 kc		Frequency rms output ms output							
±200 kc		Frequency rms output ms output							

Ψ.

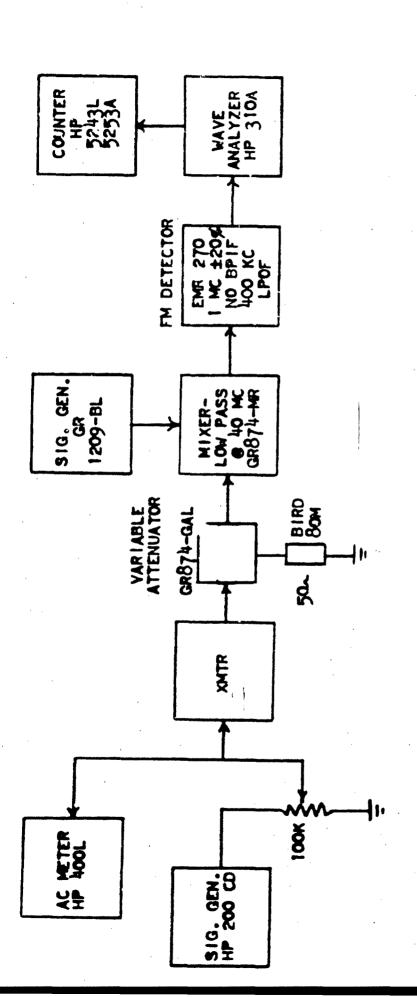


FIGURE II-2, 5-3 TRANSMITTER TOTAL HARMONIC DISTORTION TEST

TABLE II-2, 5-4 TRANSMITTER TEST RECORD, EMR 121D, 3 KC FUNDAMENTAL

h9-1-	Total Harmonic Distortion	0.33%	0.36%	0.38%	0.37%	0.40%	0.44%	0.70%	0.61%
DATE 9-1-64	Square Root Sum ma Output							8	
<b>TOR</b>	Fifth • Ha'rmonic						·		1.3mv
ORIGINATOR	Fourth Harmonic	0.7mv	0,8mv	0.9 mV	0.8mv				1.4mv
22	Third Harmonic	1.9mv	4,0mv	6.0mv	7.0mv	9.0mv	12.0mV	20.0mv	20.0mv 1.4mv
S/N 922	Second Harmonic	2.1 mv	4.8 mv	8.220	11.0mv	15.0mv	20.0mv	38.0 mv	38.0mv
MODEL 121	Fund.	O. 885'V	1.77	2.66 Y	3.54Y	4.421	5,31 V	4.19V	7.07
MODEL	3.0xc	Frequency ring output ms output	O. 415V rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output	Frequency rms output	Frequency rms output ms output
MR	Transmitter Input Level rms volts	0.210V	0.4150	0.6381	O. 332V rms output	1.057	±150 ke   1,25 V	#175 kc 1. 40 V	*200 kc 1.66V
MFR EMR	Deviation	±25 kc	±50 kc	±75 kc	*100 kc	±125 kc	±150 kc	#175 kc	±200 kc
<u>ا</u> 	. 1	<u> </u>			39 <b>-</b>	ام ما المستحدد - الم			

TRANSMITTER TEST RECORD, EMR 121D, 30 KC FUNDAMENTAL

`.	l nic 10n	<u>                                   </u>	1		<u> </u>	T			
1.64	Total R: rinonic Distortion	0.56%	7.0°	0.73%	-0.81%	0.40%	0.99%	1.0737	1.27
DATE 9.1.74	Square Root Sum ms		i			el escenes e es		 	
JAMENTAL TOR	Fifth Harmonic		1,500	, , , , , , , , , , , , , , , , , , ,	<b>M</b>	6.5%	3.0 miv	6.3 m /	2.7%
MODEL 12/ S/N 222 ORIGINATOR	Fourth Harmonic	0.4mv	0.720		1.10:0	277	4.400	6.5mv	V 45 CH
), EMR 121D, ラスス	Third Harnionic	1.8000	24.9	5,20,1	4.0,	9.00%	9.5 mv	13.0mv 6.5mv	19.0
RECORD, B $S/N$	Second Harmonic	4. 6mV	6.0	19,000	27.00.	38.Ca) v	57.0mv	64.Emv	37.00:0
12 / 12 /	ġ.	0.8857	1471	200%	3.54V	4.431	5.311	761.9	7.07V
I RANSMIT MODEL	30 KC	Frequency rms output ms output	Frequency rms output	Frequency rins output ms output	Frequency rms output				
EMR	Transmitter Input Level rms volts	0.2121	0.4201	0.6357	O.840Y	1.057	1.26	±175 kc 1.47V	±200 kc 1. 68V
MFR E	Deviation	±25 kc	±50 kc	±75 kc	#100 kc	±125 kc	±150 kc	±175 kc	±200 kc

weet of of

TABLE II-2, 5-6 TRANSMITTER TEST RECORD, EMR 121D, 70 KC FUNDAMENTAL

DATE 9-1-64	Total Harmonic Distortion	0.79%	0.93%	0.78%	1.35%	1.67%	% 081	2.27%	2.87%
DATE 9	Square Root Sum me Output	·			-				·
TOR	Fifth Harmonic		2.5mv	5.5mV	10.0 m v	6.2mv	16.0mv	9.0mJ	7.2 mV
OTIGINATOR	Fourth Harmonic		7.9 mv	9. Fmv	6.6mv	6.420	5.5 mv	11.0 m v	27.0mv
922	Third Harmonic	1.7mv	3.6 mv	3.0 m :	17.0 mv	22.0mv	16.0m	23.Camy	36.0mv 27.0mv
SIN 9	Second Harmonic	6,4 mv	13.020	16.0mJ	40.0mv	66.0m1	94.0 ms	130 mV	187mV
121.	Fund.	0.835'V	1.70%	2.577	3.31	4.198	5,10 V	5.86V	401.9
MODEL 12	70 KC	Frequency rms output ms cutput	Frequency rms output	Frequency rms cutput ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output rns output	Frequency rms output ms output	Frequency rms output ms output
EMR	Transmitter Input Level rms volts	0.2011	0.4204	0.6201	O. 840Y	1.035	1.257	1.45.V	±200 kc / 65 V
MFR	Deviation	±25 kc	±50 kc	±75 kc	±100 kc	±125 kc	±150 kc	175 kc	±200 kc

TRANSMITTER TEST RECORD, EMR 121D, 100 KC FUNDAMENTAL

DATE 9-1-64	Total Harmonic Distortion	0.98%	1.40%	1.97%	2.36%	2.71%	3,17%	3.62%	26 H/h 'H
DATE 9	Square Root Sum ma								
AMENIAL TOR	Fifth Harmonic		1.6 m v	8.577	.5,0mv	5.2 mv	5.7mv	11.0mv	14.0miv
ORIGINATOR	Fourth Harmonic		1.2 mu	5.9 mv	6,3 mv	7.7mv	6.6 mv	26.0 mv 14.0 mv 11.0 mv	28.000
922 ORIGINATOR	Third Harmonic	1.7mv	11.0mv	6.5mv	29.0mv	26.0mv	23.0mv 6.6mv	26.0mv	39.0mv
s/n	Second Harmonic	8.0 mv	21.0mv	48.0mv 6.5mv	73.0mu	110011	16000	210mv	J93mv
121	Fund.	0.8357	1,70 /	2.571	3.341	4191	5:10 V	5.86Y	6.700
MODEL	700110	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	rris output	Frequency rms output ms output
EMR	Transmitter Input Level rms volts	0,2184	0.4411	0.6500	0.8657	1.091	1.321	1.531	±200 kc. 1.76 V
MFR E	Deviation	±25 kc	±50 kc	±75 kc	±100 kc	±125 kc	±150 kc	±175 kc	±200 kc
			<del></del>	-47	2 -				.••

sheet of of 5

TABLE II-2, 5-8 TRANSMITTER TEST RECORD, EMR 121D, 225 KC FUNDAMENTAL

( )

Total Hermonic Distortion	1.09%	1.42%	2.05%	2.41%	3.08%	4.28%	5.47%	6.53%
Square Root Sum ma Output								
· Fifth Harmonic			0.3mv	0.7mV	1.2 mv	2,0 m V	2.7 mv	3.5°mv
Faurth Halmonic			0,7mv	1.4mv	2,2 mv	3.0mv	5.000	7,2mV
Third Harmonic	Jo.5'mu	4,7mv	6.8mv	11.0mv	18,0mv	30.0mv	, mo.09	97.0mv
Second Harmonic	5.6mv	22.0mv	48.0mv	75:0mu	120mv	200mu	295771	400mv
Fund,	O.79 V	1.5-8 v	2,37	3.157	3.941	4.73 V	5.571	6.300
225%	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency frms output ms output	Frequency frms output ms output	Frequency rms output ms output
Transmitter Input Level rms volts	0.2861	a 5581	0,8501	1.14 V	1.481	1.88V	ì	±200 kc . 2. 93V
Deviation	±25 kc	±50 kc	±75 kc	±100 kc	±125 kc	-±150 kc	±175 kc	±200 kc
	Transmitter Second Third Fourth Fifth Square Root Input Level Fund. Harmonic Harmonic Harmonic Sum ms rms volts 225%c	Transmitter Input Level Input Level Imput Level Input Level Imput	Transmitter  Transmitter Imput Level Imput Ind. Ind. Imput Level Imput Ind. Ind. Ind. Ind. Ind. Ind. Ind. Ind.	Fransmitter Input Level Input Level Input Level Ima volts  225Kc  Fund. Harmonic Harmonic Harmonic Sum ma  O.286V rms output  O.56Wv  Trequency  O.55V rms output  C.85OV rms output  D.85OV rms output  D.85V rms output  D.85V rms output  Trequency  O.85V rms output  D.85V rms output  Trequency  O.85V rms output  D.85V rms output  Trequency  O.85V rms output	Transmitter Input Level Industrial Industri	Transmitter Imput Level Imput	Tranguittes I Fund. Harmonic Harmonic Harmonic Harmonic Sum masouput  O. 286 V rms output  O. 558 V rms output  O. 850 V rms output  I.HV Frequency  II.HV Frequency  III.HV Frequen	Franchittes Input Level Imput

TRANSMITTER TEST RECORD, LEACH FM 200, 3 KC FUNDAMENTAL

DATE 9-3-64	oot Tot.1 is H. rmonic t l Distortion	0.843	0.63	0.36%	7.3017	1.43%	1.73%	2.03°	2.343,
	- S	15:0 KC	15:00.	15,0470	15'5 % C 0.66 % 2	1.5-0 tc 0.50mu	15,5 h 6	15.0 0.6cms	1.5 m. 6. 1. 0. 1.
OPIGINATOR L.S. B.	Fourth Harmonic II	12.0 KC 1	12 c kc +	12.6kc 1 0.75mu -	•	12.016 1.	12.0 KC 1	12,0KC / 0.9mv C	1.4m
39	Third Harmonic	90 KC	9.50 mg	9.0 AC 5.0 ms	4 0 kc	9.0 Kc	9.5 mV	9.0AC	1.0 MV
S/N	Second	2.9000	6.0 °CC /0.0 m.s	25.03 m	6.0 Kc 38.5 mu	63.0 mv	6.6 hc	6.0 hc 125 me	6.0 hc
FM200	F und.	3.0 kc 0.885V	3.6 KC 1.77 V	2.66K	3.0 KC 3,54Y	3.0 KC 4,42V	3.040	3.0 KC 6.19 V	3.016
MODEL	Fund, Freq 3 KC	Frequency rms output	Frequency rins output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rins output ms output	Frequency rms output ms output	Frequency rms output
HC H	Transmitter Input Level rms volts	0.2200	0.440	±75 kc   0.650V	±100 kc   0. 8 60 V	1.10 ×	±150 kc   .34 V	1.537	1.757.1
MF F L ENCH	Deviation	±25 kc	±50 kc	±75 kc	#100 kc	±125 kc / 10 V	±150 kc	±175 kc	±200 kc

TRANSMITTER TEST RECORD, LEACH FM 200, 30 KC FUNDAMENTAL

-4.64	Total Hermonic Distortion	041%	0.58%	0.93%	1.24%	1.48%	1.80%	2.03%	2.34%
DATE 9-464	Square Root Sun ms Output		:		•	· · · · · · · · · · · · · · · · · · ·			
ORIGINATOR M.S. B.	Fifth Harmonic	•	O. 40 mv	1.20	4.0 0.7	1.6mv	6.400	5,2mv	6000
ORIGINA	Fourth Harmonic	0.40ms	1.811	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.2 mu	2.0000	₹% % %	4.3mc	5,600
39	Third Harmonic	). J	1.9 mi	5.600	6.5m	8.2 m.c.	8.0 mv	9.3mc	your
S/N 3	Second Harmonic	3.400	10.011	24.0mu	430mc	65.0mv	95.0m	125 m	165mv 40mv
MODEL FM 200	Fund.	0.885'V	1.77	2,66	3.540	4.421	5.314	191	707
MODEL	38 KC	frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ins output	Frequency rms output ms output	Frequency rris output	Frequency rrns output ms output	Frequency rins output
LEGEN	Transmitter input I evel rms volts	C.222V	0.444	0.6601	+100 kc 0 875V	/111/	1.351	1,551	1.76 v
MF P LE	Deviation	±25 kc	±50 kc	±75 kc	±100 kc	±125 kc	±150 kc	±175 kc	+200 kc

TABLE II-2, 5-11 TRANSMITTER TEST RECORD, LEACH FM 200, 70 KC FUNDAMENTAL

	υĘ	1 70			1 · . n				
4.64	Total H. rmonic Distortion	0.37%	0.64%	0.93%	1.24%	1.52%	1.79%	1.99%	2.33
DATE 9-4-64	Sq	•		:					
ORIGINATOR (J). S. B.	Fifth			1.12.7	8.0 m	2.9 mv	7.6ms	5.4mv	7.6 mv
59 ORIGINATOR W.S. B.	Fourth Harmonic		1.85mr	5.2mv	5.4 mv	3,0 mv	6.320	3.6 mv	11.0mv
39	Third Harmonie	1.1mv	2.1 mv	3.0mv	8.5°mv	14.0 mv	10.0mv	12.0mv	12.0 mu
s/N 3	Second Harmonic	2.9mv	10.5mv	22.5mv	40.0 mv	62.0 mv	40.0 mv	116mv	155mv
MODEL FM200	Fund,	0.83	1.70 V	2.577	3.34r	4.19 V	5.10 V	5.86 V	6.707
MODEL	70 % 6.	Fréquency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency rms output ms output	Frequency irms output ms output	Frequency rms output ms output	Frequency rms output ms output
LEACH	Transmitter Input Level rms volts	Vecc.0	0.4501	0.6621	0.8721	1.134	1.36 V	1.56 r	1.774
MFR LE	Deviation	±25 kc	- ±50 kc	±75 kc	±100 kc	±125 kc	±i50 kc	±175 kc	±200 kc
				-4	6-			•	

Sheet 3 of 5

TRANSMITTER TEST RECORD, LEACH FM 200, 100 KC FUNDAMENTAL 

MFR LEACH	ACH.	}	MODEL EMZEO	S/N 39	5	OFIGINA	ORIGINATOR WS. B	DATE 9-4-64	464
Deviation	Iransmitter Input Level rms volte	100KC	Faund.	Second	Third Harmonic	Fourth Harmonic	Fifth Harmonic	Square Root Sum ms Output	Total - Hermonic Distortion
±25 kc	0.240v	Frequency rms output ms output	0.8357	J.6 M.V	1.7 mv	0.6 mlV			0.48%
±50 kc	0.497	Frequency rms output ms output	1.70V	11.0mv	5.2 mv	2,1m			0.73%
±75 kc	0.747	Frequency rms output ms output	2.577	24,2mv.14.0mv	4.0 mv	2.4mv	3.0 mv	·	0.53%
=100 kc	0.941	Frequency rms output ms output	3.34V	40.0mv	8.6m	2.0mv	5.6 m		1.24%
±125 kc	1.20 v	Frequency rms output ms output	4190	64.0mv	17.5 mv	3.5mv	3, 2, m,		1.59%
±150 kc	<i>√8/</i> : ′	Fr uency rms tput ms output	5.10 V	100.0mv 13.6mv	13.6mv	5.0mv	4.2 mv		1.980%
±175 kc	1.681	Frequency rms output ms output	5.86V	127.0mv	127.0mv 23.0mv 9.0mv	9.0mg	3.0 0.4		2.21%
±200 kc	±200 kc / 9/ v	Frequency rms output ms output	402.9	145.0mV	145.0mv 54.0mv 47.0mv	ì .	41.0 mv		2.49%
									1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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TRANSMITTER TEST RECORD, LEACH FM 200, 225 KC FINDAMENTAL

7. 9.4.64	Sum ras H. rmonic	1	0.700	0.37	Cart So. 1	1.5.33	1.84°	2.06%	2.33%
RECORD, LEACH FM 200, 225 KC FUNDAMENTAL  O S/N 39 ORIGINATOP (A S. DATE 9-4-64)	1 ifth Square Rermorie Sum		,		0.7111.	1.3 mv	2.1 ml	3.0 my	4.0
, 225 KC FU	Fourth		0.3	0.60	0.555mV 0.7mV	1.0 mlv	500	110.0 mv 28.5 mv 4.4 mv	145.0my 44.0n; 6.3ml 4.0m
ACH FM 200, 9	Third Harmonic	Lomv	ma GS C	1.9 mv	3.2 22	7.0 ms	36.0mv 15.0 FV	28.5m	44.0";
CORD, LEAC S/N_39	II T	3.2 mv	7.5 my	19.0 mv	39.0 mv 3.2 mv	60.0 mv 7.0 mv	86.0mv	110.0 my	145.0mv
: 51		0.79 V	1.5'8 v	2.37V	3.157	3.941	4737	5.577	75
TRANSMITTER TEST MODEL <u>EM2</u> (	225.KC	Frequency rms output ms output	Frequency rms output ms output	Frequency rris output nis output	Frequency rms output	Frequency rms output mr output	Frequency rms output ms output	Frequency rnis output ms output	Frequency rms output ms output
LEACH	Transmitter Input Level rms volts	0.355V	0.697	, 06 v	±100 kc // 40v	±125 kc // 7/ /	±150 kc 2.06 v	±175 kc   2.40 V	±200 kc 2,757
MFR LE	Deviation	±25 kc	34 04 41	5 <u>7</u>	±100 kc	±125 kc	±150 kc	±175 kc	±200 kc
				•	48-	·	,,	a	· .

Sheet 5 " 5

### 2.6 RECEIVER

### 2.6.1 General

A Vitro/Nems-Clark 1455A Telemetry Receiver and a Defense Electronics, Inc. TMR-2A Telemetry Receiver, both tunable from 215 Mc to 260 Mc, were evaluated as part of the equipment evaluation program. Intermediate frequency (IF) amplifier amplitude and time-delay characteristics, and output noise density were evaluated on each receiver. Total harmonic distortion was measured for the Nems-Clarke 1455A in combination with the EMR 121D Transmitter.

### 2.6.2 IF Amplifier Characteristics

### 2.6.2.1 Amplitude Response

The Nems-Clarke receiver was equipped with 5-Mc IF amplifier, IFM-500-1; the defense Electronics receiver was equipped with a 10 Mc-IF amplifier, IFA-D2. The amplitude response of the Nems-Clarke IF amplifier was tested using equipment as shown in Figure II-2.6-1 and the following procedure:

- 1. With the oscillator at 5.00 Mc select an input signal level such that the amplifier is not saturating, i.e., such that a change in input amplitude provides the same relative output change.
- 2. Tune the oscillator across the bandwidth of the amplifier. Record the input signal level required at a given frequency to maintain a constant output level equal to that at 5.0 Mc, bandcenter. Record the output level used.
- 3. The increase in signal level required relative to band center is the IF amplitude response as a function of frequency.

Results for the Nems-Clarke 1455A Receiver are given in Figure II-2.6-2 and are presented graphically in Volume I, Figure I-2.6-1.

Measurements of Defense Electronics, Inc. TMR-2A Receiver IF amplitude response characteristic were complicated by the lack of a precision voltmeter operable at and above 10 Mc. The technique employed uses the equipment as shown in Figure II-2.6-3 and the following procedure:

- 1. With the equipment connected as shown, disable the receiver automatic gain control (AGC) feature by grounding J-105, pin A.
- 2. Tune the oscillator to center frequency, 10 Mc, insert 65 db attenuation and establish a reference voltage level on the oscilloscope.

3. Tune the oscillator across the passband of the amplifier in convenient steps recording the frequency and attenuation settings required to maintain the reference level on the oscilloscope. (The response of the particular oscillator used varies smoothly from +1.0 db at 9.50 Mc to -1.0 db at 10.5 Mc, relative to 0.0 db at 10.0 Mc.)

Amplitude response data on the TMR-2A Receiver is presented in Figure II-2.6-4 and appears graphically in Figure I-2.6-2 of Volume I.

### 2.6.2.2 Intelligence-Delay Variation

Each receiver's IF amplifier was measured for intelligence time-delay variation across its passband relative to that at band center. The equipment used is outlined in Figure II-2.6-5. In general terms, the procedure involves using a 10-kc tone to generate harrow-deviation frequency modulation which, using the receiver's internal local oscillators, is positioned in frequency across the IF passband. The FM signal at the IF output is then translated and detected by a precision discriminator. Phase shift of the 10-kc intelligence tone as the FM signal is positioned at different frequencies across the IF passband can be easily converted to time delay variation relative to band center. The procedure in detail is as follows:

- l. With the transmitter input grounded, adjust the receiver local oscillators to produce an IF amplifier bandcenter signal.
- 2. Adjust the HP 650 oscillator to produce a much larger signal than that of the IF output at a frequency such that a 1.00 Mc band center signal is supplied to the EMR 270 Subcarrier Discriminator.
- 3. Apply 10 kc to the transmitter at a level such that the 1.00 Mc ±5% EMR 270 Discriminator produces 573 mv peak or 1.15 volts peak-to-peak output.
- 4. Adjust the amplitude and phase through the phase shifter so that a null is obtained at the input to the oscilloscope between the discriminator output and the phase shifter output with the IF signal at center frequency.
- 5. Ground the phase shifter output and verify that the full-scale voltage being nulled is 573 mv peak-to-peak at the HP 130B oscilloscope input.
- 6. Measure the approximate time delay between the transmitter input and the discriminator output with the Tektronix 545A Oscilloscope.
- 7. Reestablish and record the null condition for the IF signal at bandcenter.
- 8. Tune the receiver local oscillator to shift the IF signal to a new frequency position in the passband.

- 9. Tune the HP 650A to return the discriminator input to 1.00 Mc, band center.
- 10. Do not adjust the phase or amplitude settings in the lower or upper paths.
- 11. Read the peak-to-peak voltage from the HP 130B. Each 10-mv peak-to-peak increase in the null voltage as the IF signal is positioned at various places in frequency across the IF passband corresponds to a 1 phase shift at 10 kc, or 0.278 µsec of time delay variation relative to the IF bandcenter condition.

The results obtained for the time-delay variation for each of the two receivers tested are combined with the amplitude response test results as given in Volume I, Figure I-2.6-1 for the Nems-Clarke 1455A and Figure I-2.6-2 for the Defense Electronics, Inc. TMR-2A.

### 2.6.3 Output Noise Density

Receiver output noise density was measured on the Nems-Clarke 1455A and Defense Electronics TMR-2A for various carrier-to-noise ratios. The equipment employed is shown in Figure II-2.6-8. Procedures used in making the measurements were slightly different with each receiver due to variations between units. A general procedure with individual variations noted is as follows:

- 1. Establish a fixed AGC level in the receiver; -4.0 volts dc was used for the 1455A, 1.5 volts for the TMR-2A.
- 2. Measure noise. For 1455A 5-Mc IF amplifier, use J. Fluke 910A True RMS Voltmeter to measure total IF noise. For TMR-2A 10-Mc IF amplifier, use Sierra 158A High Frequency Wave Analyzer to measure the noise level in a 4.5 kc bandwidth (determined by separate test of 158A) and convert to total IF noise by the square root of the ratio of the IF bandwidth to 4.5 kc, the analyzer bandwidth.
- 3. Measure the IF amplifier output signal level with the Sierra 158A using an unmodulated carrier. Set the carrier level for the desired signal-to-noise ratio. The Sierra 158A has been calibrated to read the same as the J. Fluke 910A with a 0.6 volt, 5-Mc signal applied to both.
- 4. Measure the receiver output noise with the HF 310A frequency-selective voltmeter and divide the resulting voltage readings by the square root of the bandwidth used to normalize the data. Express this quotient in decibels.

Results obtained are presented in Figure II-2.6-9 for the 1455A and Figure

II-2.6-10 for the TMR-2A. Volume I, Figures I-2.6-3 and I-2.6-4 present the measured results in graphical form.

### 2.6.4 Total Harmonic Distortion

Total harmonic distortion characteristics of the two FM detectors of the Nems-Clarke 1455A receiver were measured in combination with the EMR 121D Trans-mitter which had been evaluated independently as previously described. The procedure of summation of individual harmonic components, as measured on a frequency-selective voltmeter, was used. The equipment employed is given in Figure II-2.6-11, the block diagram of the test.

The procedure used is as follows:

- 1. Adjust the oscillator to the desired modulating frequency. Modulation frequencies of 3 kc, 30 kc, 70 kc, 100 kc, and 225 kc were used.
- 2. Set the transmitter input level for the desired deviation in accordance with the previously measured transmitter sensitivity. Deviations from ±25 kc to ±200 kc in ±25 kc intervals were used.
- 3. Adjust the receiver gain to produce 1.0 volt rms fundamental output as measured on the HP 310A frequency-selective voltmeter.
- 4. Measure the harmonics individually and compute the total harmonic distortion.

Harmonic distortion data obtained from the Nems-Clarke 1455A in combination with the EMR 121D is given in Figure II-2.6-12 through II-2.6-21.

### 2.6.5 Intermodulation

Difference-frequency intermodulation products were measured using the block diagram of Figure II-2.6-22. Data obtained is contained in Tables II-2.6-23 and II-2.6-24. The receiver output was maintained at 1.0 volt rms.

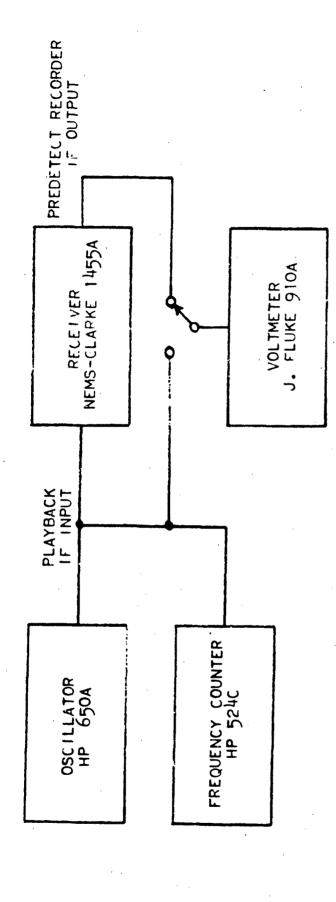
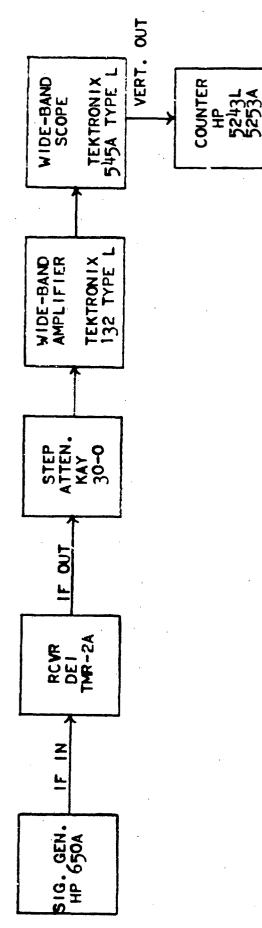


FIGURE II-2, 6-1
IF FREQUENCY RESPONSE TEST, NEMS-CLARKE 1455A

## IF AMPLITUDE RESPONSE Nems-Clarke 1455A (4, 283) & IFM 500-1 (4, 155)

Freg.	Input	Output	Response S
ke	Input	de	de
4500	-1.0	-3/	-60.0
4600	-26.6	-30	-33.4
4700	-50.8	-30	- 7.2
4717	-54.0	-30	-6.0
4738	-57.0	-30	-30
<b>4800</b>	-61.8	-30	+1.8
4900	-61.2	-30	+1.2
5000	-600	-30	0.0
5100	-57.4	-30	-2.6
5200	-58.0	-30	-2.0
5300	-52.9	-30	-7.1
5400	-30.8	-30	-29.2
5500	-13.9	-30	-16.1
5270	-57.0	- 30	-3.0
5294	-54.0	-30	-60
5603	- 3.0	-33	-60.0
1821	-61.8	-30	+1.8 (Peak)
5230	-58.0	-30	-2.0 (Peck)
5130	-56.7	-30	-3.3 (volley)



IF AMPLITUDE RESPONSE TEST, DEFENSE ELECTRONICS, TMR-2A FIGURE 11-2, 6-3

### IF AMPLITUDE RESPONSEDE THE THREE SAME IFA-DE

Frequency (mc)	Response (db)
9.34	-36
9.5	-30
9.54	- 24
9.64	-12
9.71	-6
9.75	-3
9.77	-2
9.78	-/
9,82	0
9.38	+/
9.95	0
10.0	0
10.1	0
10.15	-/
10.2	-2
10.23	-3
10.27	-6
10.34	-/2
10.47	-24
10.52	-30
16.62	- 36

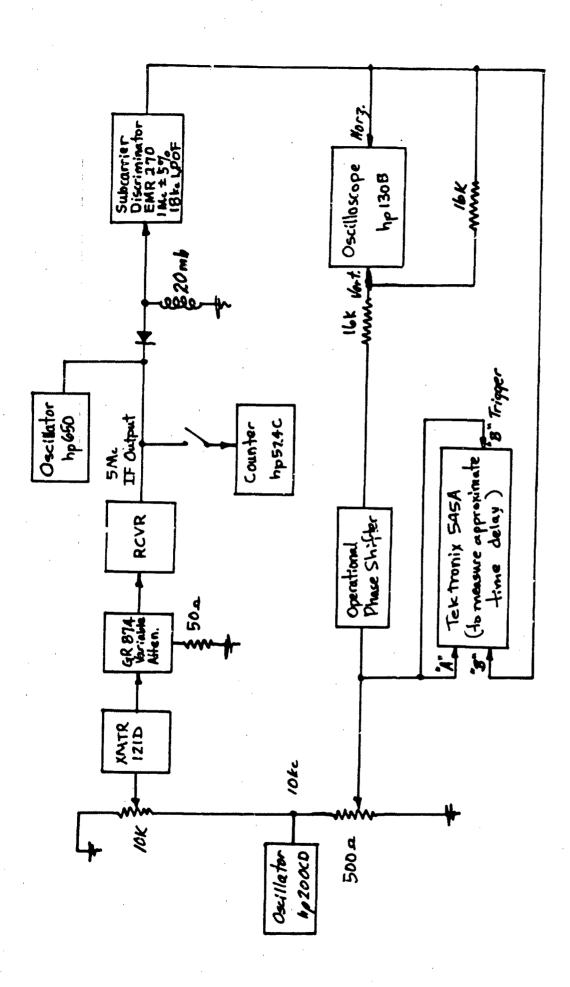


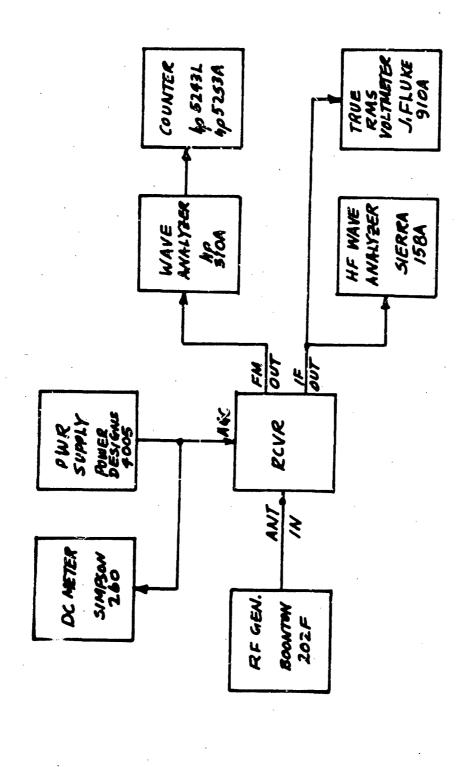
FIGURE II-2. 6-5 IF AMPLIFIER INTELLIGENCE DELAY TEST

## IF INTELLIGENCE DELAY Noms-Clarko 1955A 3/N 283 with IFM-500-1 5/N 155

fm	= 10.00	00 40	1900	000 KC	= 0.2778 MSEC.
Nomina/	MEASURE	Nure	DEGREES	CALCULATE	= 0.2778 M S.c.
		VOLTAGE	<b>U</b> +	DELAY	Time Daisy DETA
	FREA KC	Marsi Tolker	FM	P SEC.	Measure-
4600	4600	€ 10 mu		jest	-31 msec -1 pr
	4700	100 mg		2.778 "	-32 -2
4800	4800	55 mx	55°		-32 " -2
4900	4900	NO.SE \$10MV			-31 " -1 "
5000	5000	Null P.			-30 ., 0 "
5100	5100	Noise < 10 min			-3/ " -1 "
5200	5200	40 mu	4.0°	1.1112	
5300		A .P	9.40	2.611	
5400		Noise & IChi			
4717		100 mu	10°	2.778	
4738	· · · · · · · · · · · · · · · · · · ·	96 mu	9.6°	2.669 "	
5270			2.4°	2.334 "	
5294					
4650		_	•	2.500" -	
_ •	. =	85mv	_	2.361 "-	
5350		96 mv 1	•	2.669	-355 11
5450	5450	92 mu 9	9.2°	2.556 / -	27" +3 "
5325.	5325 /	104mu	19.00	2.889	33" -3 ,
5425 3	5425	20 mu	2.0	2.556"	·30 ·· 0 ··
5477	5417	104mv 1		_	27 " +3 "
4675	4675	90 mu	^	2.500 " -	_

### IF INTELLIGENCE DELAY DEI TMR-ZA with IFA-DZ

Frequency (mc)	Phase Shift (0°)	Time Delay (us)
9.6	1.0	0.28
1.7	2.7	0.75
9.8	3.4	0.94
9.9	1.4	0.39
10.0	0	0.0
10.1	1.0	0.28
10.2	2.7	0.75
10, 3	3.3	0.92
10.4	1.5	0.42



. .

FIGURE II-2, 6-8 RECEIVER OUTPUT NOISE DENSITY TEST

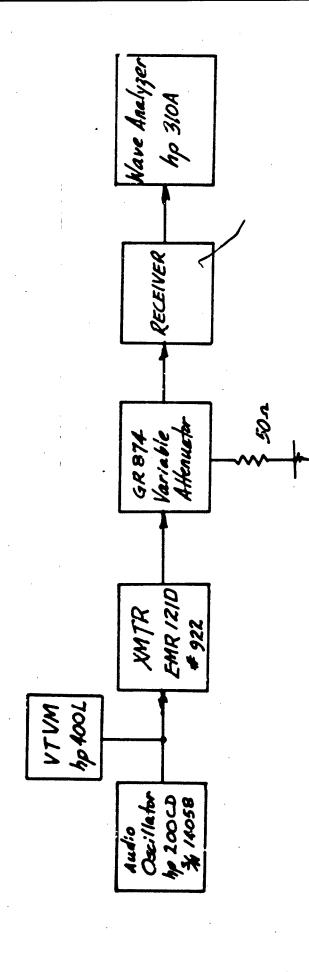
TABLE II-2, 6-9 OUTPUT NOISE DENSITY, NEMS-CLARKE 1455A

F. 11000 (db)		
En Outhat Maise in (bookpa Bw (millivalls)	32 22 22 22 22 22 22 22 22 22 22 22 22 2	
F. 17000		
En Output Noise in 1000 cm BH (millim(Az)	20 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
	*,	(5/N) = 14 db 19 * -95 + -88 -80 5 -69 5 -67 -67 -67
Em Culput Noise in 1000 car Bri (millionits)	34 × 44 × (%)	9.19 * 1.0 1.0 2.4 2.0 35. 35. 1.1 2.4
F. 71000 (db)	Signal Access*  Lise Only  -424  -42  -42  -42  -42  -42  -42  -	(\$\langle \chi_0
En Ontpat Noise In Coope But (militable)	76 Sign 186 * 186 186 * 186 186 * 186 186 * 186 186 * 186 186 * 186 187 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188 * 188 188	8.5 6.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0
Frequency	/k; 4 k; /0 k; /0 0 k; 20 0 k; 30 0 k; 40 k;	14. 44. 404. 1004. 2004. 4004.

\* 200 sps bandwidth aved instead of 1000 sps.

OUTPUT NOISE DENSITY, DEFENSE ELECTRONICS TMR-2A

Freguency	En Noise Output Noise in 2000s BW (m:11:rotts)	£4 (200)	En Output Noise in 2000ps BN (A:11:rofts)	£, 1200 (db)	Cutput Naice, is 200cm BW (m. 11:04s)	£4 (200)	En Noise Output Noise in 2004s BW (m://inoffs)	En 7200 (db)
	No Signal Aesent (1103e Only)	I Aesont 2ny)	(%)	91° 0 = 2(N/5)	(%)	9pE = 7(%)	(%)	4P9=(1%)
11/4.	230	-35.9	150	-39.2	56	- 435	98	- 52.0
216								
460	-	_						
91.								>
101.		<del>, , , , , , , , , , , , , , , , , , , </del>					26	-52.0
Zok	- (	<b>-</b>	<b>&gt;</b> [	-	<b>~</b> ∂	<b>-</b> ;	0 ;	-51.1
404	230	-35.9	/50	-39.2	95	- 43.5	44	- 50.1
708	061	-37.7	0#/	- 40.1	00/	-43.0	3	146.6
1001c	150	-37.2	140	-40.1	0//	- 42.1	70	-46.0
2007.	001	-43.0	041	1.04-	130	- 40.7	0//	-42.1
300k.	70	-16.0	00/	-43.0	00/	-43.0	98	-44.3
4004	50	-49.1	56	-180	56	-48.0	46	49.6
	(5/4)	9°6 = (NS)	(%s)	9P51=7(1/5)	(%)	(5/N)c= 20		
1/4.	6.0	579-	7.0	- 86.0	0.5	1.68-		
275	<b>-</b>	->	0.7	-0%	0.5	-89.1		
44	6.0	-67.5	/'	- 82.1	0.65	-86.8		
38	7.5	- 65.5	7.7	- 75.9	7.3	-80.7		
70/	8.0	-64.9	2.5	- 74.9	9./	- 79.2		
20t.	13.0	-60.7	5.5	-682	3.2	-72.8		
40k.	77.0	- 55.9	0.0/	-63.0	<b>i</b> .s	-66.7		
Bot.	44.0	-50.2	21.0	-56.5	/3.0	-60.7		
100k	50.0	1.64-	26.0	-54.9	16.0	-5% 2		
200kc	82.0	-44.7	40.0	-51.1	25,0	-54.9		
3004	64.0	-46.9	30.0	-53.6	20.0	-57.1		
400kc	30.0	-53.6	0.,,	-62.2	6.5	-65.7	,	



TRANSMITTER/RECEIVER TOTAL HARMONIC DISTORTION TEST FIGURE 11-2, 6-11

# FOSTER-SEELEY DETECTOR, 3 KC FUNDAMENTAL FREQUENCY

DetectorFoster-SealeDate 9 October 64 Originator 41. Bishep Serial No. 283 Serial 110. Mfg. Neme-Clarifodel 1455A Model 121D Mg. EMR Transmitter: Receiver:

Fundamental Frequency 3 kc

Deviation	Transmittor Input Level	Fund.	Second Harmonic	Third Harmonic	Fourth Harmonic	Fifth Harmonic	Total Harmonië Distortion
±25 kc	0, 210V rm	1.0V	1. 85 mv	1. 65 mv		•	0.248%
<b>±50 kc</b>	0.415V rms	1.0V	2. 5 mv	1. 70 mv		•	0.302%
±75 kc	0.628V rms	1. 0V	3.4 mv	2. 1 mv			0. 400%
≯100 kc	0.832V rms	1.0V	4. 9 mv	3.0 mv			0.575%
±125 kc	1.05V rms	1, 0V	7.0 mv	4.6 mv	0.46 mv	•	0.839%
±150 kc	1. 25V rms	1. 0V	10.5 mv	7. 3 mv	0.60 mv	0. 64 mv	1. 282%
±175 kc	1.46V rms	1.0V	17.0 mv	.11.0 mv	1.0 mv	1. 1 mv	2.030%
±200 kc	1.66V rms	1. 0V	24. 5 mv	16. 5 mv	1.75 mv	1. 7 mv	2. 954%

TOTAL HARMONIC DISTORTION DATA, NEMS-CLARKE 1455A, FOSTER-SEELEY DETECTOR, 30 KC FUNDAMENTAL FREQUENCY TABLE 11-2, 6-13

Serial No. 922 Model 121D Mg. EMR Transmitter:

Mfg. Nema-Clary Model 1455A Serial No. 283

Receiver:

Detector Foster-Seeldinte 9 October 64

Originator W.

Fundamental Frequency 30 kc

Deviation	Transmitter Input Level	Fund.	Second Harmonic	Third Harmonic	Fourth Harmonic	Fifth Harmonic	Intel Harmonic Distortion
±25 kc	0. 212V rms	1. 0V rms	0.8 mv	2.0 mv			0. 215%
±50 kc	0.420V rme	1. 0V rms	3. 1 mv	2. 9 mv		0 0 0	0.424%
±75 kc	0. 635V rms	1.0V rms	6.0 mv	8.0 mv	6 6 8	1 1 1	1. 000%
±100 kc	0.840V rms	1.0V rms	7.0 mv	15.0 mv	1.0 mv	1. 4 mv	1.664%
±125 kc	1.05V rms.	1.0V rms	9. 1 mv	24. 5 mv	1.6 mv	3. 1 mv	2. 637%
*150 kc	1. 26V rms	1.6V rms	13, 5 mv	36.0 mv	2. 7 mv	6.3 mc	3. 905%
±175 kc	1.47V rms	1.0V rms	17.0 mv	52. 0 mv	3. 2 mv	11.0 mv	5. 589%
±200 kc	1.68V rms	1.0V rms	21.0 mv	70.0 mv	3, 6 mv	17. 5 mv	7. 532%
						The state of the s	

# FOSTER-SEELEY DETECTOR, 70 KC FUNDAMENTAL FREQUENCY IOIAL MAKMUNIC DISTORTION DATA, NEMS-CLARKE 1455A

)

Detector oster-Seele Date 9 Octuber 64 Originator While Les Sorial No. 283 Serial No. MgNems-Clarke Model 1455A Model 121D MIR. EMR Transmitter: Receiver:

Fundamental Frequency 70 kc

***************************************	·					i		
Deviation	Transmitter Input Level	Fund.	Second	Third	Fourth Harinonic	Fifth Harmonic	Total Harmonic Distortion	
±25 kc	0.207V rms	l, OV rms	3.2 mv	l. 6 mv	•	1	0.358%	
±50 kc	0.420V rms	l. OV rms	5.6 mv	9.8 mv	0.7 mv		1.131%	
±75 kc	0.620V rms	1.0V rms	8.0 mv	21.0 mv	1.7 mv	1.6 mv	2 259%	
±100 kc	0.840V rms	1.0V rm	10.0 mv	37.0 mv	3, 5 mv	5.7 mv	3.891%	
±125 kc	1.03V rms	1.0V rms	12.5 mv	49. 0 mv	5.0 mv	10.0 mv	5. 179%	
±150 kc	1.25V rms	1.0V rms	17.0 mv	65.0 mv	8.0 mv	19.0 mv	7. 028%	
±175 kc	1.45V rms	1.0V rms	15, 5 mv	80.0 mv	9. 2 mv	29.0 mv	8. 698%	
±200 kc	1.65V rms	1.0V rms	8. 5. mv	94. 0 mv	9.4 mv	40.0 mv	10. 294%	

# TOTAL HARMONIC DISTORTION DATA, NEMS-CLARKE 1455A FOSTER-SEELEY DETECTOR, 100 KC FUNDAMENTAL FREQUENCY TABLE II-2, 6-15

7

Originator Lander Serial No. 922 Model 121D MIR. EMR Transmitter:

Mfg.Nems-Clarke Model 1455A Serial No. 283

Receiver:

Detectorf oster-SeeleDate 9 October 64

Fundamental Frequency 100 kc

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Deviation	Transmitter Input Level	Fund.	Second	Third Harmonic	Fourth	Fifth Harmonic	Total Harmonic Distortion
±25 kc	0.218V rms	1.0V rms	6.6 mv	3.6 mv	1		0. 752%
≠50 kc	0.441V rms	1.0V rms	10.0 mv	15.0 mv	0.54 m	0. 58 mv	1.805%
±75 kc	0, 650V rms	1.0V rms	12, 5 mv	31.0 mv	1.60 mv	1. 50 mv	3.350%
±100 kc	0.865V rms	1.0V rms	30.0 mv	49.0 mc	5.2 mv	3.6 mv	5.780%
±125 kc	1.09V rms	1: 0V rms	50, 0 mv	57: 0 mv	13. 0 mv	5.8 mv	7,715%
±150 kc	1: 32V rms	1: 0V rms	35:0 mv	80: 0 mv	17: 0 mv	11.5 mv	8, 970%
±175 kc	l: 53V rms	1: 0V rms	30.0 mv	96. 0 mv	24: 5 mv	19, 5 mv	10.534%
±200 kc	i. 76V rms	1.0V rms	24.0 mv	105.0 mv	31.0 mv	29, 0 mv	11.577%

# FOSTER-SEELEY DETECTOR, 225 KC FUNDAMENTAL FREQUENCY TOTAL HARMONIC DISTORTION DATA, NEMS-CLARKE 1455A

Serial No. 922 Model 121D MIR. EMR Transmitter:

Originator Who

Mfg. Nems-Clark Model 1455A

Receiver:

Serial No. 283

DetectorFoster-Seele pate 9 October 64

Fundamental Frequency 225 kc

 Deviation	Transmitter	Ĺ	Second	Third	Fourth	Fifth	Total Harmonic
					Harmonic	narmonic	Distortion
 ±25 kc	0.286V rms	1.0V rms	9. 1 mv	1. 1 mv	1 1		0.917%
 ±50 kc	0.558V rms	1.0V rms	17.5 inv	2. 75 mv	8 6 8	•	1.771%
 ±75 kc	0.850V rms	l. 0V rms	25.0 mv	6.8 niv			2. 591%
+100 kc	1.14V rms	1. 0V rms	28.5 mv	11.0 mv	6.8 mv	•	3. 130%
±125 kc	1.48V rms	1.0V rms	32.0 mv	17.5 mv	13.0 mv	0. 42 mv	3.872%
±150 kc	1.88V rms	1.0V rms	44.0 mv	25. 5 mv	2.45 mv	0. 72 mv	5. 092%
±175 kc	2.35V rms	1.0V rms	70.0 mv	34.0 mv	4. 5 mv	1. 35 mv	7.796%
±200 kc	2. 93V rms	1.0V rms	76.0 mv	43.0 mv	6.8 mv	1.80 mv	8. 760%

TOTAL HARMONIC DISTORTION DATA, NEMS-CLAPKE 1455A, PHASE LOCK DETECTOR, 3 KC FUNDAMENTAL FREQUENCY TABLE II-2, 6-17

Serial No. 922 Model 121D MG. EMR Transmitter:

Originator W. Brene

Mis. Nema-Clark Model 1455A

Receiver:

Serial No.

Delector Phase Lock Date 9 October 6

3 kc Fundamental Frequency\_

Deviation	Transmittor Input Level	Fund.	Second	Third Harmonic	Fourth Harmonic	Fifth Harmonic	Total Harmonic Distortion
±25 kc	0.210V rm	1.0V	1.30 mv	1.72 mv	,	1	0.216%
±50 kc	0.415V rm	1. 0V	1.9 mv	2.2 mv			0, 291%
±75 kc	0.628V rm	1. 0V	2.5 mv	3, 2 mv	0.64 mv		0.411%
±100 kc	0.832V rm	1. 0V	e. 7 mv	4.4 mv	1.2 mv	•	0.530%
±125 kc	1.05V rms	1. 0V	2.8 mv	5.6 mv	2. 1 mv	:	0.660%
±150 kc	1.25V rms	1. 0V	3.8 mv	7, 3 mv.	2.4 mv	0. 9 mv	0.862%
±175 kc	1.46V rms	1, 0V	7.4 mv	9.8 mv	3.0 mv	1.6 mv	1.274%
±200 kc	1.66V rms	1. 0V	13. 5 mv	13.0 mv	2.75 mv	2. 50 mv	1. 911%

# IUIAL HAKMUNIC DISTURTION DATA, NEMS-CLARKE 1455A, PHASE LOCK DETECTOR, 30 KC FUNDAMENTAL FREQUENCY

Serial No. Model 121D Mfg. EMR Transmitter:

MfgNems-Clarke Model 1455A Serial No.

Receiver:

Serial No. 283 Det

Detector Phase Luck Date 9 October 64

Originator 11/2

Fundamental Frequency 30 kc

						•	
Transmitter Deviation Input Level Fund.	Transmitter Input Level Fund.	五	Second Harmonic	Third Harmonic	Fourth Harmonic	Fifth Harmonic	Total Harmonic Distortion
#25 kc 0.212V rms 1.0V rms 3	1.0V rms		3. 1 mv	3. 1 mv		•	0. 438%
±50 kc 0.420V rms 1.0V rms	1.0V rms		5. 4 mv	3. 2 mv	1.0 mv	0.8 mv	0.641%
±75 kc 0.635V rms 1.0V rms	1.0V rms		7. 5 mv	7.8 mv	1. 1 mv	0.9 mv	1.091%
±100 kc 0.840V rms 1.0V rms 9	1.0V rms		9.5 mv	13.0 mv	3.0 mv	1.5 mv	1.645%
#125 kc   1.05V rms   1.0V rms	1.0V rms		11.0 mv	21. 5 mv	4.9 mv	2. 1 mv	2.473% .
±150 kc   1.26V rms   1.0V rms	1. 0V rms		14. 5 mv	32.0 mv	6. 9 mv	3.6 mv	3. 598%
±175 kc   1.47 v rms   1.0 v rms	1.0V rm		17.5 mv	46.0 mv	6.0 mv	7. 5 mv	5.014%
±200 kc   1.68V rms   1.0V rms	1.0V rm		22. 0 mv	64. 0 mv	3. 8 mv	12. 0 mv	6. 884%

TABLE 11-2, 6-19
TOTAL HARMONIC DISTORTION DATA, NEMS-CLARKE 1455A, PHASE LOCK DETECTOR, 70 KC FUNDAMFNTAL FREQUENCY

Originator 14 Bis Hop 922 Serial No. Model 121D MIR. EMR Transmitter:

Detector Phase Lock Date 19 October 64 283 Serial No. Mfg. Nems-Clark-Model 1455A.

Receiver:

Fundamental Frequency 70 kc

Deviation	Transmitter Input Level	Fund.	Second	Third	Fourth	Fifth Harmonic	Total Harmonic Distortion
±25 kc	0.207V rms	1.0V rms	5.0 mv	1.6 mv	0.9 mv		0.533%
±50 kc	0.420V rms	l. 0V rms	8.0 mv	3. 6 mv	2.2 mv	0, 55 mv	0. 906%
±75, kc	0.620V rms	1.0V rms	12.5 mv	8.2	1.0 mv		1.498%
±100 kc	0,840V rms	l. 0V rms	16.5 mv	11,5 m	l. 3 mv	0.5 mv	2. 016%
±175 kc	1.03V rms	1.0V rms	22. 0 mv	12.0 mv	1. 9 mv	•	2. 513%
. ±150 kc	1.25V rms	1.0V rms	51.0 mv	16.0 mv	7.4 mv	1. 2 mv	5. 397%
±175 kc	1.45V rms	1.0V rms	125.0 mv	51.0 mv	4.8 mv	4.8 mv	13.517%
±200 kc	1. ó5V rms	1.0V rms	610.0 mv	100, 0 mv	75.0 mv	45.0 mv	62.430%

# PHASE LCCK DETECTOR, 100 KC FUNDAMENTAL FREQUENCY TOTAL HARMONIC DISTORTION DATA, NEMS-CLARKE 1455A,

Originator W. Bis ... Serial No. Mfg. EMP Model 121D Transmitter: Receiver:

Serial No. 283 Mg Nems-Clarke Model 1455A

Detector Phase Lock Date 9 October 64

Fundamental Frequency 100 kc

Deviation	Transmitter Input Level	Fund.	Second	Fhird Harmonic	Fourth	Fifth Harmonic	Total Harmonic Distortion
	0.218V rms	1.0V rms	1.8 mv	1. 45 ու	0, 52 ուv	0. 5 mv	0. 242%
±50 kc	0.441V rms	l. 0V rms	5.6 mv	2. 7 mv	0. 44 mv	0.54 mv	0. 626%
±75 kc	0.650V rms	i. OV rms	24. 5 mv	2.75 mv	0.84 mv	0.88 mv	2. 468%
:100 kc	0. 865V rms	l.OV rms	32.0 mv	75.0 mv	2. 4 mv	1. 2 mv	8. 159%
±125 kc	1.09V rms	1.0V rms	50, 0 mv	56.0 mv	9.5 mv	7. 9 mv	7. 608%
±150 kc	1. 32V rms.	l. OV rms	Inoperativ				
±175 kc	1, 53V rms	l. 0V rms	Inoperative	<b>ပ</b>			
±200 kc	1.76V rms	l.OV rms	Inoperative	ა			

# PHASE LOCK DETECTOR, 225 KC FUNDAMENTAL FREQUENCY TOTAL HALMONIC DISTORTION DATA, NEMS-CLARKE 1455A, **TABLE II-2, 6-21**

Serial No. 922 Mfg. EMR Model 121D Transmitter:

Originator de. P. 11.19

Receiver:

Mg. Nems-Clark Model 1455A

Serial No. 283

Detector Phase Lock Date 9 Cctober 64

Fundamental Frequency 225 kc

Deviation	Transmitter Input Level	Fund.	Second Harmonic	Third Harmonic	Fourth Harmonic	Fifth Harmonic	Total Itarmonic Distortion
 +25 kc	0.286V rms	1.0V rms	4.5 mv	1. 7 աv	•		0.481%
 ±50 kc	0.558V rms	l. 0V rms	5.6 my	1. 2 mv	8 8	0.6 mv	0.576%
±75 kc	0.850V rms	l. 0V rms	14. 0 mv	5.8 mv	1.0 mv	0. 5 mv	1.520%
±100 kc	i. 14V rms	1. 0V rms	30.0 mv	9. 6 mv	1.0 mv	0. 72 mv	3.152%
±125 kc	1.48V rms	1.0V rms	41.0 mv	13. 2 mv	2. 4 mv	0. 62 inv	4.314%
 ±150 kc	1.88V rms	1.0V rms	42.0 mv	17.5 mv	4.0 mv	0. 72 mv	4.568%
 ±175 kc	2. 35V rms	1.0V rms	46.0 mv	20. 5.mv	5.0 mv	1. 05 mv	5. 062%
±200 kc	2. 93V rms	1.0V rms	51.0 mv	22. 5 mv	5.8 mv	1. 30 mv	5. 606%

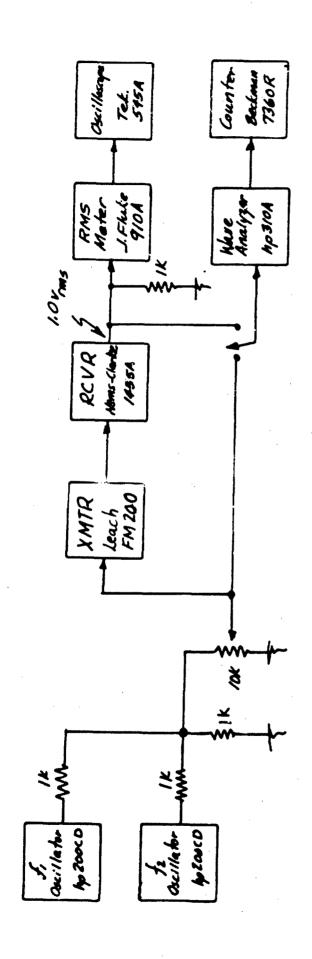


FIGURE II-2. 6-22 DIFFERENCE FREQUENCY INTERMODULATION TEST, LEACH FM 200 AND NEMS-CLARKE 1455A

### TABLE II-2.6-23 DIFFERENCE FREQUENCY INTERMODULATION DATA, LEACH FM 200 AND NEMS-CLARKE 1455A

Modulating Frequency Lc	Transmitter Injust Vrms	Peak Deviation Kc	Receiver Output Frequency kc	Receiver Output Level mr <sub>rms</sub>	Percentage Intermed.
70.0 52.5	1.35°	200 150	70.0	775	1.55%
70.0 52.5	1.62	180 135	70.0 17.5	775 6.6	0.85%
70.0 52.5	1.44	160 120	70.0 17.5	790 77	0.98%
70.0 52.5	1.26	140	70.0 17.5	785 10.7	1.36%
70.0 52.5	1.08 0.81	120 90	70.0 17.5	790	1.45%
70.0 52.5	0.90 0.68	100 75	70.0 17.5	805 10.8	1.34%
70.0 52.5	0.72 0.54	80	70.0 17.5	790 9.7	1.23%
70.0 52.5	0.54	60 45	70.0	790 8.0	1.05%
70.0 52.5	0.36	40 30	70.0	795 5.6	0.70 %
7 0.0 52.5	0.18	20 15	70.0 17.5	795 <sup>-</sup> 2.8	0.35%

### TABLE II-2.6-24 DIFFERENCE FREQUENCY INTERMODULATION DATA, LEACH FM 200 AND NEMS-CLARKE 1455A

Modulating Frequency Kc	Transmitter Input Vrms	Peak Deviation &c	Receiver Output Frequency Kc	Receiver Output Level mrms	Percentage Intermol.
124 93	2.0 1.5	200	124	720 66	9.15%
124	1.8 1.4	180 135	124	730 35	4.80%
124	1.6	160	124	730 25	3.43%
124 93	).4 ).0	140	124	750 21	2.80%
124 93	1.2 0.90	120 90	124 31	745 <sup>-</sup> 18.4	2.47%
93	1.0 0.75	100 75	124 31	755 15.5	2.06%
124 93	0.80 0.60	80 60	124	760 12.8	1.68%
93	0.60	45°	31	760	1.32 %
93	0.40	40 30	3/	760	0.86%
124 93	0.20	20 15	124 31	770 3.0	0.39%

#### 2.7 GROUP DETRANSLATOR

#### 2.7.1 General

The EMR Model 259 Group Frequency Detranslator accepts a multiplex of FM subcarriers in the range between 5 kc and 1100 kc, and using a reference signal appearing at the input along with the data subcarriers, detranslates the multiplex into groups of multiplexed subcarriers suitable for direct application to subcarrier discriminators.

The Model 259 uses the reference signal in the input multiplex to synthesize the frequencies required to detranslate the respective subcarrier groups. Each group which is to be detranslated is selected from the input multiplex by a group band-pass filter. The separated group of subcarriers and its corresponding reference frequency are applied to a balanced modulator which drives an output amplifier which is, in turn, suitable for driving a bank of discriminators. The output signal represents the selected group of subcarriers translated down in frequency to the spectrum occupied by the lowest frequency group.

The Model 259 contains a delay line to equalize the envelope delay of the input multiplex and the envelope delay of the reference frequency so that tape-speed errors will be essentially the same in the translated channels as in the untranslated ones. Vernier adjustment of this equalization is provided for each detranslated group. The outputs of all groups are time correlated so that tape-speed compensation may be used without external delay lines. Since the deviation bandwidths of all data discriminators are equal, the data outputs are also time correlated.

Normally, one bank of discriminators is used for each group. For applications where only one bank of discriminators is used on a time-sharing basis, as was the case in the baseband evaluation, a switch on the front panel of the Model 259 makes possible the connection of the discriminator bank to any group output. A calibrate-operate switch is also provided. With this switch in the calibration position, all discriminator banks are connected to the output of the lowest-frequency group selector, thus enabling calibration of all discriminators with the calibration signals available from an EMR Model 260 Modular Three-Point Calibrator.

Section 1.5 of Volume I contains the constant-bandwidth system used in the base-band evaluation.

#### 2.7.2 Specifications

A detailed evaluation of the EMR 289 Modular Group Frequency Detranslator used in the constant bandwidth system was not undertaken as part of the study contract. Operation within specification was, however, certified by other EMR personnel. A summary of specifications is included below.

Subcarrier Frequencies: A multiplex of FM subcarrier frequencies in the range from 5 kc to 1100 kc is converted into groups of subcarriers suitable for direct application to subcarrier discriminators.

Data Time Correlation: Data channel time errors contributed by the Model 259 Group Frequency Detranslator are less than  $\pm 1^{\circ}$  from the BSL delay for standard EMR systems at a deviation ratio of 2 or greater.

Multiplex Input Voltage: 10 volts peak-to-peak maximum. Normal level of each individual subcarrier is 100 my rms.

Multiplex Input Impedance: 10,000 ohms

Reference Input: 10 millivolts to 1 volt rms from a compatible EMR reference discriminator with constant-bandwidth reference channel selector (for example, Model 210A with 210T-03, Model 267R-03, or Model 270A with 270T-03). The normal reference input to the Model 259 is 100 millivolts rms. The level of the reference in the multiplex should be 6 db above the level of the subcarrier with with highest amplitude.

Group Outputs: (Specification applies to each output.)

Voltage:

10 volts peak-to-peak maximum (open circuit)

Current:

30 ma maximum

Impedance:

91 ohms

Stability:

If the output current does not exceed 30 ma, no instability will result from any capacitive load. An output overload or short circuit

will not damage the unit.

Gain: Adjusted at the factory to 6 db  $\pm$  1 db to each subcarrier.

Intermodulation Distortion: Each intermodulation distortion product, at normal input level, is less than 0.5% of the amplitude of any subcarrier.

Subcarrier Feedthrough: For flat subcarrier emphasis, lower-group subcarriers in the detranslated group outputs are suppressed at least 46 db.

Image Rejection: For flat subcarrier emphasis, images of undesired groups which appear in the desired group are suppressed at least 46 db.

#### 2.8 SUBCARRIER DISCRIMINATOR

No separate equipment evaluation was performed on the EMR 210 Subcarrier Discriminators. Before use in the baseband evaluation, each unit was returned to the EMR manufacturing test department and retested to certify operation within specification. A summary of performance characteristics pertinent to the baseband evaluation is presented in Volume I, Section 2.8.

#### 2.9 TAPE RECORDER

#### 2.9.1 Amplitude Response

Amplitude response data on the Mincom G-107 and Ampex FR 1400 Tape Recorders were obtained using the following procedure:

- a. Clean and degauss the heads using the Magneraser hand degausser on the G-107 heads and the Ampex Model 111 bulk degausser on the removable Ampex heads.
- b. Degauss the tape with the bulk degausser.
- c. Apply 1.0 volt rms to the input and adjust the input level control until the monitor meter indicates 0.0 db. This provides normal record level to the recorder heads. The Ampex FR 1400 input level attenuator has been preset and locked (by the manufacturer's representative) so that a 1.0 volt rms input provides normal record level.
- d. With the recorder operating, adjust the output attenuator for 0.0 db on the 1.0 volt rms range of the voltmeter (use high damping) with a 1.0 volt rms, 1000 cps, input applied.
- e. Sweep the oscillator as required to obtain the frequency response characteristic, taking care to assure a 1.0 volt rms input signal at each measured frequency.
- f. Repeat for each track of the recorder.

The measured data is contained in Tables II-2.9-1 and II-2.9-2 and is presented graphically in Figures I-2.9-1 and I-2.9-2 of Volume I. Because of recall of the tape recorders by the manufacturers, a second Ampex FR 1400 tape recorder was borrowed in-house for use with the constant-bandwidth evaluation. This machine contained 500-kc electronics, modified by Ampex to extend to 600 kc, and was capable of operation only at 120 ips. Only its frequency response was measured (Table II-2.9-14).

#### 2.9.2 Phase Response

Tape recorder phase response was measured using equipment as shown in the block diagram, Figure II-2.9-3. The procedure used is as follows:

- a. Degauss tape, heads, and transport mechanisms.
- b. Set the oscillator frequency so that the last flip-flop in the string generates a square wave in the neighborhood of recorder low-frequency cutoff.
- c. Use the lower frequency square wave as  $f_1$  and the next higher as  $f_2$  ( $f_2$  will be second harmonic of  $f_1$ ).
- d. Set Khron-Hite low-frequency cutoff to 20 cps, and high-frequency cutoff to the fundamental frequency of its input square wave.
- e. Observe summation of two sinusoids at "A" on one trace of a dual-trace oscilloscope.
- f. Place delay line in f<sub>1</sub> path and, with recorder operating in record/reproduce mode, observe recorder cutput on second trace of oscilloscope.
- g. Operate the oscilloscope on alternate trace mode and trigger the oscilloscope internally so that the trace starts at the same input voltage level on each sweep.
- h. Adjust the delay through the delay line so that the waveforms at A and B are identical. Display both traces superimposed on oscilloscope, to assure best possible alignment of waveshape, and photograph.
- i. Move flip-flop outputs up one flip-flop each and repeat, producing harmonic combinations across as much of recorder bandwidth as practical.

The high-frequency cutoff of the Khron-Hite filters is 200 kc. Also, the minimum step adjustment of the delay line is 1 usec. Therefore, no data was taken at frequencies higher than 200 kc. Measured data is presented in Table II-2.9-4. A typical photograph is shown in Figure II-2.9-5. Volume I, Figure I-2.9-3 presents the data graphically.

#### 2. 9. 3 Noise Density

Output noise density as a function of frequency position in the band was measured on each of the two tape recorders as shown at the bottom of Table II-2.9-6. The

#### following procedure was used:

- a. Degauss heads, tape, and transport mechanism.
- b. Apply a 1.0 volt rms 1000 cps sine wave to the recorder input. For the G-107, adjust the input for 0.0 db on the input meter yielding normal record level. The FR 1400 is preadjusted and locked so that 1.0 volt rms input is normal record level.
- c. Operate the recorder in record/reproduce mode at 60 ips.
- d. With the Hewlett-Packard 310A set for 200 cps bandwidth, measure the recorder output noise as a function of frequency, being careful to avoid 1000 cps and its harmonics.
- e. As a check, disconnect the analyzer input and measure its residual noise level in 200 cps bandwidth position.

The data is contained in Tables II-2.9-6 and II-2.9-7 and presented graphically in Figure I-2.9-4.

#### 2.9.4 Intermodulation

Intermodulation tests were made using the technique outlined in the block diagram of Figure II-2. 9-8. Both sum and difference intermodulation products were measured; the measure data is tabulated in Table II-2. 9-9 and presented graphically in Figure I-2. 5 of Volume I.

#### 2.9.5 Total Harmonic Distortion

Using equipment as described in Table II-2.9-10, total harmonic distortion was measured on the two tape recorders using the following procedure:

- a. Degauss tape, heads, and transport mechanism.
- b. Apply an input signal of 1.0 volt rms and 1000 cps and adjust input and output attenuators as necessary to operate recorder at normal record level.
- c. Operate the tape recorder at 60 ips in record/reproduce mode.
- d. Maintaining 1.0 volt rms input and output level, adjust the oscillator frequency across the band of the recorder.

- e. At each input frequency, measure the harmonic content of the recorder output with the frequency-selective voltmeter operating with a 200 cps bandwidth.
- f. Combine the rms voltage measure of each harmonic in rms fashion to obtain the total harmonic distortion.

The measured data is given in Tables II-2. 9-10 and II-2. 9-11 and presented graphically in Figure I-2. 9-6 of Volume I.

#### 2.9.6 Crosstalk

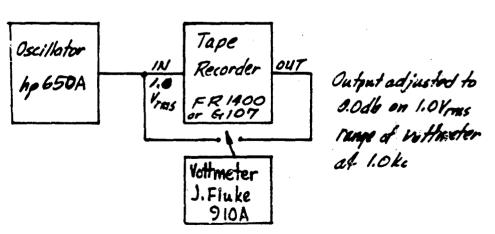
Using equipment as described at the bottom of Table II-2.9-12, crosstalk between channels was measured on the two tape recorders using the following procedure:

- a. Repeat instructions a. through d. of section 2.9.5, above, establishing normal record conditions.
- b. At each input frequency, measure the output of the channel containing the input frequency and the two higher-numbered and two lower-numbered channels. (This measures the channels on adjacent tape tracks and those on adjacent head positions.)

The measured data is given in Tables II-2. 9-12 and II-2. 9-13.

TABLE II-2.9-1
FREQUENCY RESPONSE TEST
AMPEX FR 1400 TRACK NO. 2, ELECTRONICS NO. 1 AND NO. 2

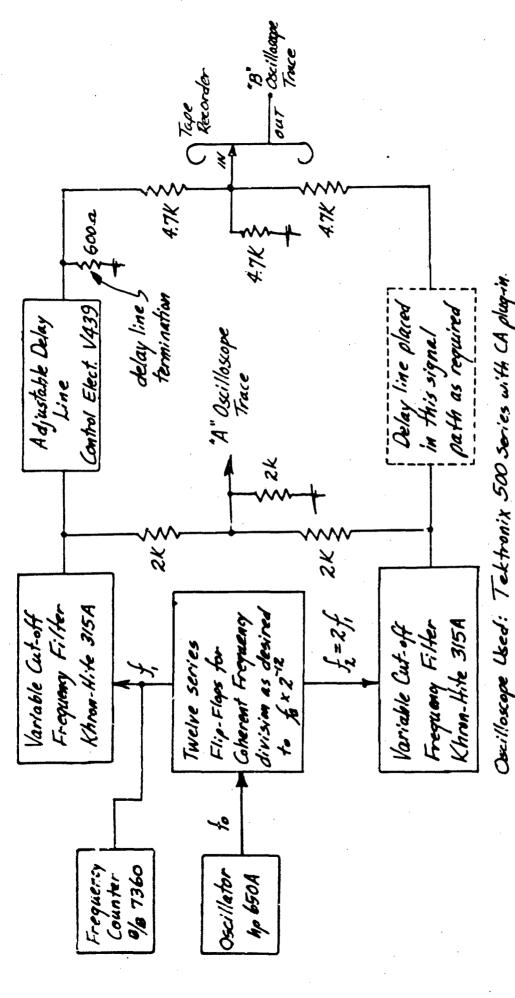
	onics l ick 2	1	onics 1 ck 2		ronics 2 ack 2	i	onics 2 ck 2
Freq.	Relative Output db	Freq.	Relative Output db	Freq.	Relative Output db	Freq.	Relative Output db
252	-6.0	cps 80kc		cps 230	-6.0	cps /Okc	
310	- 3.0	100k	• - •	275	-3.0	20kc	+0.2
329	-2.7	160kc	+1.7 PEAK	300	-2.0	40k	+0.4
350	-30	200kc	+1.6	332	-1.6	70k	+1.0
429	-3.7 min	300kc	+1.2	421	-2.6	100kc	
500	-1.9	400tc	+0.8	479	-1.0	137kc	+1.8 PEAR
700	-0.9	450kc	+0.6	556	O. OEAK	200kc	+1.6
1.0kc	0.0	500 kc	+0.6	670	-0.5 MIN	300k	+1.2
1.5kc	+0.3	550kc	+0.3	789	+0.2 MAK	400kc	+0.9
3.0kc	+0.1	600tc	-0.6	1.0kc	0.0	500kc	+0.2
7.0kc	0.0	670kc	-2.0	2.0kc	+0.6	600tc	-0.4
10 kc	0.0	715k	-3.0	3.0kc	+0.6	7/4-kc	-3.0
20 kc	-0.2	800kc	-6.0	4.0kc	+0.4	808 kc	-6.0
40 kc	+0.2			7.0kc	+0.4		



BLOCK DIAGRAM TAPE RECORDER FREQUENCY RESPONSE

TABLE II-2.9-2 FREQUENCY RESPONSE TEST, MINCOM G-107

Channel	One	Channel	Three	Channel	Four	Channel	Two
Input	Output	Input	Output	Input	Output	Input	Output
Freq	Level	Freq	Level	Freq	Level	Freq	Level
82 cps	-6.0 db	87cps	-6.0 db	90cps	-6.0 db	90 cps	-6.0db
120 cps	-4.216	152 cps	-3.0 db	168 cps	-3.0db	165 cps	-3.0 db
181 cps	-3.0 db	300 cps	- 1.4 db	209 cps	-2.0 db	300 cps	-1.3 db
398cps	-1.096	500cps	-1.2 16	270 cps	-1.0 db	535 cps	-1.0 db
500 cps	-0.8 99	800 cps	-1.046	600 cps	-0.849	800 cps	-0.846
600 cps	-0.8 46	850 cps	-0.8 db	800cps	-0.899	1.0 KC	0.0 db
800 cps	-0.811	900 cps	-0.6db	900cps	-0.636	1.2 KC	+0.986
900cps	-0.546	t .	0.099			2.0 KC	+1.2 db
1	0.046		+0.846		_	_	+1.3 16
1.2 KC		1.33 KC	min. Pr	6.0 KC		5.5 KC	
2.0 KC	. Tenk		+0.5 db	_	+1.2 db	10 KC	+1.1 db
6.0 KC		2.46 KC		12 KC	1	20 KC	+0.6db
23 kc		5.0 KC	1		+0.7 46	40 KC	+0.1 db
50 KC	-0.4 db	8.0 xc	1	40 KC	+0.1 46		-0.1 db
110 kc	-0.6 db	12 KC	+0.8 99	60 KC	0.0 46	80 KC	-0.2 16
	-1.0 db		min et.		1		
	0.0 db				ľ		
	-1.0 db		1		•		!
	-2.0 db				L L		i
	-3.0 db		*	305 KC	-6.0 db	278 kc	-3.0db
340 kc	-6.0db	300 KC	-0.8db			310 KC	db 0.0-
	Į.	306 KC		•			
	ì	326 Kc					**************************************
		346 KC.					
		350 kc.	-6.8 46				

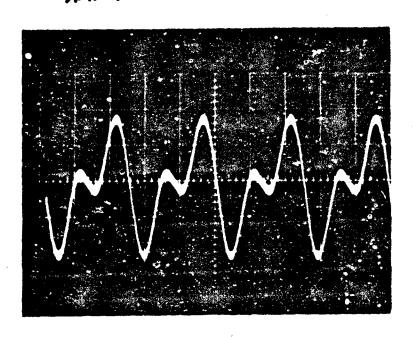


TAPE RECORDER TIME-DELAY AND PHASE-RESPONSE TEST FIGURE 11-2, 9-3

#### TAPE RECORDER TIME-DELAY AND PHASE-RESPONSE DATA

Undekyed Fregnomy	Delayed Frequency	Delay Masured	Cumulative Dotou	Phase Shift
Mincom G107:		Je.sec	,	,
32 kc	16kc	0	0	0
16 Kz	8kc	2.0	Z	5.8°
8te	4ke	6	8	11.5
4ke	2 kc	20	28	202°
24	1 kc	85	113	40.7°
/kc	500cps	270	383	69.0°
5000	250cps	740	1143	127.0
Ampex FR 1400				
64kc	32kc	0	0	•
32 kc	16kc	/	1	5,8°
16kc	8kc	0	/	2.90
8kc	4kc	7	8	11.5°
4kc	Zkc	22	<i>30</i>	21.6
2 kc	1 kc	100	130	46.80
1kc	500098	400	<i>530</i>	95.4

#### MISEX FRIADE L- 2- JL



 $f_i = 2kc$  22 uses of delay to 2kc  $f_i = 4kc$ 

Use of oscilloscope internal trigger and alternate trace features allows trace A, before delay line and tape recorder, und trace B, recorder output, to be superimposed and held steady for nulling.

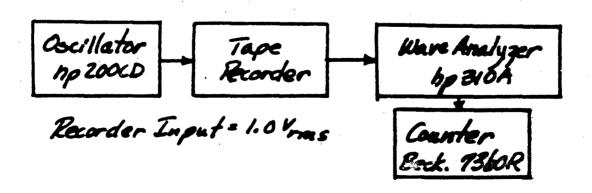
FIGURE II-2.9-5

TYPICAL OUTPUT PHOTOGRAPH TAPE RECORDER

TIME-DELAY AND PHASE-RESPONSE TEST

#### NOISE TEST - MINCOM GIOT

Franco	Lere!	Residual	Level	db, Relative
Frequency	Au	Roading	√200	4 1.0 V.
400	4000	20.0	203	-71.0
2.4kc	2000	1	142	-77.0
5.0kc	500		35.4	-89.0
10.0kc	250		17.6	-95.0
20.0k	200		14.2	-97.0
25.0kc	160		14.3	-98.9
40.0kc	125		8.8	-101.1
100.0k.	110		7.8	-102.2
200.0k.	150		10.6	- 99.5
300,0k.	350		24.7	-92.1
400.0kg	250		17.6	- 95.0
500.0kg	200		142	- 97.0
700.0kg	150		10.6	- 99.5
900.0kg	100	♥ -	7.1	-103.0
1000.0kc	80	20.0	5.7	-104.9



#### NOISE TEST - AMPEX FR 1400

Frequency	Leve/ mv	Rosidual Roading	<b>Leve</b> / √200	db, Rel. to 1.0 v
400cps	14	0.06mv	9.99mv	-60.0
500 cps	10		0.707mv	-63.0
2.5kc	1.7		O.IZmr	-78.4
5.5kc	0.80		57 pv	-84.9
8.0 kc	0.65		46 pv	-86.7
16.0kc	0.40		28.2 AV	-91.0
32.0k	0.25		17.7 pm	-95.0
69.0kc	0.22		15.6 UV	-96.2
128.0kc	0.22	·	15.6 pv	-96.Z
256.0 kg	0.23		16.3 pt	-95.8
512.0kg	0.32	·	22.6 pv	-92.9
1024.0k.	0.60	₩.	42.4 pv	-87.4
1.4 Mc	0.62	0.06mr	13.8 pv	-87.2

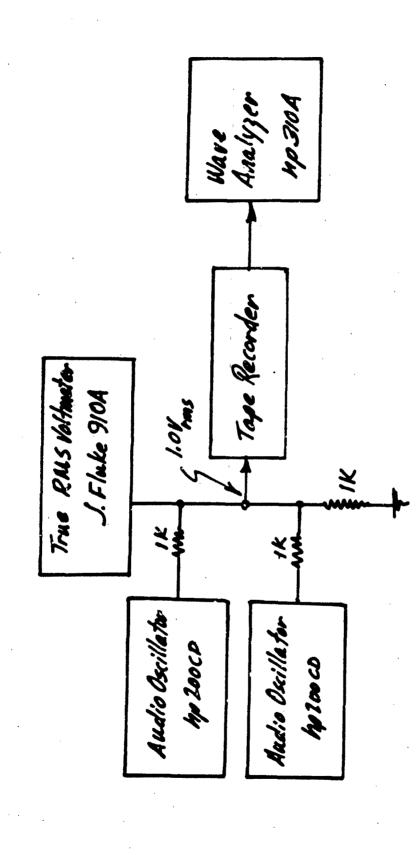


FIGURE II-2.9-8
INTERMODULATION TEST BLOCK DIAGRAM

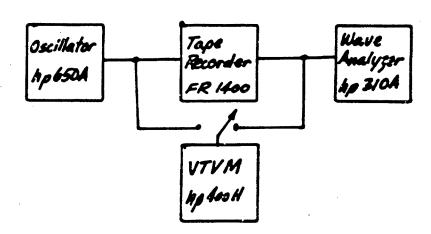
## INTERMODULATION TEST DATA

MI	incom (	G107		1	AMPEX	FR 140	00
f.	h	1,+f2	f f2	f.	f.	fith	f f2
500	600	35mz	rms	500	1k.	7.5mv	_
700	800	3.5mb	-	700	1.Kc	5mu	
1kc	2kc	3.5mv	-	1kc	2kc	5,0m	
1.4kc	2.4 kc	2.5mm	3.5mv	1.4kc	2kc	4.5m	_
Zki	3 kc	2.2mv	4.0 m	2kc	3k.	Atm	
3 kc	4 kc	1.8my	2.6 mm	3 Kc	4kc	43mv	_
4kc	5kc	1.6mv	2.0 mm	4 KC	5kc	4.3mr	_
5kc	6 Kc	1.8mr	2.0 m	5 kc	6kc	4.3mv	-
7kc	8 kc	1.8mr	2.0mv	7kc	8kc	4.3mv	-
10ke	11 kc	2.0mr	20 mv	10 kc	15kc	4.4mv	4.7mv
14kc	15 kc	1.3mr	1.5 mv	14 K	2460	5.0 ml	4.7mv
20ke	21 kc	1.4mr	1.5 mv	Zokc	30kc	5.0 my	4.8m
30kc	31 kc	1.5mr	1.5 MV	30 Kc	40kc	5.5 mv	6.7m2
40k	41 kc	1.3mr	1.3 mv	40 Kc	50k.	5.7mv	8. = mi
50k	51kc	1.4mv	1.3 mm	50 kc	bore	5.3mv	8.7mi
70kc	71kc	44mv	1.0 mV	70 kc		6.0mv	Honey
100k	101kc	~	0.60 m	100 kc		7.0mv	12mv
140kc	141kc		0.65 mV	140 K		7.0mv	6,8 m/
200Ec	201kz	_	0.90 my	200 Kc	210kg	B.Omv	15.5mV
300k	301kc		0.60 mV	300 kc	310 K	3.0mV	12.5 mv
		f, = fz am		400 kc	410Ke		14.0mv
and f.	++==1.0	Vrms, nor	mal recond	500kc	510kc		14.5m
			iere/	600 Kc	650ks		14,5mV

## TOTAL HARMONIC DISTORTION AMPEX FR 1400

Fund. *	Har	monic Leve	./	
Freq.	234	monic Leve	4 th	T.H.D.
1.0 Kc		8.0mr		0.87.
4.0kc	1.1mr	7.6mr		0.77%
10kc		7.5 mv	•	0.75%
20kc	1.0mr	10.0 mv		1.0%
40kc	1.5 mv	12.5mv		1.3%
100kc	3.4 mr	8.4 mv		0.9%
200kc	2.7mv	9.5mv	2.0mv	1.0%
400kc	3.0mv	3.0mv		0.43%

<sup>\*</sup> Fundamental Level = 1.0 Vrms input and output



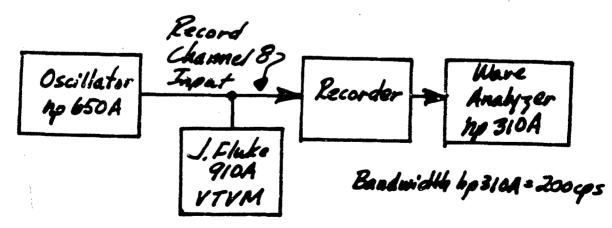
# TOTAL HARMONIC DISTORTION MINCOM GIOT

Fund. * Freq.	Hari	monic Level	
rreg.	2nd	nonic Level  3rd 4th	T.H.D.
500cps		7.0mv —	0.7%
1kc	6.0mr	7.0mr —	0.97.
4kc	5.5mv	7.0mr -	0.9%
10kc	6.0mv	7.5mv —	1.0%
40kc	7.5mr	10.mv -	1.2%
100k	4.0mv	18. mv	1.8%
250k	8.0m	5.0mr -	0.9%

<sup>\*</sup> Fundamental Level = 1.0 Vrms input & output.

### CROSSTALK - AMPEX FR 1400 Recorder Speed: 60:ps

Frequency Record Chan. 8	Record Chin.	Record Chan.	Record Chan.	Record Chan.	Record Chan,
CPS	6	7	8	9	10
	MY	mv sms	rms	Mo V Mors	MV PMS
400	28.	90.	1.0	90.	<i>3</i> 5.
600	10.	23.	1	25	15.
700	9.0	25,		28.	14.
1kc	6.5	6.0		7.0	10.
4ke	4.0	1.5		2.4	8.0
10kc	4.0	0.60		3.0	8.0
40 kc	3.4	C.30		32	7.5
100kc	3.0	0.25		2.9	6.9
400 kc	5.0	0.50		1.6	7.2
booki	4.0	2.0	1.0	4.0	10.



# CROSSTALK-MINCOM G 107 Recorder Speed-60:ps

Becord Channel 2 Frequency		Becord Channel	Record Chame	Record Channel
C/PS	1	2	3	4
	MY	V <sub>rms</sub>	ner	no V
1kc	9.0	1.0	9.0	13.
2 kc	7.0		5.5	15.
5kc	4.0		2.5	14.
10 kc	2.2		9.0	110
20kc	2.5		0.80	10.
50kc	3.5		2.0	<b>&amp;</b> 5
100kc	5.0		2.5	7.5
150kc	9.0		3.0	7.0
200 kc	18.		/3.	5.0
250kc	40.	4	15.	8.0
Booke	90.	1.0	50	15

# FREQUENCY RESPONSE TEST AMPEX-MODIFIED FR 1400

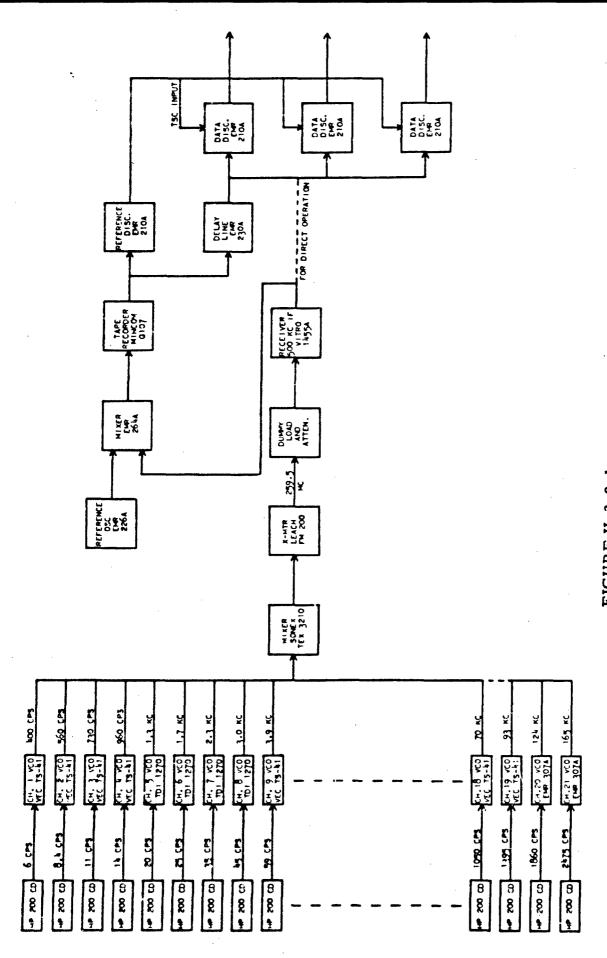
Frequency	Relative Attenuation
Kc	di
265 cps	-3.0
330 cps	-1.0
740 cps	0.0
1.0 kc	0.0 (Ref. Point)
60.0kc	+0.5
100.0kc	+0.5
145.0kc	+1.0
200.0kc	+ 1.5
280.0 kc	+2.5
4 40.0kc	<i>+2.5</i>
600.0kc	0.0
650.0kc	<i>-3.0</i>
710.0k=	-9.0

Channel Record Reproduce; Tape Speed: 120ips

### SECTION 3

### SYSTEM EVALUATION DATA

The detailed procedure for the system test performed on each of the baseban as well as the measured data are contained in the following sections. For reerence, the block diagrams for each experimental telemeter are shown in Fi ures II-3.0-1, II-3.0-2, and II-3.0-3.



BLOCK DIAGRAM OF LABORATORY TELEMETER USED FOR EVALUATION OF PROPORTIONAL BANDWIDTH BASEBANDS FIGURE II-3, 0-1

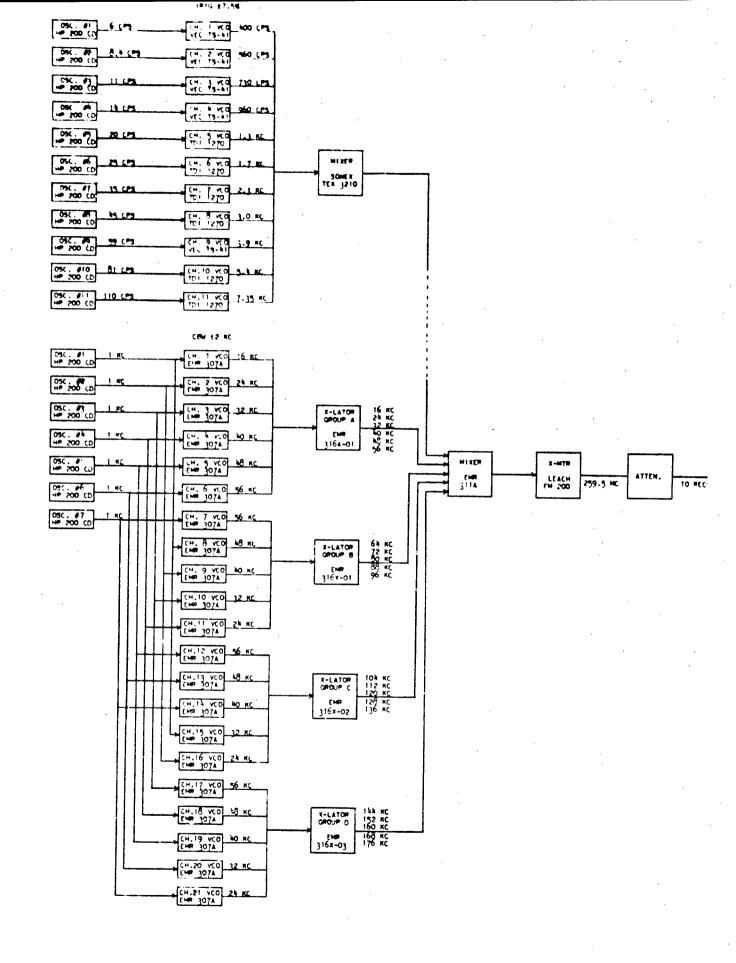
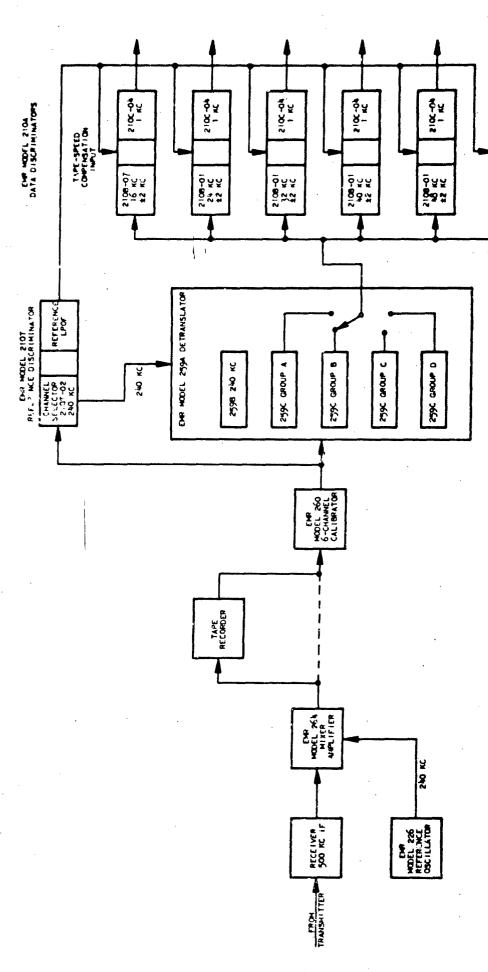


FIGURE 11-3, 0-2
BLOCK DIAGRAM OF AIRBORNE LABORATORY TELEMETER
USED FOR EVALUATION OF CONSTANT AND COMBINATIONAL
BANDWIDTH BASEBANDS



EVALUATION OF CONSTANT AND COMBINATIONAL BANDWIDTH BASEBANDS BLOCK DIAGRAM OF GROUND LABORATORY TELEMETER USED FOR

FIGURE 11-3, 0-3

**4**000 ~

### 3.1 PRE-EMPHASIS SCHEDULE PROCEDURE AND RAW DATA

#### 3.1.1 General

A pre-emphasis schedule for a particular system is considered optimized when identical signal-to-noise ratios occur in each subcarrier discriminator output. Since the receiver output noise characteristics are dependent upon the receiver input carrier-to-noise ratio, a pre-emphasis schedule can only be optimized at one particular receiver carrier-to-noise ratio. Thus, a choice must be made as to carrier-to-noise ratio to be used. For the particular system being evaluated a carrier-to-noise ratio of 9 db, approximately the condition necessary to cause the receiver to threshold, was chosen for optimizing the pre-emphasis schedule.

Normally the subcarrier discriminator output signal-to-noise ratio is measured; however, the subcarrier-to-noise ratio in the band-pass input filter is directly related to the output signal-to-noise ratio. Therefore, for convenience, the pre-emphasis is optimized to produce identical subcarrier-to-noise ratios at the output of the band-pass input filter.

In essence, the procedure is to set a receiver IF carrier-to-noise ratio of 9 db and adjust the individual VCO amplitude levels for equal subcarrier-to-noise ratios in the discriminator while maintaining a multiplex level which does not cause the transmitter output to exceed the radiated spectrum specification. There are several problems inherent to this technique.

The first problem is that of providing a receiver IF carrier-to-noise ratio of 9 db. With the receiver used in the system evaluation, the IF carrier-to-noise ratio is measured at the predetection recording output, which is the IF output just prior to the first-limiter input. If the IF amplifier is a linear system, its input and output carrier-to-noise ratios are identical; however, care must be taken to prevent IF saturation. Through experiment it was found that the maximum unmodulated IF output level which does not cause saturation is 110 mv rms. In addition, the IF saturation characteristic was found to vary somewhat with the AGC voltage. The greatest linear range occurred when the AGC voltage was externally held constant at a -4 vott level. Thus, with the AGC held at -4 volts, the unmodulated IF signal level is measured with a frequency selective voltmeter; this technique eliminates wideband noise and provides an accurate signal level measurement. The input carrier is then turned off and the IF noise measured with a true rms meter.

The second problem is that of adjusting the VCO levels to produce equal subcarrier-to-noise ratios while maintaining a fixed multiplex level so that radiated spectrum specification is not exceeded. This is a trial-and-error method consisting of choosing a trial pre-emphasis schedule, checking to determine if the radiated spectrum is exceeded, and then readjusting the pre-emphasis. There are several short-cuts to this procedure which are given in the following detailed procedure.

#### 3.1.2 Detailed Procedure

- a. Choose a trial taper and, using the radiated-spectrum test described in the next section, determine the maximum total rms transmitter deviation allewable.
- b. Select the deviation for the highest frequency channel from the graph in Figure II-3.1-1.
- c. Starting with the highest frequency channel, set the VCO output levels to the selected taper. A minimum deviation of 3 kc should not be exceeded; therefore, the lower channels may need to be adjusted to equal amplitudes.
- d. Adjust the gain of the mixer amplifier to provide a full multiplex rms level to produce the selected rms transmitter deviation.
- e. With the transmitter unmodulated, externally set the AGC voltage to -4v dc and adjust the rf signal level for an IF carrier-to-noise ratio of 9 db.
- f. Set the video gain of the receiver to produce 2.0 volts rms full multiplex output.
- g. With the VCOs at center frequency (unmodulated), measure the sub-carrier signal-to-noise ratio at the output of the band-pass input filter by measuring the subcarrier signal level and then turning the particular VCO off and measuring the noise. Repeat for each channel.
- h. Readjust the VCO levels to produce equal subcarrier signal-to-noise ratios while maintaining the multiplex level previously selected.
- i. Recheck the radiated-spectrum level and readjust the total multiplex level if necessary. It has been found that once the taper has been adjusted for equal subcarrier-to-noise ratios, small variations in the total multiplex level do not alter the relative relationships of the individual subcarrier-to-noise ratios.
- 3.1.3 FM/FM Proportional Multiplex RMS Carrier Frequency Deviation

Refer to the graph in Figure II-3.1-1.

#### Problem:

The problem is to find relationship between RMS carrier deviation (total) and deviation allocated to top subcarrier, in terms of common ratio between adjacent subcarrier center frequencies, and in terms of constant pre-emphasis slope.

#### Definitions and Conditions:

- 1. Y (>1.0) is common ratio between adjacent subcarrier center frequencies (Y  $\approx$  1.3 for IRIG).
- 2. f<sub>dh</sub> is the peak carrier deviation allocated to the highest-frequency subcarrier.
- 3.  $f_{8k}$  is the center frequency of subcarrier channel k, where k = 1, 2, ...h.
- 4. fdk is the peak carrier deviation allocated to channel k.
- 5. a is the slope of the log-deviation versus log-frequency preemphasis function. It is taken as a constant.
- 6. A large number of subcarriers is assumed.

The peak carrier deviation allocated to subcarrier k is

$$f_{dk} = Cf_{sk}^{a} \tag{1}$$

where C is a constant. For the highest subcarrier, k = h, hence

$$f_{dh} = Cf_{sh}^{a}$$

$$C = \frac{f_{dh}}{f_{sh}^{a}}$$
(2)

from (1) and (2):

$$f_{dk} = f_{dh} \left( \frac{f_{sk}}{f_{sh}} \right)^{a}$$
(3)

Because of the common ratio between adjacent subcarrier frequencies:

$$f_{sk} = \frac{f_{sh}}{y(h-k)}$$

$$\frac{f_{sk}}{f_{sh}} = \frac{1}{y(h-k)}$$
(4)

from (3) and (4) then:

$$f_{dk} = f_{dh} \left[ \frac{1}{y(h-k)} \right]^{a}$$
 (5)

The mean-square carrier deviation due to channel k is:

$$\frac{1}{2} f_{dk}^2 = \frac{1}{2} f_{dh}^2 \left[ \frac{1}{y(h-k)} \right]^{2a}$$
 (6)

the total mean-square carrier deviation is

$$F_{d}^{2} = \sum_{k=1}^{n} \frac{1}{2} f_{dk}^{2}$$

$$= \frac{1}{2} f_{dh}^{2} \sum_{k=1}^{h} \left[ \frac{1}{y(h-k)} \right]^{2a}$$

$$= \frac{1}{2} f_{dh}^{2} \sum_{k=1}^{h} \left[ \frac{1}{y(h-k)} \right]$$

$$= \frac{1}{2} f_{dh}^{2} \sum_{k=1}^{h} \left[ \frac{1}{y^{2a}(h-k)} \right]$$

$$= \frac{1}{2} f_{dh}^{2} \sum_{k=1}^{h} \left[ \frac{1}{y^{2a}} \right]^{h-k}$$

$$F_{d}^{2} = \frac{1}{2} f_{dh}^{2} \left[ 1 + \left( \frac{1}{y^{2a}} \right) + \left( \frac{1}{y^{2a}} \right)^{2} \dots \left( \frac{1}{y^{2a}} \right)^{h-1} \right]$$
(7)

For very large values of h, this is approximately

$$F_{d}^{2} = \frac{1}{2} f_{dh}^{2} \left[ \frac{1}{1 - \frac{1}{y^{2a}}} \right]$$

$$F_{d}^{2} = \frac{1}{2} f_{dh}^{2} \left[ \frac{y^{2a}}{y^{2a} - 1} \right]$$
(8)

The total rms carrier deviation is

$$F_{d} = f_{dh} = \sqrt{\frac{1}{2}} \left[ \frac{y^{2a}}{y^{2a} - 1} \right]^{\frac{1}{2}}$$
 (9)

#### 3.1.4 Results

### 3.1.4.1 IRIG Baseband

For the IRIG baseband, channels 1 through 18, pre-emphasis was optimized using a multiplex level at the transmitter input of 1.0v rms. The measured data is included in Table II-3.1-2 and presented graphically in Figure I-3.2-1.

#### 3.1.4.2 IRIG Baseband--Wideband Channel

The IRIG baseband, channels 1 through 16 and E, was optimized using a multiplex level at the transmitter input of 1.0v rms. The measured data is included in Table II-3.1-3 and presented graphically in Figure I-3.2-3.

### 3.1.4.3 Trial Expanded Proportional-Bandwidth Baseband

The pre-emphasis schedule for the expanded baseband, channels 1 through 20, was optimized using a multiplex level at the transmitter input of 1.0v rms. The measured data is included in Table II-3.1-4 and presented graphically in Figure I-3.2-4.

### 3.1.4.4 Expanded Proportional-Bandwidth Baseband

The pre-emphasis schedule for the expanded baseband, channels 1 through 21, was optimized using a multiplex level at the transmitter input of 750 mv rms. The measured data is included in Table II-3.1-5 and presented graphically in Figure I-3.2-5.

### 3.1.4.5 Expanded Proportional-Bandwidth Baseband--Wideband Channel

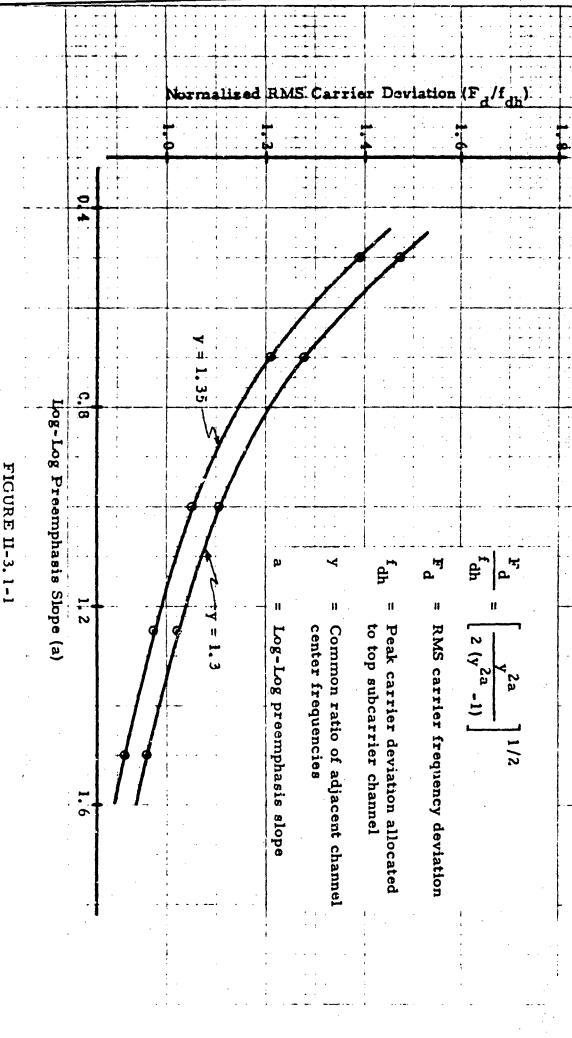
The expanded baseband, channels I through 19 and H, pre-emphasis schedule was optimized using a multiplex level at the transmitter input of 630 mv rms. The measured data is included in Table II-3.1-6 and presented graphically in Figure I-3.2-6.

#### 3. 1. 4. 6 Constant-Bandwidth Baseband

The pre-emphasis schedule for the constant-bandwidth baseband, channels I through 21, was optimized using a multiplex level at the transmitter input of 360 mv rms. The measured data is included in Table II-3.1-7 and presented graphically in Figure I-3.2-8. With channels 17 through 21, Group D, removed and the same taper, the multiplex level at the transmitter was increased to 615 mv rms. The data measured for one channel in each group is included in Table II-3.1-8.

#### 3.1.4.7 Combinational-Bandwidth Baseband

The pre-emphasis schedule for the combinational-bandwidth baseband, IRIG channels I through II and constant-bandwidth channels I through 21, was optimized using a total multiplex level at the transmitter input of 635 mv rms; 600 mv rms for the constant-bandwidth channels and 210 mv rms for the IRIG channels. The measured data is included in Table II-3.1-9 and is plotted in Figure I-3.2-9.



FM/FM PROPORTIONAL MULTIPLEX RMS CARRIER FREQUENCY DEVIATION

### TABLE II-3. 1-2 PREEMPHASIS DATA FOR IRIG BASEBAND, CHANNELS 1 THROUGH 18

System Description: IRIC Chanacks 1 Through 18

igum Deser	· · · · · · · · · · · · · · · · · · ·	./ 0 .		1 0
(S/N)c: 9 db	AGC:	4. Oude	Multiplex:	1.0 Uxms
Channei Frequency (kc)	Signal (dbm)	Noise (dbm)	(S/N) <sub>s</sub> (dbm)	VCO Level (dbm)
0.40±7.5°°	-25.4	-53.8	28.4	-25.0
0.56±7.5%	-24.7	-49.2	24.5	-25.0
0. 73±7. 5 <sup>σ</sup> <sub>0</sub>	-24.8	-45.2	20.4	-25.0
0.96±7.5%	-24.3	-47.2	22.9	-25,0
1.30±7.5%	-24.0	-47,6	23.6	-25.0
1.70±7.5%	-23.2	-46.6	23,4	-23.5
2.30±7.5%	-21.9	-45.1	23.2	-22.5
3.00±7.5%	-21.3	-42.7	21.4	-21.5
3.90±7.5%	-20.5	-43.4	22.9	-20.5
5.40±7.5%	-18.2	-41.8	23.6	-18.5
7.35±7.5%	-16.7	-39.0	22.3	-16.6
10.5 ±7.5%	-14.3	- 38.6	24.3	-14.5
14.5 ±7.5%	-13.0	-37.0	24.0	-12.7
22.0 ±7.5%	- 9.8	- 35.0	25.2	-10.0
30.0 ±7.5%	- 8. C	- 30.0	22.0	- 7.8
40.0 ±7.5%	- 5.9	-29.2	23.3	-5.8
$52.5 \pm 7.5\%$	- 4.6	-26.4	21.8	-4.0
7ე. 0 ±7. 5%	- 2.8	-24.0	212	-2./
93.0 ±7.5%				
124.0 ±7.5%				
165.0 ±7.5%				
70.0 ±15%				
165.0 ±15%	·			

Name: ERC Date: 1-3-65

### TABLE II-3. 1-3 PREEMPHASIS DATA FOR IRIG BASEBAND, CHANNELS 1 THROUGH 16 AND E

System Description: IRIC Channels | Through, 16 and E

(S/N)c: 9db	AGC:_ <u>-</u>	4. Oude	Multiplex:_	1. Ourms
Channel Frequency (kc)	Signal (dbm)	Noise (dbm)	(S/N) <sub>s</sub> (dbm)	VCO Level (dbm)
0.40±7.5%	-27.8	- 52.0	24.2	-27.0
0.56±7.5%	- 27.4	-48.5	21.1	-27.4
0.73±7.5%	-26.8	-46.6	19.8	-267
0.96±7.5%	-26.4	-46.8	20.4	-26.9
1.30±7.5%	-24.2	-46.4	20.2	-26.7
1.70±7.5%	-25.6	-45.6	20.0	-25.8
2.30±7.5%	_ , ,	- 44.0	19,9	-24.7
3.00±7.5%	- 23.8	-43.4	19.6	-23.8
3. 90±7. 5%	-22.8	- 42.2	19.4	-22.7
5.40±7.5%	-20.6	- 40.7	20.1	-20.6
7.35±7.5%	-19.2	-39.7	20.5	-18.9
10.5 ±7.5%	-17.0	- 38.2	21.2	-17.0
14.5 ±7.5%	-15.4	-36.0	20.6	-15.1
22.0 ±7.5%	-12.0	-33.8	21.8	-12.2
30.0 ±7.5%	- 9.3	-30.0	20.7	- 9.2
40.0 ±7.5%	-7.4	-29.0	21.6	- 7.4
52.5 ±7.5%				
70.0 =7.5%				
93.0 ±7.5%	·			
124.0 ±7.5%				
165.0 ±7.5%	,			
70.0 ±15%	0.0	-21.6	21.6	+0.8
165.0 ±15%				

Name: <u>FBC</u> Date: 1-12-65

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### TABLE II-3. 1-4 FREEMPHASIS DATA FOR EXPANDED PROPORTIONAL BANDWIDTH BASEBAND, CHANNELS 1 THROUGH 20

(S/N): 9db AGC: -4.0udc Multiplex: 1.0ums

Channel Frequency (kc) Signal (dbm) Noise (dbm) (dbm) (dbm) (dbm)  0.40±7.5% -27.8 -50.0 22.2 -28.0  0.56±7.5% -27.5 -47.0 19.5 -28.2  0.73±7.5% -28.3 -45.0 16.7 -29.0  0.96±7.5% -27.2 -44.5 17.3 -28.4  1.30±7.5% -26.7 -43.5 16.8 -28.2  1.70±7.5% -26.7 -43.5 16.8 -28.2  1.70±7.5% -26.3 -41.0 14.7 -27.9  3.00±7.5% -26.3 -41.0 14.7 -27.9  3.00±7.5% -25.0 -40.5 15.5 -25.9  3.90±7.5% -24.7 -39.2 14.5 -25.6  5.40±7.5% -21.1 -36.8 15.7 -21.9  10.5±7.5% -18.8 -33.2 14.4 -19.3  22.0±7.5% -14.8 -30.0 15.2 -15.7  30.0±7.5% -17.0 -27.2 14.2 -13.6  40.0±7.5% -17.0 -27.2 14.7 -10.0  70.0±7.5% -7.6 -2.4 -17.7 14.7 -10.0  70.0±7.5% -3.4 -2.4 -17.7 15.3 -0.6  165.0±7.5% -2.4 -17.7 15.3 -0.6	(3/14)c: 4 db		7. Uudc	Multiplex:	1. OUrms
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Frequency			1	Level
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.40±7.5%	-27.8	-50.0	22.2	-28.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.56±7.5%	- 27.5	-47.0	19.5	- 28.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.73±7.5%	-28.3	-45.0	16.7	-29.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.96±7.5%	-27.2	-44.5	17.3	-28.4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.30±7.5%	-26.7	-43.5	16.8	-28.2
$3.00\pm7.5\%$ $-25.0$ $-40.5$ $/5.5$ $-25.9$ $3.90\pm7.5\%$ $-24.7$ $-39.2$ $/4.5$ $-23.6$ $5.40\pm7.5\%$ $-23.2$ $-38.0$ $/5.8$ $-24.2$ $7.35\pm7.5\%$ $-2/.1$ $-36.8$ $/5.7$ $-21.9$ $10.5\pm7.5\%$ $-/9.6$ $-35.1$ $/5.5$ $-20.5$ $14.5\pm7.5\%$ $-/8.8$ $-33.2$ $/4.4$ $-/9.3$ $22.0\pm7.5\%$ $-/4.8$ $-30.0$ $/5.2$ $-/5.7$ $30.0\pm7.5\%$ $-/3.0$ $-27.2$ $/4.2$ $-/3.6$ $40.0\pm7.5\%$ $-//9.9$ $-26.8$ $/4.9$ $-/2.4$ $-/2.4$ $-/2.5$ $-/2.5$ $-7.5$ $-7.6$ $-22.5$ $/4.9$ $-7.5$ $-7.5$ $-7.5$ $-7.5$ $-7.5$ $-7.5$ $-20.5$ $-3.4$ $-20.5$ $/5.1$ $-4.7$ $-10.0$ $-24.7$ $/5.3$ $-0.6$ $-20.0$ $-27.5\%$ $-2.4$ $-17.7$ $/5.3$ $-0.6$ $-20.0$	1.70±7.5%	- 27.8	-43.0	15.2	-29.0
$3.00\pm7.5\%$ $-25.0$ $-40.5$ $/5.5$ $-25.9$ $3.90\pm7.5\%$ $-24.7$ $-39.2$ $/4.5$ $-23.6$ $5.40\pm7.5\%$ $-23.2$ $-38.0$ $/5.8$ $-24.2$ $7.35\pm7.5\%$ $-2/.1$ $-36.8$ $/5.7$ $-21.9$ $10.5\pm7.5\%$ $-/9.6$ $-35.1$ $/5.5$ $-20.5$ $14.5\pm7.5\%$ $-/8.8$ $-33.2$ $/4.4$ $-/9.3$ $22.0\pm7.5\%$ $-/4.8$ $-30.0$ $/5.2$ $-/5.7$ $30.0\pm7.5\%$ $-/3.0$ $-27.2$ $/4.2$ $-/3.6$ $40.0\pm7.5\%$ $-//9.9$ $-26.8$ $/4.9$ $-/2.4$ $-/2.4$ $-/2.5$ $-/2.5$ $-7.5$ $-7.6$ $-22.5$ $/4.9$ $-7.5$ $-7.5$ $-7.5$ $-7.5$ $-7.5$ $-7.5$ $-20.5$ $-3.4$ $-20.5$ $/5.1$ $-4.7$ $-10.0$ $-24.7$ $/5.3$ $-0.6$ $-20.0$ $-27.5\%$ $-2.4$ $-17.7$ $/5.3$ $-0.6$ $-20.0$	2.30±7.5%	-26.3	-41.0	14.7	-27.9
$3.90\pm7.5\%$ $-24.7$ $-39.2$ $14.5$ $-25.6$ $5.40\pm7.5\%$ $-23.2$ $-38.0$ $15.8$ $-24.2$ $7.35\pm7.5\%$ $-21.1$ $-36.8$ $15.7$ $-21.9$ $10.5\pm7.5\%$ $-19.6$ $-35.1$ $15.5$ $-20.5$ $14.5\pm7.5\%$ $-18.8$ $-33.2$ $14.4$ $-19.3$ $22.0\pm7.5\%$ $-14.8$ $-30.0$ $15.2$ $-15.7$ $30.0\pm7.5\%$ $-11.9$ $-26.8$ $14.9$ $-12.4$ $52.5\pm7.5\%$ $-10.0$ $-24.7$ $14.7$ $-10.0$ $70.0\pm7.5\%$ $-7.6$ $-2.4$ $-20.5$ $14.9$ $-7.5$ $-3.4$ $-20.5$ $14.9$ $-7.5$ $-3.4$ $-20.5$ $15.1$ $-4.7$ $124.0\pm7.5\%$ $-2.4$ $-17.7$ $15.3$ $-0.6$ $165.0\pm7.5\%$	3.00±7.5%	-25.0	-40.5	15.5	
$7.35\pm7.5\%$ $-2/.1$ $-36.8$ $15.7$ $-21.9$ $10.5\pm7.5\%$ $-19.6$ $-35.1$ $15.5$ $-20.5$ $14.5\pm7.5\%$ $-18.8$ $-33.2$ $14.4$ $-19.3$ $22.0\pm7.5\%$ $-14.8$ $-30.0$ $15.2$ $-15.7$ $30.0\pm7.5\%$ $-13.0$ $-27.2$ $14.2$ $-13.6$ $40.0\pm7.5\%$ $-11.9$ $-26.8$ $14.9$ $-12.4$ $52.5\pm7.5\%$ $-10.0$ $-24.7$ $14.7$ $-10.0$ $70.0\pm7.5\%$ $-3.4$ $-20.5$ $14.9$ $-7.5$ $93.0\pm7.5\%$ $-3.4$ $-20.5$ $15.1$ $-4.7$ $124.0\pm7.5\%$ $-2.4$ $-17.7$ $15.3$ $-0.6$ $165.0\pm7.5\%$	3. 90±7. 5%	-24.7		14.5	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.40±7.5%	-23.2	-38.0	15.8	-24.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7.35±7.5%	-21.1	- 34.8	15.7	-21.9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.5 ±7.5%	-19.6	-35./	15.5	-20.5
$30.0 \pm 7.5\%$ $-13.0$ $-27.2$ $14.2$ $-13.6$ $40.0 \pm 7.5\%$ $-11.9$ $-26.8$ $14.9$ $-12.4$ $52.5 \pm 7.5\%$ $-10.0$ $-24.7$ $14.7$ $-10.0$ $70.0 \pm 7.5\%$ $-7.6$ $-22.5$ $14.9$ $-7.5$ $93.0 \pm 7.5\%$ $-3.4$ $-20.5$ $15.1$ $-4.7$ $124.0 \pm 7.5\%$ $-2.4$ $-17.7$ $15.3$ $-0.6$ $165.0 \pm 7.5\%$	14.5 ±7.5%	-18.8	- 33.2	14.4	-19.3
$40.0 \pm 7.5\%$ $-1/.9$ $-26.8$ $14.9$ $-12.4$ $52.5 \pm 7.5\%$ $-10.0$ $-24.7$ $14.7$ $-10.0$ $70.0 \pm 7.5\%$ $-7.6$ $-22.5$ $14.9$ $-7.5$ $93.0 \pm 7.5\%$ $-3.4$ $-20.5$ $15.1$ $-4.7$ $124.0 \pm 7.5\%$ $-2.4$ $-17.7$ $15.3$ $-0.6$ $165.0 \pm 7.5\%$ $-10.0$ $-$	22.0 ±7.5%	-14.8	-30.0	15.2	-15.7
52.5 ±7.5% -10.0 -24.7   14.7 -10.0   70.0 =7.5% -7.6   -22.5   14.9   -7.5   93.0 ±7.5% -3.4   -20.5   15.1   -4.7   124.0 ±7.5%   -2.4   -17.7   15.3   -0.6   165.0 ±7.5%   70.0 ±15%	30.0 ±7.5%	-13.0	-27.2	14.2	-13.6
70. 0 = 7. 5% - 7. 6 - 22.5	40.0 ±7.5%	-11.9	-26.8	14.9	-12.4
93. 0 ±7. 5% - 5.4 - 20.5 /5./ -4.7  124. 0 ±7. 5% - 2.4 - /7. 7 /5.3 - 0.6  165. 0 ±7. 5% - 2.4 - /7. 7 /5.3 - 0.6	52.5 ±7.5%	-10.0	-24.7	14.7	-10.0
124. 0 ±7. 5% - 2.4 - 17.7 15.3 - 0.6 165. 0 ±7. 5%	70.0 =7.5%	-7.6	-22.5	14.9	-7.5
165.0 ±7.5% 70.0 ±15%	93.0 ±7.5%	-5.4	-20.5	15.1	-4.7
70.0 ±15%	124.0 ±7.5%	- 2.4	-17.7	15:3	-0.6
	165.0 ±7.5%				
165 0 +15%	70.0 ±15%				
103. 0 213 /8	165.0 ±15%	·			

Name: W. Bishop Date: 1-22-65

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### TABLE II-3, 1-5 PREEMPHASIS DATA FOR EXPANDED PROPORTIONAL BANDWIDTH BASEBAND, CHANNELS 1 THROUGH 21

System Description: PBW Channels 1 Through 21

(S/N): 9db AGC: -4.0 udc Multiplex: 750 muxes

(S/N) <sub>c</sub> : 9 db	AG <b>C</b> :	4.0 Udc	Multiplex:_	750 muxm
Channel Frequency (kc)	nal (dbm)	Noise (dbm)	(S/N) <sub>s</sub> (dbm)	VCO Level (dbm)
0.40±7.5%	-25.7	-50.5	24.8	-28.8
0.56±7.5%	-25.1	-48.5	23.4	-28.8
0.73±7.5%	-24.7	-46.0	21.3	-28.5
0.96±7.5%	-24.7	-45.5	20.8	-28.8
1.30±7.5%	-24.3	-45.0	20.7	-28.5
1.70±7.5%	-24.9	- 45.5	19.6	-28.8
2.30±7.5%	-24.3	-43.0	18.7	-28.6
3.00±7.5%	-25./	-42.2	17.1	-28.8
3. 90±7. 5%	- 25.2	-41.4	16.2	-28.8
5.40±7.5%	-25.4	-39.8	14.4	-29.2
7.35±7.5%	-25.5	-385	13.0	-29.1
10.5 ±7.5%	-249	-37.0	12.1	-28.7
14.5 ±7.5%	-24.5	-34.6	10.1	-28.2
22.0 ±7.5%	-21.4	-32.0	10.6	-25.0
30.0 ±7.5%	- 19.2	-29.6	10.4	-22.8
40.0 ±7.5%	- 16.6	-26,6	10.0	-20.2
52.5 ±7.5%	-14.4	-24.4	10.0	-17.7
70.0 = 7.5%	-11.6	-21.1	9.7	-14.7
93.0 ±7.5%	-8.5	-18.4	9.9	-11.2
124.0 ±7.5%	-5.1	-15.0	9.9	-6.8
165.0 ±7.5%	-2.0	-11.8	9, 8	-2.6
70.0 ±15%				
165.0 ±15%				

Name: MDL/WSB Date: 1-26-65

## TABLE II-3. 1-6 PREEMPHASIS DATA FOR EXPANDED PROPORTIONAL BANDWIDTH BASEBAND, CHANNELS 1 THROUGH 19 AND H

(S/N): 9db AGC: -4 Dude Multiplex: D 434-

(S/N) <sub>c</sub> : 4db	AGC:_=	7.0 udc	Multiplex:_	0.63Urms
Channel Frequency (kc)	Signal (dbm)	Noise (dbm)	(S/N) <sub>s</sub> (dbm)	VCO Level (dbm)
0. 40±7. 5%	-26.5	-52.0	25.5	-30,6
0.56±7.5%	-25:0	-48.0	23.0	- 29.5
0.73±7.5%	-25.6	-47.0	21.4	-30.4
0.96±7.5%	-24.8	-45.5	20.7	-30.0
1.30±7.5%	-24.4	-45.5	21.1	-29.8
1.70±7.5%	-25.6	-44.5	18.4	-30.6
2.30±7.5%	-24.2	-43.5	19.3	-29.5
3.00±7.5%	-26.0	-42.0	16.0	-30.6
3.90±7.5%	T	-42.0	16.8	- 29,8
5.40±7.5%	-25.4	-40.5	15.1	- 30.3
7. 35±7. 5%	-25.2	- 39.6	14.4	-30.0
10.5 ±7.5%	-25.2	-37.5	12.3	-30.2
14.5 ±7.5%	-25.0	-35.4	10.4	-29.7
22.0 ±7.5%	-24.7	-32.5	7.8	-29.6
30.0 ±7.5%	-22.2	-30.0	7.8	-27.6
40.0 ±7.5%	-19.6	-26.8	7.2	-24.7
$52.5 \pm 7.5\%$	- 16.5	-23.8	7.3	-21.1
70.0 ±7.5%	-13.0	-20,5	7.5	-17.6
93. 0 <b>±7.</b> 5%	-10.1	-17.5	7.4	-14.2
124.0 ±7.5%		,		
165.0 ±7.5%				
70.0 ±15%			•	
165.0 ±15%	-0.2	-7.6	7.4	-2.4

Name: W. Bishop Fate: 1-29-6.5

### TABLE II-3. 1-7 PREEMPHASIS DATA FOR 21-CHANNEL CONSTANT BANDWIDTH BASEBAND

System Description: Constant Bandwidth Multiplex (S/N, c: 9db AGC: -40 VDC Multiplex: 360 mvrms

(9)14, c.	AD AUC	- 7.0 VIC	Materprex	JOO MILIAI.
Channel Frequency (kc)	Signal (dbm)	Noise (dbm)	(S/N) (db)	VCO Lavel (dbm)
176.0	-18.0	- 23.5	5.5	-15.0
168.0	-17.2	-22,8	5.6	-155
160.0	-16.5	-22.0	5.5	-15.9
152.0	-17,0	-22.6	5.6	-16.5
144.0	-16.9	-22.5	5.6	-17.4
136.0	-17.8	- 23.0	52	- 18,1
128.0	-16.8	-22.2	5.4	-190
120, 0	-16.1	- 21.7	5.6	-195
112.0	-17,2	- 22.6	5.4	-20,3
104.0	-16.8	- 22.0	5.2	-21.3
96. 0	-16.0	-21.4	5.4	-22.1
88.0	-16.0	-21.5	5,5	-22.9
80.0	-16.0	-21.4	5.4	-23.5
72.0	-15.8	- 21.5	5.7	-24.3
64.0	-15.8	-21.7	5.9	-25.1
. 56.0	-17.2	-22.8	5.6	-26.6
48.0	-17.7	- 23.3	5.6	-27.6
40.0	-17.5	-23.3	5.8	-28.6
32.0	-18.1	-239	5.8	-30.5
24.0	-17.7	-24.6	6.9	-30.6
16.0	- 18.3	-25.6	7.3	-31.6
7. 35				
5.4				
3. 9				
3.0				
2.3				
1.7				
1.3				
0, 96				
0. 73				
0,56				
0.40				

-113- Name: WdB Date; 3-12-65

TABLE II-3. 1-8
PREEMPHASIS DATA FOR 16-CHAPNEL CONSTANT BANDWIDTH BASEBAND

System Description: Channels / Alrengh 16 Constant Breliefeth

(S/N)<sub>c</sub>: 9db AGC:-40Vdc Multiplex: 615 mv rms; Ref: 200 mv<sub>rms</sub>

	` C				
	Channel Frequency (kc)	Signal (dbm)	Noise (dbm)	(S/N) <sub>s</sub> (db)	VCO Level (dbm)
;	175.0				
	168.0				
	160.0	·	$\gg <$		
,	152.0				
,	144.0				
#	136.0	-21.2	-32.5	11.3	
	128.0				
	120.0				
	112.0				·
	104.0				
	96. 0				
*	88.0	-17.7	-30.0	12.3	
[	80.0				
	72. 0		,		
	64. 0				
	56.0				·
	48.0				
*	40.0	-18.0	-30.0	12.0	
	32.0				·
	24.0				
	16.0				
	2, 35				
	5. 4				
	3. 9				
	3. 0				
L	2. 3				
	1.7		X		
	1.3				
	0.96				
	0,73				
	0.50		<u> </u>		
	. 40	<u> </u>			

-114- Name: WSE/MOL Date; 3-8-65

### TABLE II-3. 1-9 PREEMPHASIS DATA FOR COMBINATIONAL BANDWIDTH BASEBAND

System Description: Combastional Sunday, sth Multiplex
(S/M)c: 906 AGC: -4000c Multiplex: 635 murms

	<del></del>	~ · · · · · · · · · · · · · · · · · · ·		
Channel Frequency	Signal (dbm)	Noise	(S/11) <sub>s</sub> (db)	VCO Level (dbm)
(kc)		(dbm)		
	-20.4	- 29./	8.7	-/0.5
168. 0	- 19. 2	-28.3	9.1	-11.0
160.0	-18.6	-27.5	8.9	-11.4
1: 2. 0	-19.0	-28, c	9:0	-11.9
144.0	-18.8	-27.8	9.0	-/2.8
136.0	-19.7	-28.5	8.8	-136
128. 0	<i>- 18,7</i>	-27.5	8.8	-14.5
120.0	- 18.0	-27.0	9,0	-14.8
112.0	- 19.0	<i>-27.9</i>	8.9_	-15.6
104.0	-18.4	-27.3	8.9	-16.5
96.0	-17.9	-26.6	8.7	-17.4
88.0	-17.9	-24.6	8,7	-18.2
80.0	-17.8	-26.4	8,6	-18.8
72. 0	-17.6	-26.4	8.8	-9.6
64.0	-17.5	-26.5	9.0	-20,5
56.0	8.9	- 27.5	8.6	-22.0
48.0	-19.3	-27.8	8.5	-230
40.0	-19,2	-27,6	8.4	-24,0
32.0	- 19.6	-27.8	8,2	-25.8
24.0	-19.0	-27.9	8.9	-26,0
16.0	-19.5	-28,1	8.6	-27.0
7. 35	-9.1	-34,0	24.9	-16.6
5.4	- 11.0	-36,0	25.0	- 18.5
3.9	- 13. Z	-36.5	23, 3	-20.5
3.0	-13.7	-37.2	23.5	-21.5
2.3	-14,2	-38.4	24.2	- 72.5
1.7	-15.5	-39,8	24.3	-23.5
1.3	-16.2	-39.0	22.1	-25.0
0.96	-16.3	-41,0	24.7	- 250
0. 73	-16.8	-40.0	23.2	25.0
0.56	- 17.5	-43.0	25.5	- 75.0
0.40	-18.5	-46.0	27.5	- 25. U
			· <del></del>	

-115- Name: WSB Date; 3-12-65

#### 3.2 RADIATED SPECTRUM TEST

#### 3.2.1 General

The object of the radiated spectrum test is to determine the maximum transmitter drive that will not exceed the transmitter radiated spectrum specification:

The power spectral density, as measured in a 1000-cps bandwidth, outside a bandwidth of ±320 kc shall not exceed -50.5 db referenced to the unmodulated carrier. Carrier components outside a ±500 kc bandwidth shall not exceed -25 dbm.

For test purposes, an allowance of 26 kc is made on each side of the spectrum for transmitter drift. Also, the ±500-kc-bandwidth specification was checked at 75 db below the unmodulated carrier which is the -25 dbm level for a 100-watt transmitter.

The general technique used in measuring the transmitter radiated power spectral density is to translate the transmitter output spectrum down to a frequency range around 1 Mc and then use a frequency selective voltmeter with a 1 kc bandwidth to measure the power spectral density. This translation technique proides a quantitative measure on an rms voltmeter of the power spectral density. A resuging by eye as required by spectrum analyzers is eliminated. The frequercy selective voltmeter used in this test has a frequency range from 1.0 kc to 1.5 Mc. In order to measure the complete transmitter spectrum within this range, it is necessary to first place the local oscillator frequency 1 Mc below the carrier frequency. Measurements are then made from 1.2 Mc down to several hundred kilocycles. The local oscillator is next placed 1 Mc higher in frequency than the carrier. Having the local oscillator above the carrier inverts the output spectrum of the transmitter in the translation process. Thus, the other side of the spectrum can now be measured with the frequency selective voltmeter. This method gives an accurate, convenient, and quantitative measurement of the total transmitter power spectral density.

#### 3.2.2 Detailed Procedure

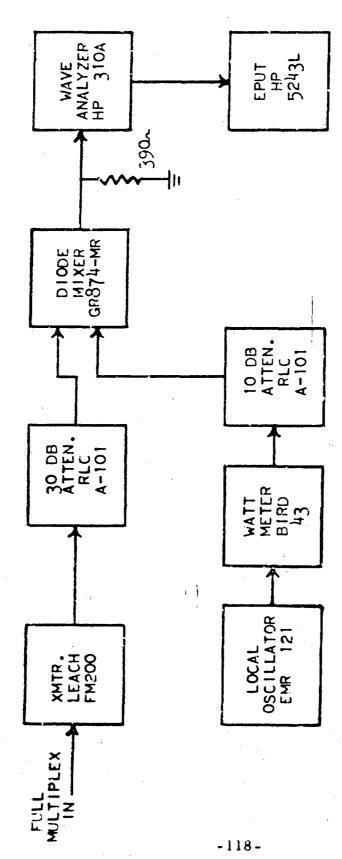
- a. The block diagram for this test is shown in Figure II-3.2-1.
- b. Choose an attenuator for the local oscillator so that the local oscillator provides at least ten times as much current to the crystal diode as does the transmitter output.
  - c. Tune the local oscillator 1 Mc below the frequency of the transmitter.

- d. With the transmitter unmodulated, tune the frequency selected volt-meter to the unmodulated carrier. This should be approximately 1 Mc. Note the level of the unmodulated carrier.
- e. Modulate the transmitter with the full multiplex. The VCOs should be unmodulated and at center frequency.
- f. With the frequency selective voltmeter set to the 1000-cycle band-width position, measure the radiated power spectral density by sweeping the frequency selective voltmeter from 1.2 Mc to 100 kc and noting the meter readings.
- g. Tune the local oscillator to 1 Mc above the frequency of the carrier and repeat the previous readings.
- h. The transmitter radiated power spectral density curve hould be down 50.5 db from the peak of the modulated power spectral density curve.
- i. If the radiated spectrum specification is exceeded, reduce the gain of the mixer amplifier \( \) repeat the test.

### 3.2.3 Results

The radiated spectrum data—given in Tables II-3.2-2 through II-3.2-6—Specific data may be found with the aid of the following chart:

Multiplex Description	Doea Shown in Table	Data Plotted in Figure
IRIG Channels 1 through 18	II-3.2-2	I-3.3-3
IRIG Channels 1 through 16 and E	3.2-3	I-3.3-4
Expanded Channels 1 through 21	II-3.2-4	I-3.3-5
Expanded Channels 1 through 19 and H	II-3.2-5	I-3.3-6
Constant-Bandwidth Channels 1 through 21	II-3.2-0	I-3.3-7
Constant-Bandwidth Channels 1 through 16	Ц-3.2-7	I-3.3-8
Combination Bandwidth	II-3.2-8	I-3.3-9



TRANSMITTER RADIATED SPECTRUM TEST BLOCK DIAGRAM FIGURE II-3, 2-1

### TABLE II-3.2-2 RADIATED SPECTRUM DATA: IRIG CHANNELS 1 THROUGH 18

Local Oscillator 253.7 mc			Local Oscillator 269.7 mc			
Measured	Normalized	Level in	Measured	Normalized	Level in	
Frequency	Frequency	1.0 kc BW	Frequency	Frequency	1.0 kc BW	
(kc)	(kc)	(dbm)	(kc)	(kc)	(dbm)	
1000		-35.5	1000	0	-35,5	
950	-50	-36.5	950	+50	-36.2	
900	-100	-39.5	900	+100	-39.0	
850	-150	-43.5	850	+150	-44.0	
800	-200	-49.5	800	+200	-50.5	
750	-250	-56.0	750	+250	-59.0	
700	- 300	-64.5	700	+300	-68.0	
450	-350	-74.0	650	+350	- 78.0	
600	-400	-84.0	600	+400	-93.0	
550	-450	-940	550	+450	-101.0	
500	-500	-100.0	500	+500	-102.0	
450	-53-0	-101.0	450	+550	-102.0	
400	-600	-102.0	400	+600	-102.0	
350	-650	-101.0	350	+650	-102.0	
300	-700	- 101.0	300	+700	-102.0	
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Name: 438 Date: 11-23-64

### TABLE II-3.2-3 RADIATED SPECTRUM DATA: IRIG CHANNELS 1 THROUGH 16 AND E

Baseband Structure: 1R1G Channels 1Through 16 and E

Multiplex Level: 1.0 Urms Unmodulated XMTR: 259,7 mc

-18.5 dbm

Local Oscillator 2.4.8.7 mc			Local Oscillator 260.7 mc			
Measured	Normalized	Level in	Measured	Normalized	Level in	
Frequency	Frequency	1.0 kc BW	Frequency	Frequency	1.0 kc BW	
(kc)	(kc)	(dbm)	(kc)	(kc)	(dbm)	
1000	0	-42.0	1000	0	-42.0	
950	-50	-430	950	+50	-43.0	
900	-100	-45.5	900	+/00	-45,5	
850	-150	-540	8.50	+1.50	-57,0	
800	-200	-57.5	800	+200	-58.5	
750	-250	-65.5	750	+250	-67.5	
700	-300	-75.0	700	4300	-780	
650	-350	-84:0	650	+350	-89.5	
600	-400	-96.0	600	+400	-101.0	
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Name: MDL Date: 1-12-65

### TABLE II-3.2-4 RADIATED SPECTRUM DATA: EXPANDED CHANNELS 1 THROUGH 21

Multiplex Level: 750 mVrms Unmodulated XMTR: 259.7 mc \_-/5.2 dbm

Local Oscillator 258.7 mc			Local O-cillator 258.7 mc		
Measured	Normalized	Level in	Measured	Normalized	Level in
Frequency	Frequency	1.0 kc BW	Frequency	Frequency	1.0 kc BW
(kc)	(kc)	(dbm)	(kc)	(kc)	(dbm)
1000	0	-30.0	1000	0	-30.0
975	-25	-45.0	1025	125	-45.0
950	-50	-47.5	1050	+50	-47.5
925	- 75	-49.5	1075	+75	-49.5
907	-93	-48.0	1093	+93	-48.0
900	-/00	-50.0	1100	+100	-50.0
875	-125	-47.0	1/25	+125-	-47.0
850	-150	-57,5	1150	+150	-52.5
835	-/65	-45,5	1165	+165	-46.0
825	-175	250.0	1/75	+175	-50.0
800	-200	-60.5	1200	t200	-6/15
775	-225	-62,5	1225	+225	-63,5
750	-250	-63.5	1250	+250	-64,5
725	-275	-67.0	1275	+275	-67.5
711	-289	-620	1289	+289	-63,5
700	-300	-66.5	1300	+300	-68.5
675	-325	-67.2	1325	<i>+325</i> ⁻	-695
670	-330	-66.5	1330	+330	-68.5
650	-350	-76.0	1350	+3570	-78.5
625	~375	-78.8	/375	+375	- 82.0
600	-400	-82.0	1400	+400	-85.5
5370	-450	-82,5	1450	+450	-86.5
500	-500	-90.5	1500	+570	-95.0
450	-550	-99.0	1550	+550	-1040
400	-600	-1040	1600	+600	-104.0
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Name: WS 8/MDL Date: 1-26-65

### TABLE II-3.2-5 RADIATED SPECTRUM DATA: EXPANDED CHANNELS 1 THROUGH 19 AND H

Baseband Structure: Expanded Channels 17hrand 19 and H

Multiplex Level: 630 myrms Unmodulated XMTR: 259.7 mc

-13.8 dbm

Local Oscillator 260.7 mc			Local Oscillator 260.7 mc		
Measured	Normalized	Level in	Measured	Normalized	Level in
Frequency	Frequency	1.0 kc BW	Frequency	Frequency	1.0 kc BW
(kc)	(kc)	(dbm)	(kc)	(kc)	(dbm)
1000	0	-26.5	1000	0	-26.5
1025	-25	-45.5	975	+25	-45.5
1050	-50	-48.5	950	+50	-48.5
1075	- 75	-49,2	925	+75	-49.0
1093	-93	-47.5	907	+93	-47.5
1100	-100	-50.5	900	+100	-49.5
1125	-125	-62.0	875	+125	-622
1150	-150	-52,5	850	+150	-53.0
1165	-165	-42.0	835	+165	-420
1175	-175	-48.0	825	+175	-47.0
1200	-200	-64.0	800	+260	-63.0
1225	-225	-65.5	775	+225	-64.5
1235	- 235	-64.0	765	+235	-63.0
1250	-250	-66.0	750	+250	-66.0
1258	-258	-63.5	742	1258	-62.5
1275	-275	-760	725	+275	-73.0
1300	-300	-82.0	700	+300	-8/,0
1325	-325	-65.0	675	+325	-64.5
1330	-330	-64.5	670	+330	-63.4
1350	-350	-82.0	1.50	+350	-770
1375	-375	-87.0	625	+375	-845-
1460	-400	- 87.C	400	+400	-835-
1425	-425	-87.2	5-75	+425	-83.0
1450	-450	-97.0	550	+450	-920
1475	-475	-99.0	525	+475	-/00.0
1500	-500	- 92.5	500	1500	-88.3
15-25	-525	-99.2	475	+5525	-/00.0 -88.3 -/03.0

Name: WSB Date: 1-29-65

### TABLE II-3.2-6

### RADIATED SPECTRUM DATA: CONSTANT BANDWIDTH MULTIPLEX CHANNELS 1 THROUGH 21

Baseband Structure: Channe 1-21 CBW

Multiplex Level: 360 myrms Unmodulated XMTR: 2597 mc

-14.8 dbm

Local Oscillator 2582 mc			Local Oscillator 258.2 mc		
Measured Frequency (kc)	Normalized Frequency (kc)	Level in 1.0 kc BW (dbm)	Measured Frequency (kc)	Normalized Frequency (kc)	Level in 1.0 kc BW (dbm)
1500	0	-15.1	1252	- 248	-65.0
1442	8	- 61.0	1244	- 256	-65.5
1484	- 16	- 38.2	1236	- 264	-600
1476	- 24	-40.5	1228	- 272	-66.5
1468	- 32	-43.0	1220	- 280	-66.5
1460	- 40	-43.0	1212	- 288	-66.5
1452	- 48	-43.5	1204	- 296	-67.5
1444	- 56	-44.0	1196	- 304	-68.0
7436	- 64	- 43.8	1188	- 312	-68.0
1428	- 72	-44.0	1180	- 320	-690
1420	- 80	-44.2	1172	_ 328	-67.0
1412	- 68	-44.5	1164	- 336	-71.5
1404	- 96	-44.4	1156	- 344	-72.0
1396	-104	-44.5	1148	- 352	-78.0
1388	- 112	-44.2	1'40	- 360	-84.5
1380	- 120	-74.2	1132	- 368	-85.0
1372	- 128	44.3	1124	- 376	-85.0
1364	- 136	-44.2	1116	- 384	-86.0
1356	_ 144	-44.0	1108	- 392	-86.5
1348	- 152	-438	1100	- 400	-86.5
1340	-160	-43.8	1092	- 408	-87.5
1332	- 168	-44.0	1084	- 416	-87.5
1324	- 176	- 44.0	1076	- 424	-87.5
1316	- 184	-61.0	1068	- 432	-88.0
1308	- 19.2	-61.0	1060	- 440	-88.5
1300	- 200	-63.0	1052	- 448	-81.5
1292	- 208	-63.0	1044	- 456	-88.5
1284	- 216	-64.0	1034	- 464	-89.0
1276	- 224	-64.5	1028	- 472	-89.5
1268	- 232	-645	1020	- 480	-40.2
1260	-240	-64.0	1012	- 488	-90.2

Sheet 1 of 2

Name: WSB/MOL Date: 3-12-65

## TABLE II-3. 2-6 (CONT'D.) RADIATED SPECTRUM DATA: CONSTANT BANDWIDTH MULTIPLEX CHANNELS 1 THROUGH 21

Baseband Structure: Channel 1-21 CBW

Multiplex Level: 360 myrms Unmodulated XMTR: 259.7 mc -14.8 dbm

Local Oscillator 2582 mc			Local Oscillator 26/.2 mc		
feasured requency (kc)	Normalized Frequency (kc)	Level in 1.0 kc BW (dbm)	Measured Frequency (kc)	Normalized Frequency (kc)	Level in 1.0 kc BW (dbm)
1004	-496	-90.5	1330	210	-676
996	-504	-92.0	1212	211	-68.1
988	-512	-920	1204	2%	-68.4
980	-520	-92.0	1196	304	-60.1
			1188	3/2	-69.6
			1180	320	-70.6
			1020	480	- 47.6
			1012	418	-98.6
	·		1004	496	-99.6
			996	504	-102.0
			987	512	-102.0
			980	520	-102.0
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Sheet Zof 2

Name: 458/102 Date: 3-12-65

### TABLE II-3, 2-7 RADIATED SPECTRUM DATA: CONSTANT BANDWIDTH MULTIPLEX CHANNELS 1 THROUGH 16

Baseband Structure: Channe 1-16, CBW

Multiplex Level: 6/5 MU-me Unmodulated XMTR: 2507

dbm

Local Oscillator 2587 mc			Local Oscillator 258.7 mc		
Measured	Normalized	Level in	Measured	Normalized	Level in
Frequency	Frequency	1.0 kc BW	Frequency	Frequency	1.0 kc BW
(kc)	(kc)	(dbm)	(kc)	(kc)	(dbm)
1000	٥	-15.8	1248	248	-55.0
1008	8	-41.0	1256	256	-570
1016	16	-30.5	1264	264	-58.0
1024	24	-32.5	1272	272	-62.0
1032	32	-33.5	1280	280	-64.0
1040	40	- 34.5	1288	288	-65.5
1048	48	-34,5	1296	296	-66.0
1056	56	-35.0	1304	304	-67.0
1064	64.	-35.5	1312	312	-68.0
1072	72	-36,0	1320	320	-68,5
1080	90	-35.5	1328	328	-69.5
1088	88	-34.0	1336	336	-70.0
1096	96	- 34.0	1344	344	-71.5
1104	104	-36.0	1352	332	-72.5
1112	ila	-36.5	1360	360	-74.0
1120	120	-36.5	1368	368	-75.0
1128	128	-37.0	1376	376	-77.0
1136	136	-37.0	1384	384	-78.0
1144	144	-46.5	1392	392	-81.0
1152	152	-46.5	1400	400	-83.0
1160	160	-47.5	1408	403	-84.5
1168	148	-48.5	1416	416	-86.0
1176	176	-49.0	1424	424	-87.0
1184	184	-49.5	1432	432	- 83.0
1192	192	-50.0	1440	440	-89.0
1200	200	-50.5	1448	448	-90.0
1200	208	-57.5	1452	45%	- 92.1
1216	216	-52.0	1456	464	-930
1224	224	-470	1472	412	- 92.0 - 93.0 - 94.0
1232	232	-53.0 -53.5 -54.5	1480	464 472 480	-95.0
1240	240	A- 11 A-	1488	488	-97.0

Name: W3 8/AD4 Date: 3-9-65

# TABLE II-3. 2-7 (CONT'D.) RADIATED SPECTRUM DATA: CONSTANT BANDWIDTH MULTIPLEX CHANNELS 1 THROUGH 16

Multiplex Level: 6/5 MVyms Unmodulated XMTR: 259,7 mc -14,2 dbm

Local Oscillator 258.7 mc			Local Oscillator mc		
feasured requency (kc)	Normalized Frequency (kc)	Level in 1.0 kc BW (dbm)	Measured Frequency (kc)	Normalized Frequency (kc)	Level in 1,0 kc BW (dbm)
1496 1504 1528 1536 1544	496 504 528 536 544	-98.5 -99.5 -97.0 -96.0 -96.0			
1552	552	-94.0			

Name: (4) S 8 /MDL Date: 3-9-65

# TABLE II-3.2-8 RADIATED SPECTRUM DATA: COMBINATIONAL BANDWIDTH MULTIPLEX

Multiplex Level: 635 murms Unmodulated XMTR: 559.7 mc dbm

Local Oscillator 2378,2 mc			Local Oscillator 258,2 mc		
Measured	Normalized	Level in	Measured	Normalized	Level in
Frequency	Frequency	1.0 kc BW	Frequency	Frequency	1.0 kc BW
(kc)	(kc)	(dbm)	(kc)	(kc)	(dbm)
1500		-32.5	1252	-248	-65:2
1492	- 8	-33.0	1244	- 256	-65.5
1484	-16	-34.0	1236	- 264	-66.0
1476	-24	-36.5	1338	- 272	-66.5
1468	- 32	-40.0	1220	-280	-66.8
1460	- 40	-42.5	1212	-288	-67.0
1452	- 48	-46.5	1204	-296	-67.5
1444	- 56	-48.5	1196	-304	-68.0
1436	- 64	-49.5	1188	- 3/2	-68.5
1428	- 72	-49.8	1180	- 320	-(09.5
1420	- 80	-49.8	1172	- 328	-70.0
1412	- 88	-49.8	1164	-336	-70.8
1404	- 96	-49.8	1156	- 344	-72.5
1396	-/04	-49.9	1/48	- 352	-73.5
1388	-112	- 49.8	1140	-360	75.5
1380	-120	-49.8	1132	-368	-77.5
1372	-128	-49.8	1124	-376	-79.5
1364	- 136	-49.8	1116	-384	-81.0
1356	- 144	-49.8	1108	- 392	-82.5
1348	-152	-49.8	1100	- 400	-83.5
1340	-160	-50.0	1092	- 408	-83.5
1332	-168	-50.5	1084	-416	- 84.0
1324	-176	-51.5	1076	- 424	- 84,5
1316	-184	-53.0	1068	- 432	-85,5
1308	-192	-55.0	1060	-440	-85.5 -86.0
1300	- 200	-57.0	1052	- 448	-86.5
1292	- 208		1044	-456	-87.0
1284	-216	-62.0	1036	-464	-87.5
1276	- 224	-63.5	1078	-472	- 88.0
1268	- 232	-64.5	1020	-480	-89.0
1260	- 240	-64.8	1012	- 488	-90.0

Sheet 1 of 2

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## TABLE II-3.2-8 (CONT'D.) RADIATED SPECTRUM DATA: COMBINATIONAL BANDWIDTH MULTIPLEX

Multiplex Level: <u>G35 mrrms</u> Unmodulated XMTR: <u>259 7</u> mc dbm

Local Oscillator 25/2 me			Local Oscillator 261.2 mc		
Measured Frequency (kc)	Normalized Frequency (kc)	Level in 1.0 kc BW (dbm)	Measured Frequency (kc)	Normalized Frequency (kc)	Level in 1.0 kc BW (dbm)
1004	-496	-91.0	1220	280	-675
996	-504	-020	1212	288	-690
988	- 5/2	-930	1204	296	-68.5
980	-520	-940	1196	304	-69.5
			1188	3/2	-70.0
			1180	320	-70.5
	·		1020	480	- 925
			1012	487	-93.0
	·		1004	496	-950
			496	504	-96.0
			988	5/2	-970
			980	520	-985
					·
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#### 3.3 SYSTEM INTERMODULATION TEST

#### 3.3.1 General

The system intermodulation test consists of removing the modulation for one particular channel, called the search channel, and substituting a voltage ramp to sweep the channel slowly from low bandedge (LBE) to high bandedge (HBE). With the remaining channels in the multiplex modulated by sine-wave oscillators, the intermodulation on the search channel output is viewed on an oscilloscope and photographed. In the technique used, the oscilloscope horizontal sweep waveform deviated the search channel from LBE to HBE in 40 seconds. The block diagram for the test is shown in Figure II-3.3-1.

#### 3.3.2 Detailed Procedure

- a. With the pre-emphasis schedule and transmitter deviation selected from previous tests, provide the receiver with an rf signal so that the IF S/N ratio is greater than 20 db.
  - b. Calibrate all VCOs.
- c. Deviate all VCOs FBW at 5 cps or 0.1  $f_{\rm m}$ , whichever is larger, where  $f_{\rm m}$  is the maximum data response of the channel for the particular deviation ratio.
- d. Set the discriminator output level for  $\pm 10$  volts for bandedge deviation.
- e. Set the oscilloscope sweep speed to 5 sec/cm and adjust the amplitude of search channel input to deviate the channel to full bandwidth (FBW). This should be verified by viewing the dc-coupled sweep on a vertical scale of 5 v/cm.
- f. The ac-coupled trace can now be used to view intermodulation noise on the 0.1v/cm vertical scale. Using the single trace provision, photograph the trace with a lens setting of f:10.

#### 3.3.3 Results

Typical data are shown in Figure II-3.3-2. In Figure II-3.3.2a, trace no. 1 is the discriminator output dc coupled and showing the horizontal calibration. Trace no. 2 is the amplified and ac-coupled discriminator output signal. This particular test has been arranged to demonstrate a beat note by holding the VCOs causing the beat at center frequency. Figure II-3.3-2b is the same channel with the same VCOs modulated. To prevent overexposure, the direct-coupled-discriminator

output is not shown on the data photographs. The photograph in Figure II-3.3-2a was taken using an alternate-sweep mode. In all cases, the calibration was checked prior to taking a photograph.

#### 3. 3. 3. 1 IRIG Baseband

The detailed conditions for the test were:

Test channels: IRIG channels 1 through 18

Multiplex level: 1.0 volt rms

IF S/N ratio: 39 db

Deviation ratio: 5, 2, and 1

LPOF: Nominal f for DR, constant amplitude 18 db/octave type

Figures II-3.3-3 through II-3.3-20 show the results of the 18-channel system test. The data has been summarized in Figure I-3.4-2.

#### 3. 3. 3. 2 Wideband IRIG Baseband

The detailed conditions for the test were:

Test channels: IRIG channels I through 16 plus channel E

Multiplex level: 1.0 volt rms

IF S/N Ratio: 39 db

Deviation ratio: 5

LPOF: Nominal f for DR = 5, constant amplitude 18 db/octave

type

Figures II-3.3-21 through II-3.3-26 show the results of the wideband IRIG system operated at a deviation ratio of 5. The data is summarized in Table I-3.4-3.

### 3.3.3.3 Expanded Baseband

The detailed conditions for this test were:

Test channels: 1 through 21

Multiplex level: 750 mv rms

IF S/N ratio: 39 db

Deviation ratio: 5

LPOF: Nominal  $f_c$  for DR = 5, constant amplitude 18 db/octave

type

Figures II-3, 3-27 through II-3, 3-33 show the results of the 21-channel system. The data is summarized in Table I-3, 4-3.

### 3.3.3.4 Wideband Expanded Baseband

The detailed conditions for this test were:

Test channels: i through 19 plus channel H

Multiplex level: 630 mv rms

IF S/N ratio: 39 db

Deviation ratio: 5

LPOF: Nominal  $f_c$  for DR = 5, constant amplitude 18 db/octave

type

Figures II-3. 3-34 through II-3. 3-40 show the results of the wideband expanded baseband system. The data has been summarized in Table I-3. 4-3.

#### 3.3.3.5 Constant-Bandwidth Baseband

The detailed conditions for this test were:

Test channel: 1 through 21

Multiplex level: 360 mv rms

IF S/N ratio: 39 db

Deviation ratio: 2

LPOF: Nominal  $f_c$  for DR = 2, constant amplitude 42 db/octave

type

Figures II-3. 3-41 through II-3. 3-47 show the results of the constant-bandwidth baseband intermodulation for a deviation ratio = 2. This data is summarized in Table I-3. 4-4.

Figures II-3. 3-48 through II-3. 3-55 show the results of intermodulation data for constant-bandwidth channels 6, 10, 14, and 19 for deviation ratios of 1, 2, and 4 for these conditions of modulation on all other channels: modulation index equal to deviation ratio of search channel and with all channels at center frequency unmodulated. This data is summarized in Table I-3. 4-5.

Figure II-3. 3-56 shows a comparison of deviation ratios of 4, 2, and 1 on constant-bandwidth channel 6. Figure II-3. 3-57 shows the effect of changing the subcarrier discriminator output filter from a 7 pole (42 db/octave) to a 3 pole (18 db/octave) type on constant-bandwidth channels 3, 6, and 19. Figure II-3. 3-58 shows the effect of bypassing the rf link in the constant-bandwidth system for channel 6 operated at a deviation ratio of 2. Figure II-3. 3-59 shows the effect of replacing the Nems-Clarke Model 1455A with a Defense Electronics Model TMR-2A Receiver in the normal constant-bandwidth system. The above data is summarized in Table I-3. 4-7.

The constant-bandwidth-system intermodulation was investigated using an EMR Model 246A in place of the Leach Model FM 200 Transmitter. Data for various system modifications was taken and is shown in Figures II-3.3-60 and II-3.3-61. This data is discussed in Section 3.4 of Volume I and is summarized in Table I-3.4-8.

#### 3.3.3.6 Combinational-Bandwidth Baseband

The detailed conditions for this test were:

Test channels: IRIG channels 1 through 11; CBW channels 1 through 21

Multiplex level: 635 mv rms; IRIG channels, 210 mv rms; CBW channels, 600 mv rms

IF S/N ratio: 39 db

Deviation ratio: IRIG channels, DR = 5; CBW channels, DR = 2

LPOF: Nominal f<sub>c</sub> for DR used, constant amplitude: 42 db/octave for CBW channels, 18 db/octave for IRIG channels

Figures II-3. 3-62 through II-3. 3-72 show the results of the combinational-bandwidth baseband intermodulation. Figure II-3. 3-73 shows the inclusion of IRIG channel 12 into the baseband. This data is summarized in Table I-3. 4-6.

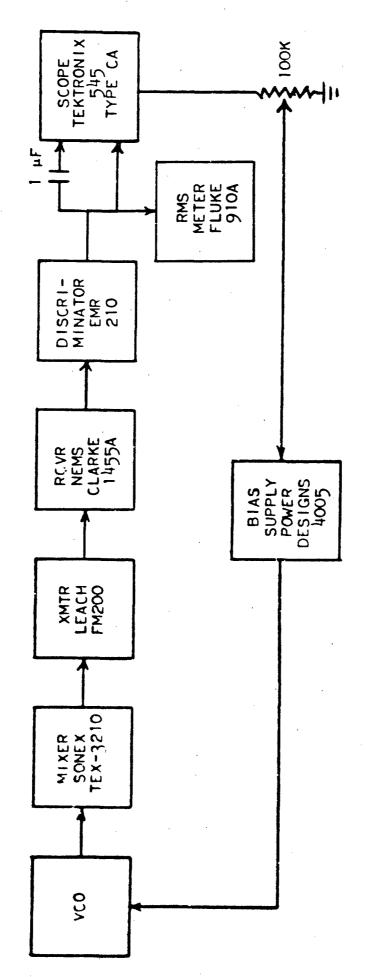
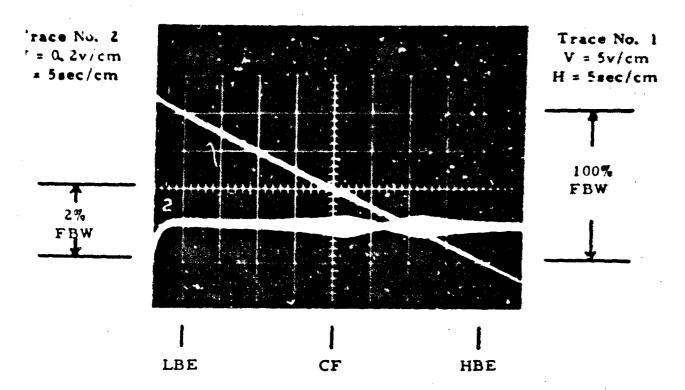
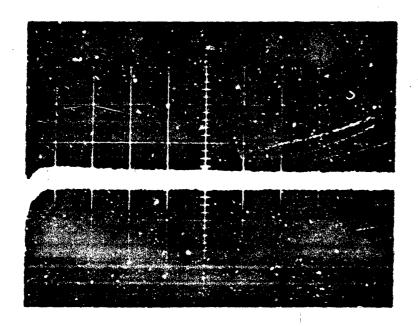


FIGURE 11-3, 3-1
INTERMODULATION TEST BLOCK DIAGRAM



a. Search Channel: 22 kc. 52.5 kc and 30.0 kc at center frequency, all other channels off. RM5 level - 35 mv max.



b. Search Channel: 22 kc. 52.5 kc and 30.0 kc modulated FBW at 0.1 f<sub>m</sub>. All other channels off. RMS level = 12 mv max.

FIGURE II-3.3-2 MODULATION TEST: CALIBRATION AND EXPLANATION OF TECHNIQUE

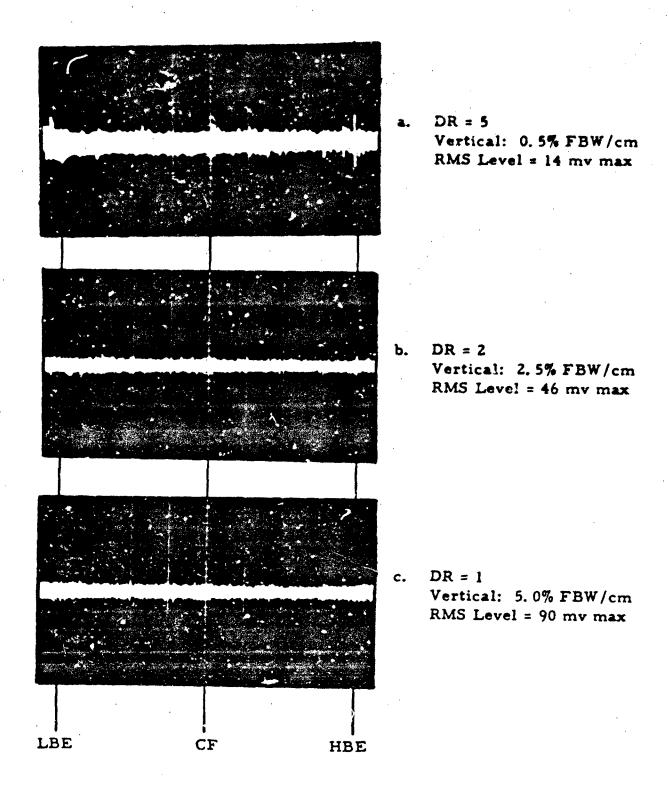
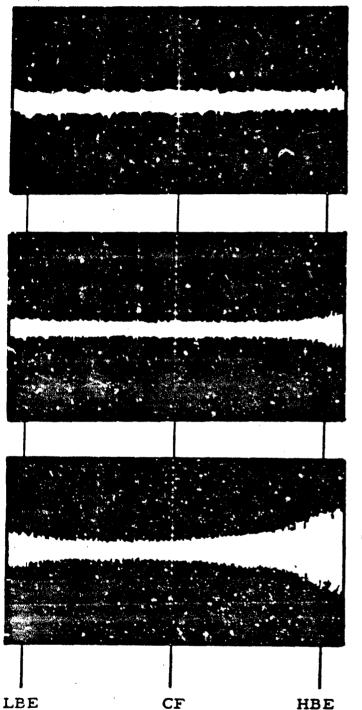


FIGURE II-3.3-3
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 1



a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 11 mv max

b. DR = 2 Vertical: 2.5% FBW/cm RMS Level = 50 mv max

c. DR = 1 Vertical: 5.0% FBW/cm RMS Level = 300 mv max

FIGURE II-3.3-4
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 2

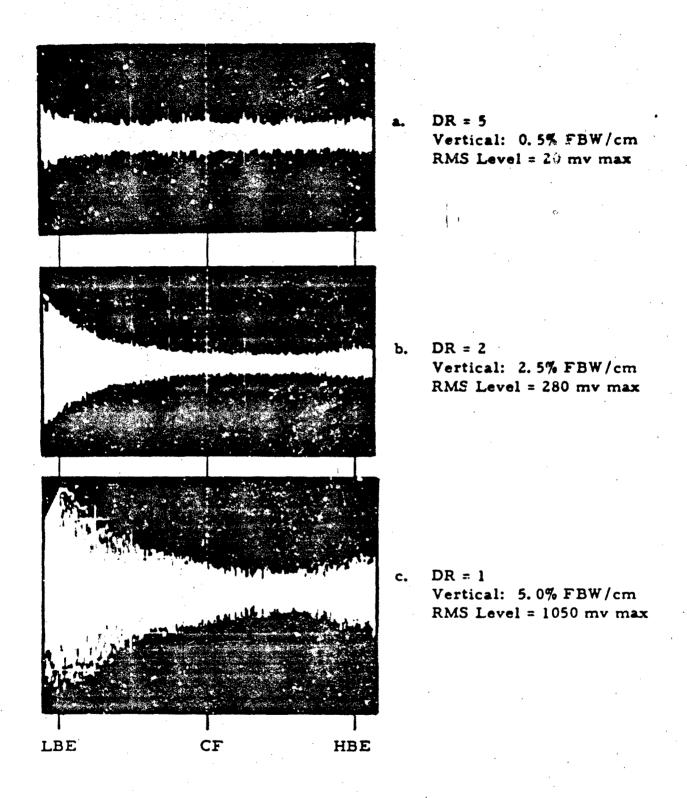
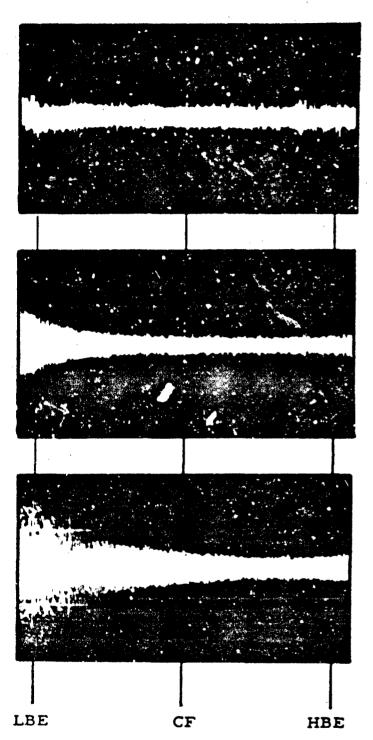


FIGURE II-3.3-5
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5 2, AND 1; CHANNEL 3



a. DR = 5 Vertical: C. 5% FBW/cm RMS Level = 15 mv max

b. DR = 2Vertical: 2.5% FBW/cmRMS Level = 130 mv max

vertical: 5.0% FBW/cm RMS Level = 630 mv max

FIGURE II-3.3-6
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 4

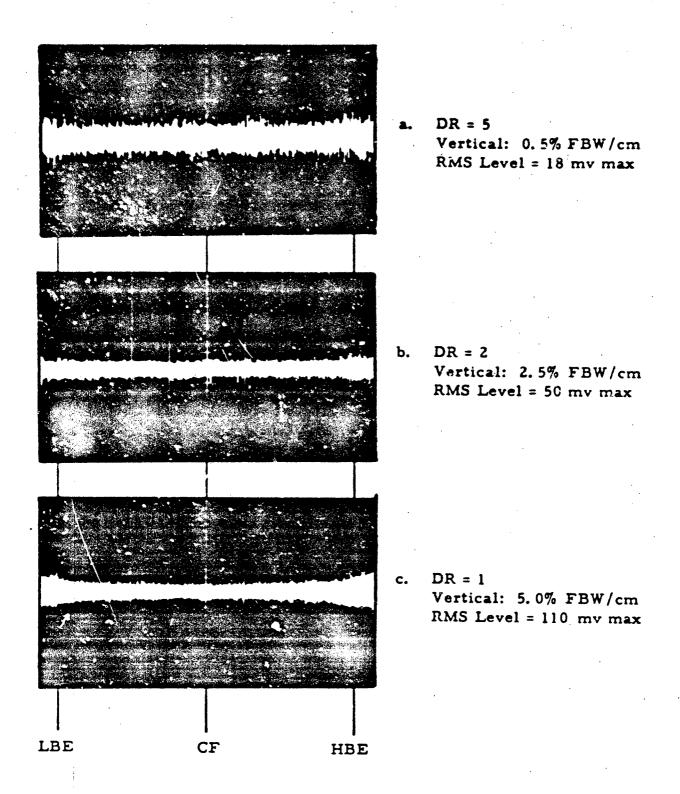
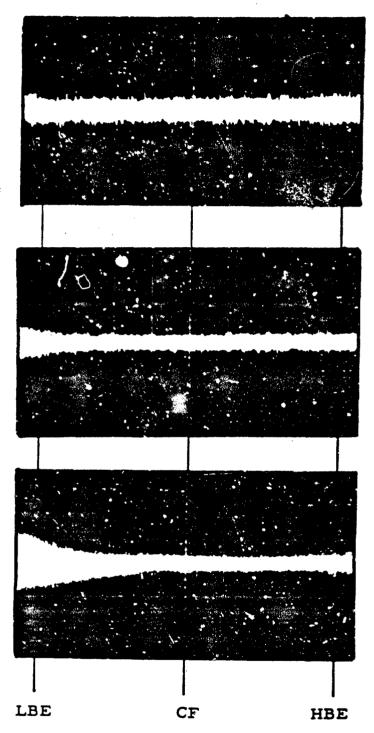


FIGURE II-3.3-7
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 5



a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 15 mv max

b. DR = 2
Vertical: 2.5% FBW/cm
RMS Level = 55 mv max

c. DR = 1 Vertical: 5.0% FBW/cm RMS Level = 240 mv max

FIGURE II-3.3-8
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 6

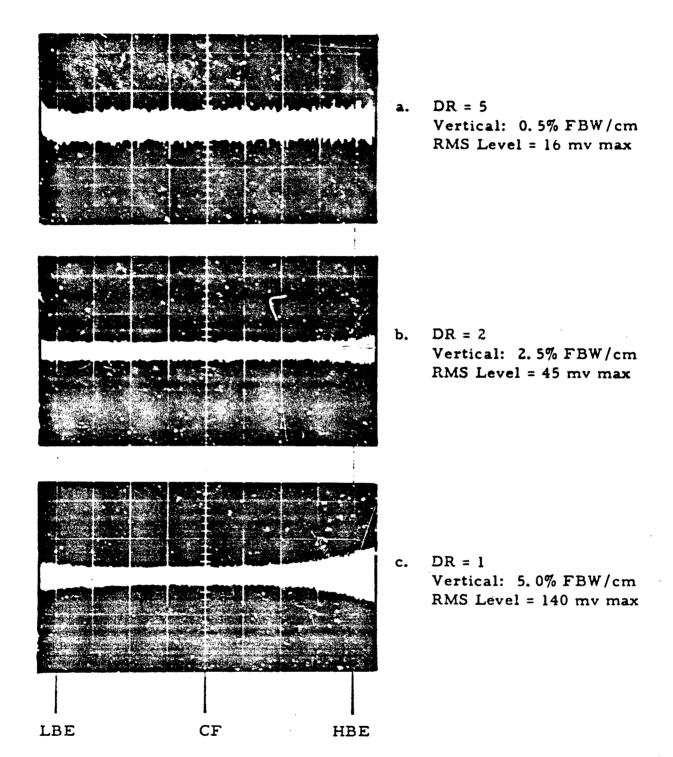
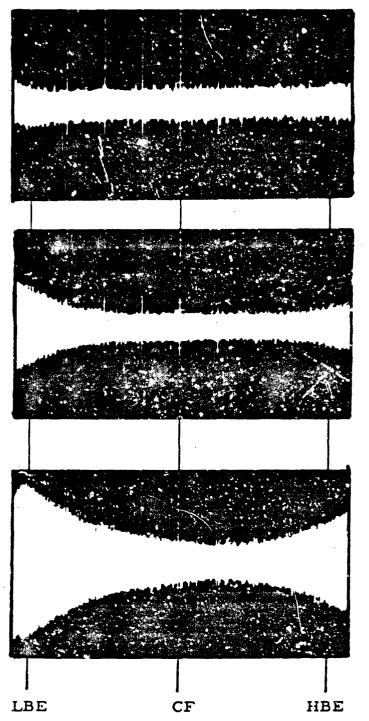


FIGURE II-3.3-9
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 7

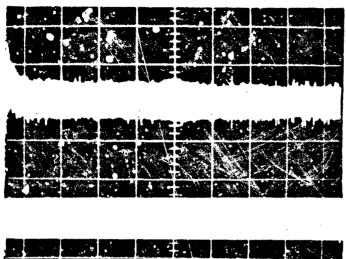


a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 15.5 mv max

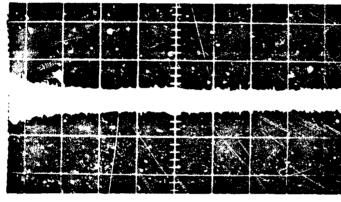
b. DR = 2
Vertical: 2.5% FBW/cm
RMS Level = 170 mv max

c. DR = 1 Vertical: 5.0% FDW/cm RMS Level = 680 mv max

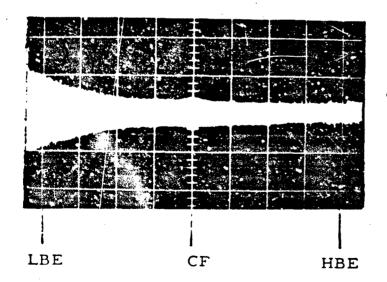
FIGURE II-3. 3-10
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 8



a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 17 mv max

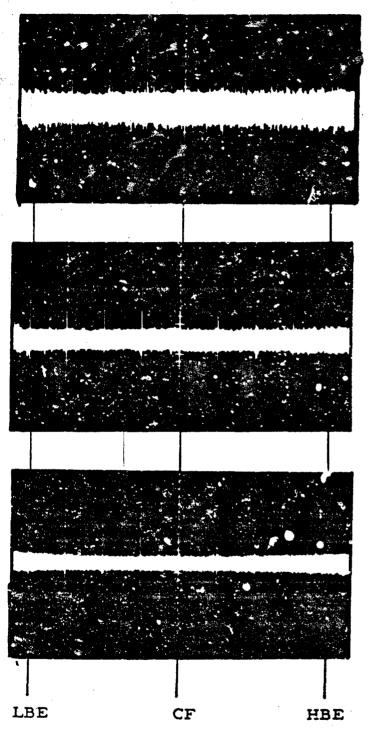


b. DR = 2 Vertical: 2.5% FBW/cm RMS Level = 75 mv max



c. DR = 1 Vertical: 5.0% FBW/cm RMS Level = 300 mv max

FIGURE II-3. 3-11
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 9

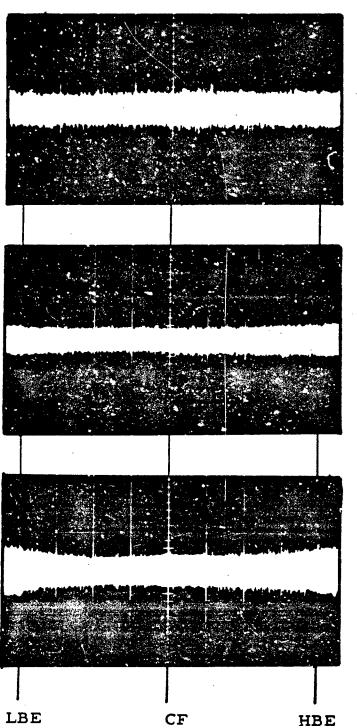


a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 18 mv max

b. DR = 2Vertical: 2.5% FBW/cmRMS Level = 53 mv max

c. DR = 1 Vertical: 5.0% FBW/cm RMS Level = 85 mv max

FIGURE II-3.3-12
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 10

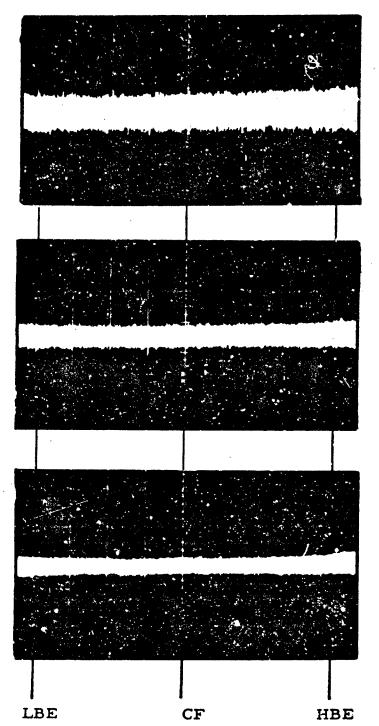


a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 17 mv max

b. DR = 2
Vertical: 2.5% FBW/cm
RMS Level: 70 mv max

c. DR = 1 Vertical: 5.0% FBW/cm RMS Level: 170 mv max

FIGURE II-3.3-13
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 11



a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 19 mv max

DR = 2Vertical: 2.5% FBW/cmRMS Level = 55 mv max

c. DR = 1
Vertical: 5.0% FBW/cm
RMS Level = 90 mv max

FIGURE II-3.3-14
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 12

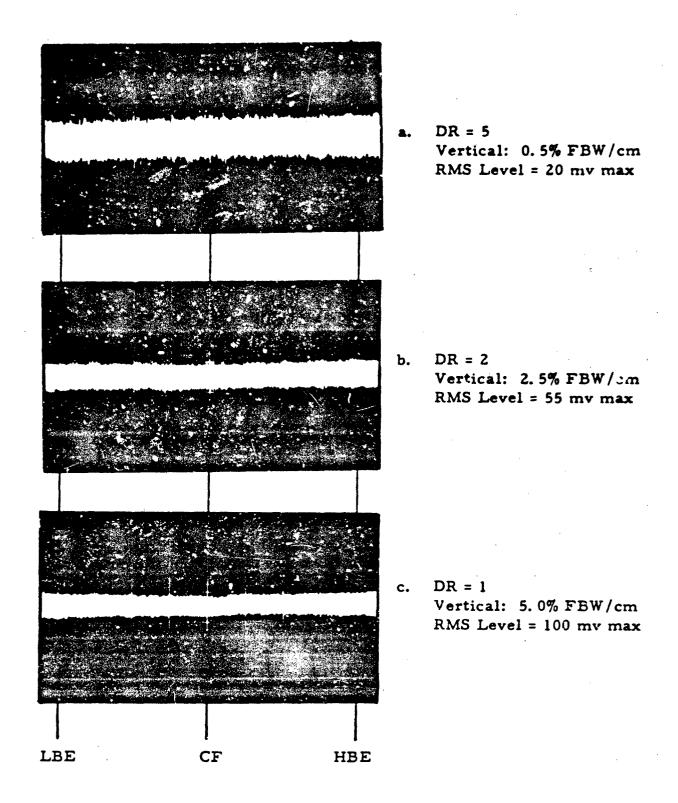


FIGURE II-3. 3-15 INTERMODULATION TEST: IRIG MULTIPLEX; SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 13

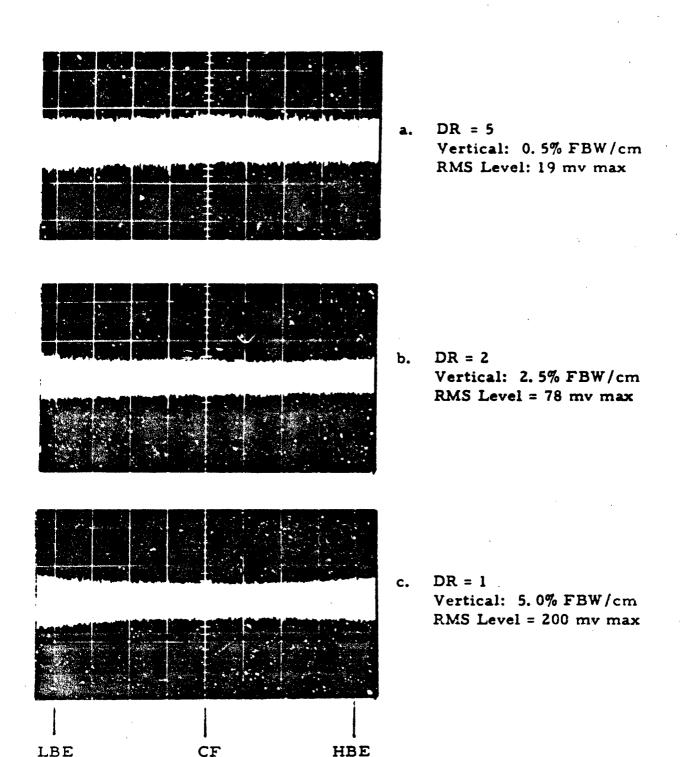


FIGURE II-3. 3-16
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 14

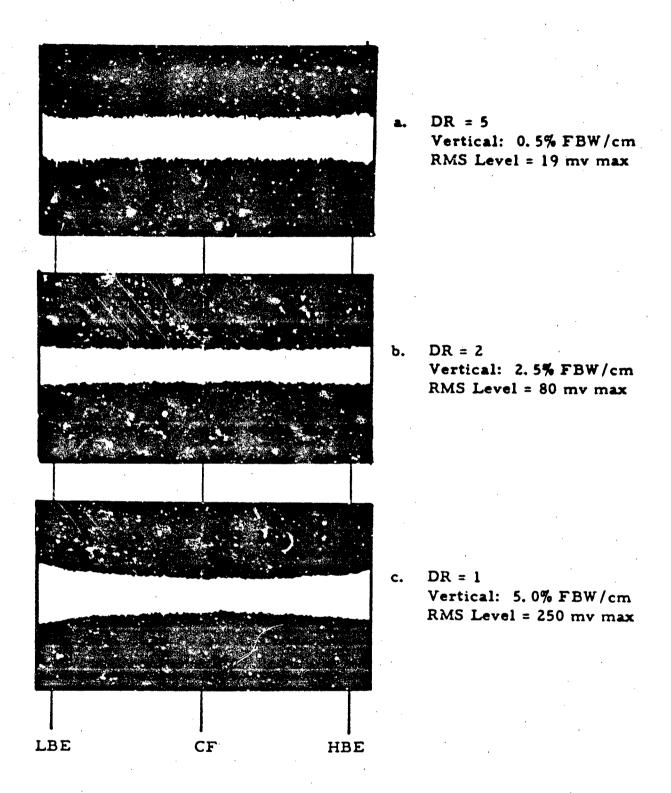
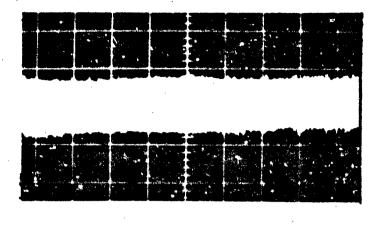
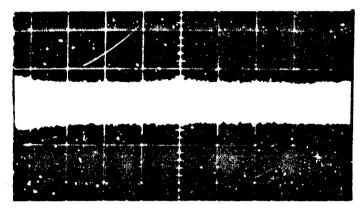


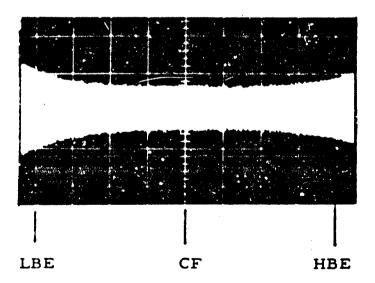
FIGURE II-3. 3-17
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 15



a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 19.5 mv max

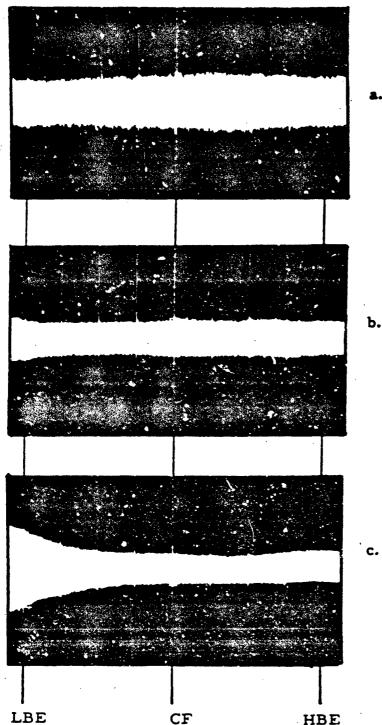


b. DR = 2 Vertical: 2.5% FBW/cm RMS Level = 90 mv max



c. DR = 1 Vertical: 5.0% FBW/cm RMS Level = 350 mv max

FIGURE II-3. 3-18
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 16

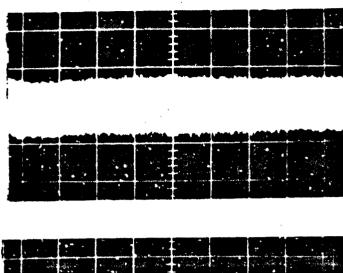


a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 25 mv max

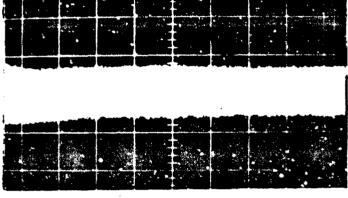
b. DR = 2 Vertical: 2.5% FBW/cm RMS Level = 80 mv max

c. DR = 1 Vertical: 5.0% FBW/cm RMS Level = 300 mv max

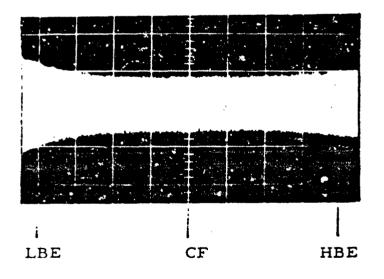
FIGURE II-1.3-19
INTERMODULATION TEST: IRIC MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 17



a. DR = 5 Vertical: 0.5% FBW/cm RMS Level = 21 mv max

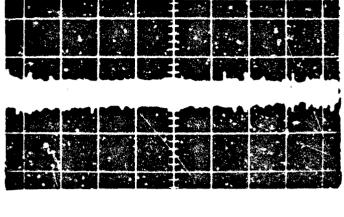


b. DR = 2
Vertical: 2.5% FBW/cm
RMS Level = 90 mv max

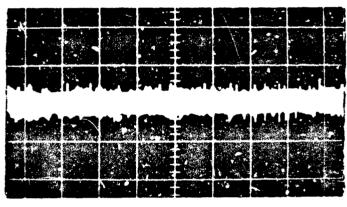


c. DR = 1
Vertical: 5.0% FBW/cm
RMS Level = 350 mv max

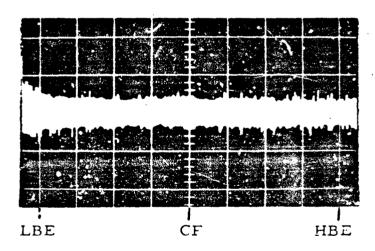
FIGURE II-3. 3-20
INTERMODULATION TEST: IRIG MULTIPLEX;
SEARCH CHANNEL DR = 5, 2, AND 1; CHANNEL 18



Channel 1, 400 cps  $\pm 7.5\%$ DR = 5 RMS Level = 28 mv max.



Channel 2, 560 cps  $\pm$ 7.5% DR = 5 RMS Level = 23 mv max.

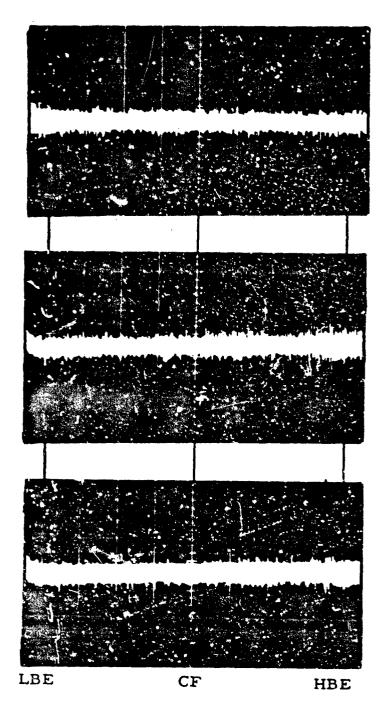


Channel 3, 730 cps DR = 5 RMS Level = 26 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-21
INTERMODULATION TEST: IRIG WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 1, 2, AND 3



Channel 4, 960 cps  $\pm$ 7.5% DR = 5 RMS Level = 15 mv max.

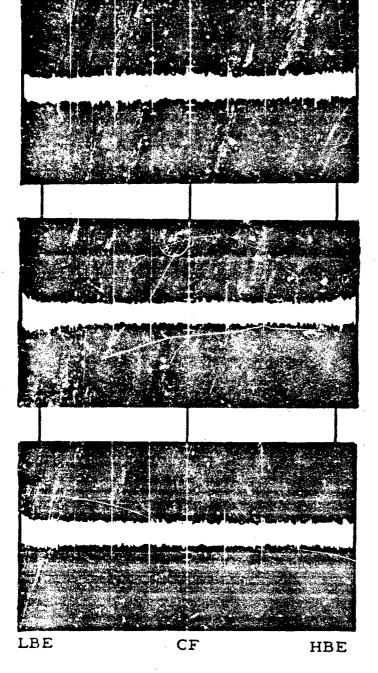
Channel 5, 1.3 kc  $\pm$ 7.5% DR = 5 RMS Level = 18 mv max.

Channel 6, 1.7 kc  $\pm$ 7.5% DR = 5 RMS Level = 15 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3. 3-22
INTERMODULATION TEST: IRIG WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 4, 5, AND 6



Channel 7, 2.3 kc  $\pm$ 7.5% DR = 5 RMS Level = 14 mv max.

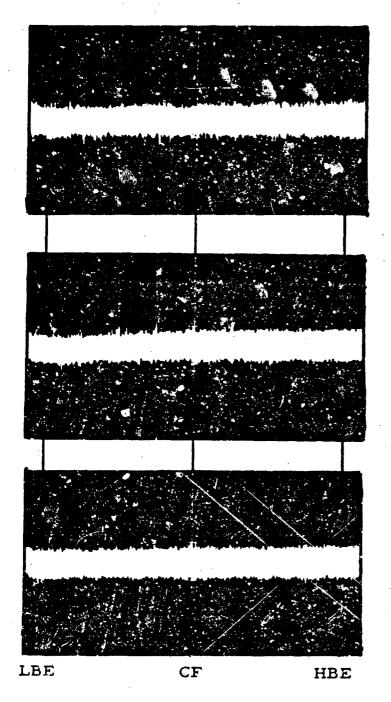
Channel 8, 3 kc  $\pm$ 7.5% DR = 5 RMS Level = 12 mv max.

Channel 9, 3. 9 kc ±7. 5% DR = 5 RMS Level = 12. 5 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-23
INTERMODULATION TEST: IRIG WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 7, 8, AND 9



Channel 10, 5.4 kc ±7.5% DR = 5 RMS Level = 17.5 mv max.

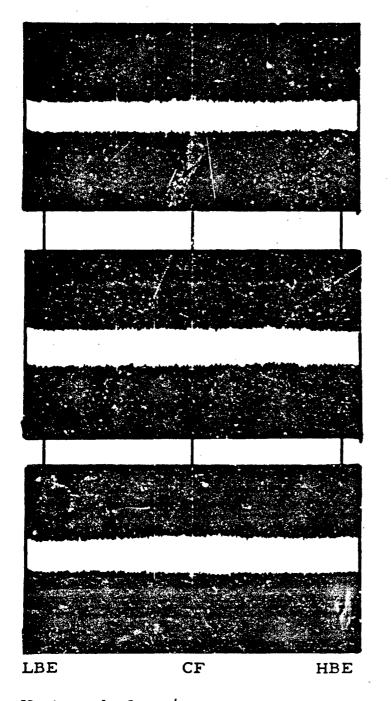
Channel 11, 7.35 kc  $\pm$ 7.5% DP = 5 RMS Level = 16.5 mv max.

Channel 12, 10.5 kc  $\pm$ 7.5% DR = 5 RMS Level = 17 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3. 3-24
INTERMODULATION TEST: IRIG WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 10, 11, AND 12



Channel 13, 14.5 kc ±7.5% DR = 5 RMS Level = 15 mv max.

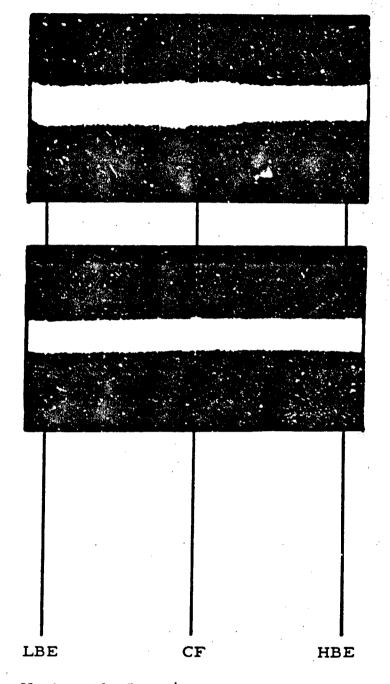
Channel 14, 22 kc ±7.5% DR = 5 RMS Level = 17 mv max.

Channel 15, 30 kc ±7.5% DR = 5 RMS Level = 19 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-25
INTERMODULATION TEST: IRIG WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 13, 14, AND 15



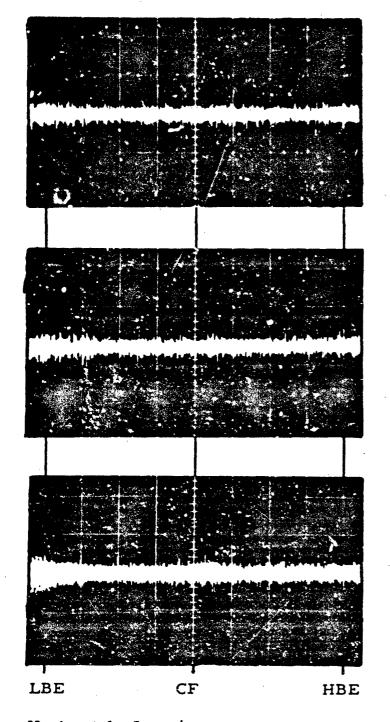
Channel 16, 40 kc ±7.5% DR = 5 RMS Level = 25 mv max.

Channel E, 70 kc ±15% DR = 5 RMS Level = 16.5 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3. 3-26
INTERMODULATION TEST: IRIG WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 16 AND E



Channel 1, 400 cps  $\pm$ 7.5% DR = 5 RMS Level = 20 mv max.

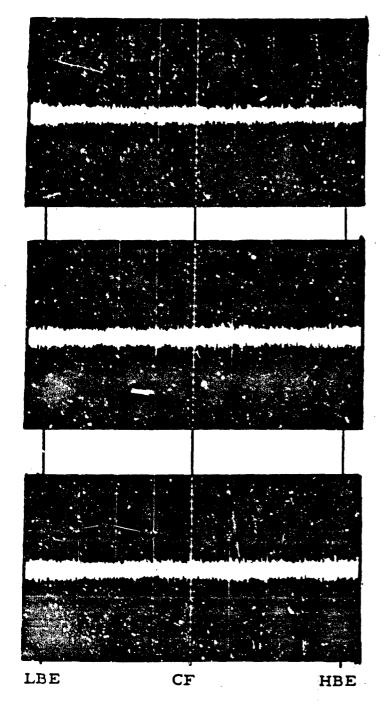
Channel 2, 560 cps  $\pm$ 7.5% DR = 5 RMS Level = 25 mv max.

Channel 3, 730 cps  $\pm$ 7.5% DR = 5 RMS Level = 18 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-27
INTERMODULATION TEST: EXPANDED MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 1, 2, AND 3



Channel 4, 960 cps  $\pm$ 7, 5% DR = 5 RMS Level = 13 mv max.

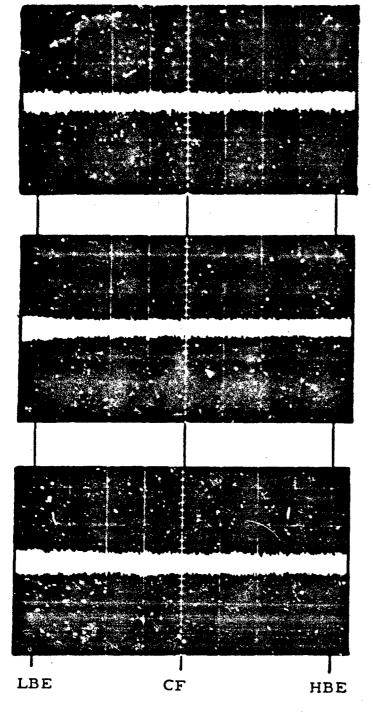
Channel 5, 1.3 kc  $\pm$ 7.5% DR = 5 RMS Level = 20 r v max.

Channel 6, 1.7 kc  $\pm$ 7.5% DR = 5 RMS Level = 18 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3. 3-28
INTERMODULATION TEST: EXPANDED MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 4, 5, AND 6



Channel 7, 2.3 kc ±7.5% DR = 5 RMS Level = 15 mv max.

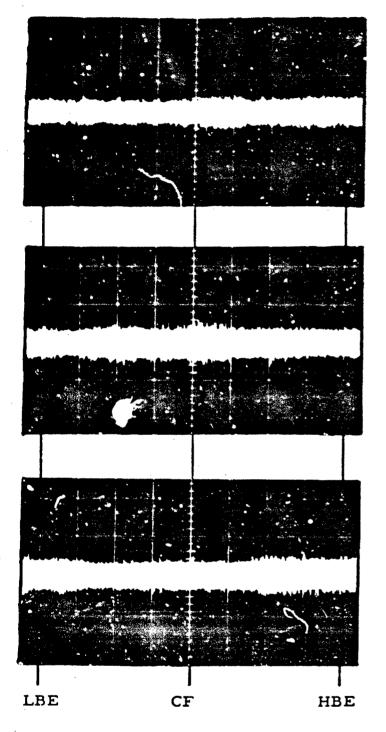
Channel 8, 3.0 kc  $\pm$ 7.5% DR = 5 RMS Level = 15 mv max.

Channel 9, 3.9 kc  $\pm$ 7.5% DR = 5 RMS Level = 15 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-29
INTERMODULATION TEST: EXPANDED MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 7, 8, AND 9



Channel 10, 5.4 kc ±7.5% DR = 5 RMS Level = 19 mv max.

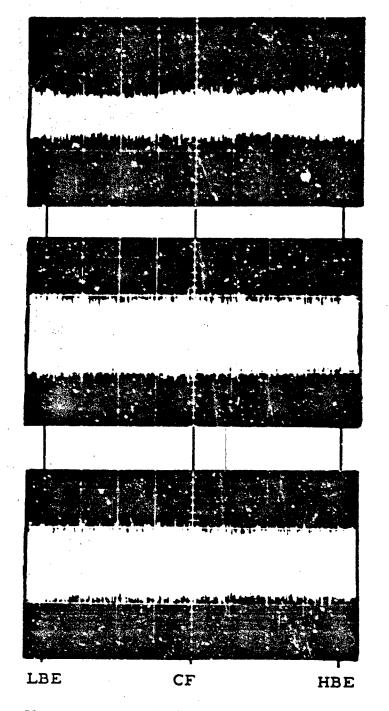
Channel 11, 7.35 kc ±7.5% DR = 5 RMS Level = 18 mv max.

Channel 12, 10.5 kc ±7.5% DR = 5 RMS Level = 19 mv max.

Horizontal: 5sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-30
INTERMODULATION TEST: EXPANDED MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 10, 11, AND 12



Channel 13, 14.5 kc ±7.5% DR = 5 RMS Level = 24 mv max.

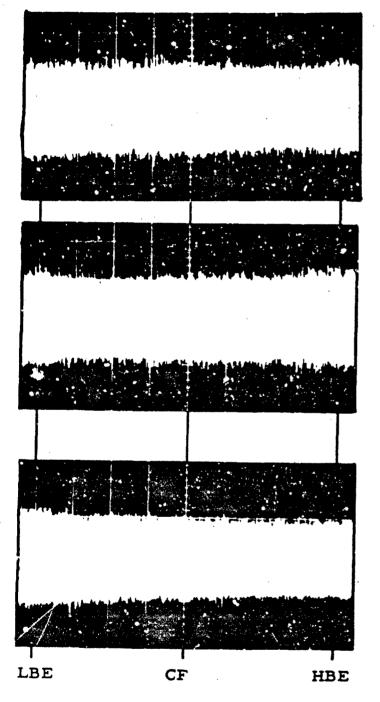
Channel 14, 22.0 kc ±7.5% DR = 5 RMS Level = 31 mv max.

Channel 15, 30.0 kc  $\pm$ 7.5% DR = 5 RMS Level = 32 my max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-31
INTERMODULATION TEST: EXPANDED MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 13, 14, AND 15



Channel 16, 40.0 kc  $\pm$ 7.5% DR = 5 RMS Level = 35 mv max.

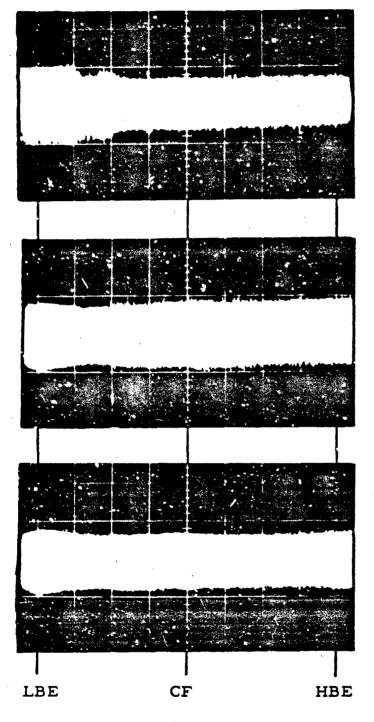
Channel 17, 52.5 kc  $\pm$ 7.5% DR = 5 RMS Level = 36 mv max.

Channel 18, 70.0 kc  $\pm$ 7.5% DR = 5 RMS Level = 31 mv max.

Horizontal: 5 sec/cm.

Vertical: 0.5% FBW/cm

FIGURE II-3.3-32
INTERMODULATION TEST: EXPANDED MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 16, 17, AND 18



Channel 19, 93.0 kc  $\pm$ 7.5% DR = 5 RMS Level = 27 mv max.

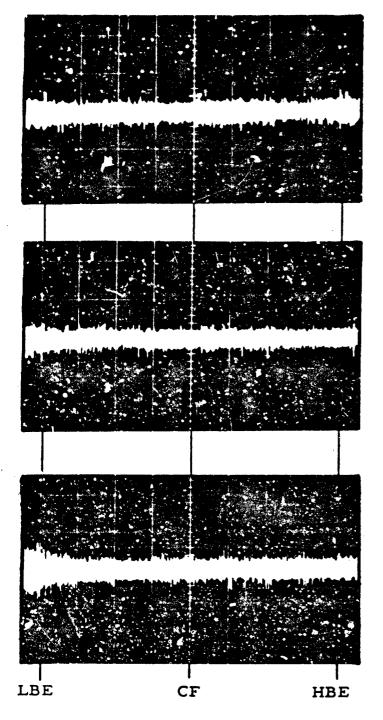
Channel 20, 124.0 kc ±7.5% DR = 5 RMS Level = 26 my max.

Channel 21, 165. 0 kc  $\pm$ 7. 5% DR = 5 RMS Level = 21 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-33
INTERMODULATION TEST: EXPANDED MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 19, 20, AND 21



Channel 1, 400 cps ±7.5% DR = 5 RMS Level = 24 mv max.

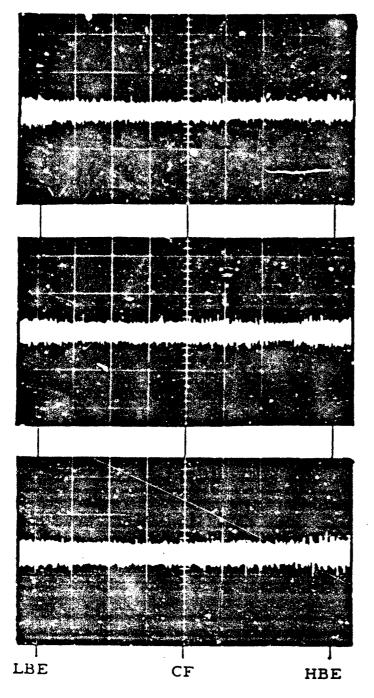
Channel 2, 560 cps ±7.5% DR = 5 RMS Level = 20 mv max.

Channel 3, 730 cps  $\pm$ 7.5% DR = 5 RMS Level = 22 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-34
INTERMODULATION TEST: EXPANDED WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 1, 2, AND 3



Channel 4, 960 cps  $\pm$ 7, 5% DR = 5 RMS Level = 16 mv max.

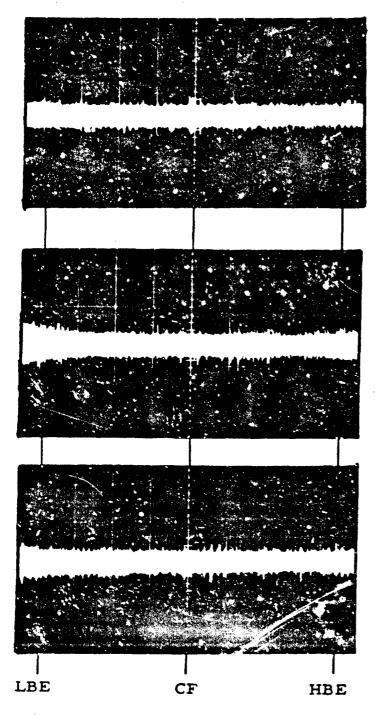
Channel 5, 1.3 kc  $\pm$ 7.5% DR = 5 RMS Level = 16 mv max.

Channel 6, 1.7 kc  $\pm$ 7.5% DR = 5 RMS Level = 15 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3. 3-35
INTERMODULATION TEST: EXPANDED WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 4, 5, AND 6



Channel 7, 2.3 kc  $\pm$ 7, 5% DR = 5 RMS Level = 17 mv max.

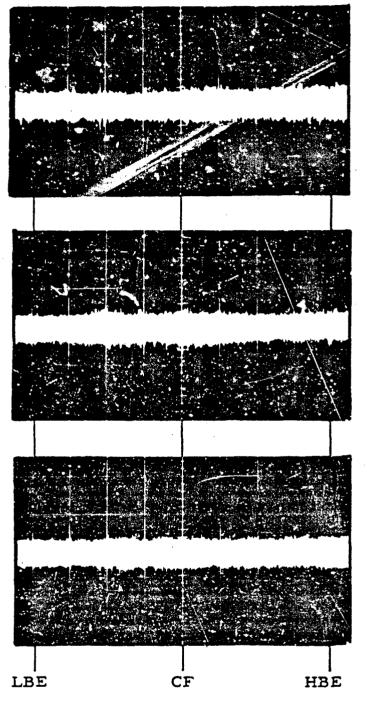
Channel 8, 3.0 kc  $\pm$ 7.5% DR = 5 RMS Level = 15 mv max.

Channel 9, 3. 9 kc  $\pm$ 7. 5% DR = 5 RMS Level = 16 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-36
INTERMODULATION TEST: EXPANDED WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 7, 8, AND 9



Horizontal: 5 sec/cm

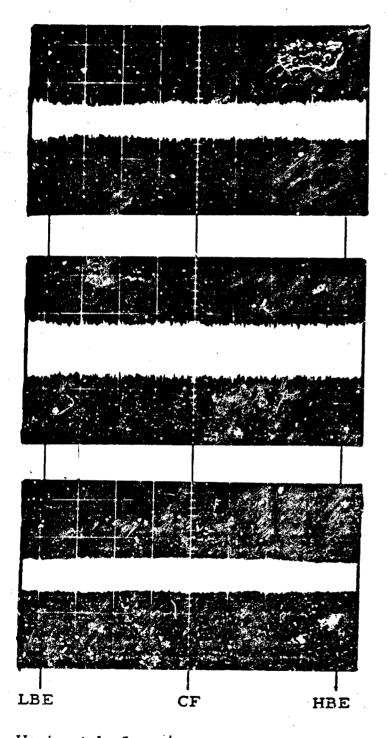
Channel 10, 5.4 kc ±7.5% DR = 5 RMS Level = 18 mv max.

Channel 11, 7.35 kc  $\pm$ 7.5% DR = 5 RMS Level = 18 mv max.

Channel 12, 10.5 kc ±7.5% DR = 5 RMS Level = 16 mv max.

Vertical: 0.5% BW/cm

FIGURE II-3.3-37
INTERMODULATION TEST: EXPANDED WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 10, 11, AND 12



Channel 13, 14.5 kc  $\pm$ 7.5% DR = 5 RMS Level = 20 mv max.

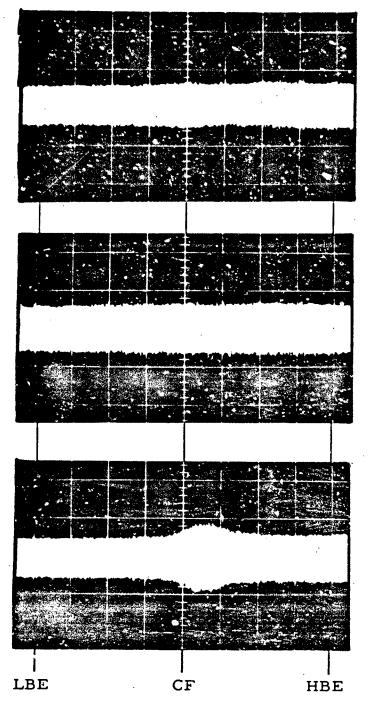
Channel 14, 22 kc  $\pm$ 7.5% DR = 5 RMS Level = 27 mv max.

Channel 15, 30 kc  $\pm$ 7.5% DR = 5 RMS Level = 22 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3. 3-38
INTERMODULATION TEST: EXPANDED WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 13, 14, AND 15



Channel 16, 40 kc ±7.5% DR = 5 RMS Level = 23 mv max.

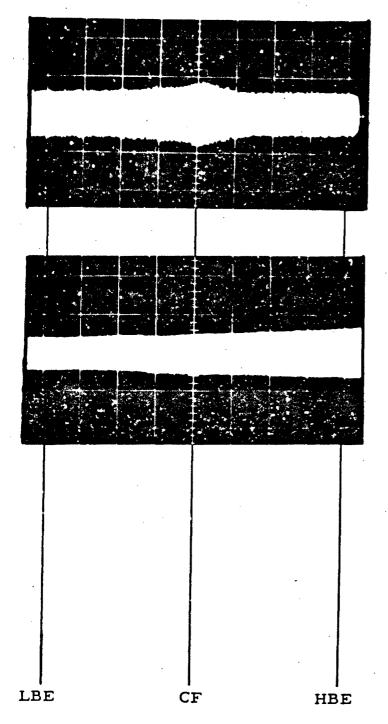
Channel 17, 52.5 kc ±7.5% DR = 5 RMS Level = 24 mv max.

Channel 18, 70 kc  $\pm$ 7.5% DR = 5 RMS Level = 30 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3.3-39
INTERMODULATION TEST: EXPANDED WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNELS 16, 17, AND 18



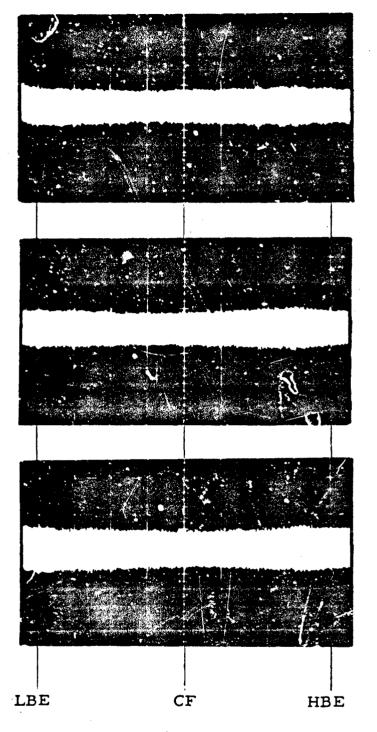
Channel 19, 93 kc  $\pm$ 7.5% DR = 5 RMS Level = 25 mv max.

Channel H, 165 kc ±15% DR = 5 RMS Level = 25 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

FIGURE II-3. 3-40
INTERMODULATION TEST: EXPANDED WIDEBAND MULTIPLEX;
SEARCH CHANNEL DR = 5; CHANNEL 19 AND H



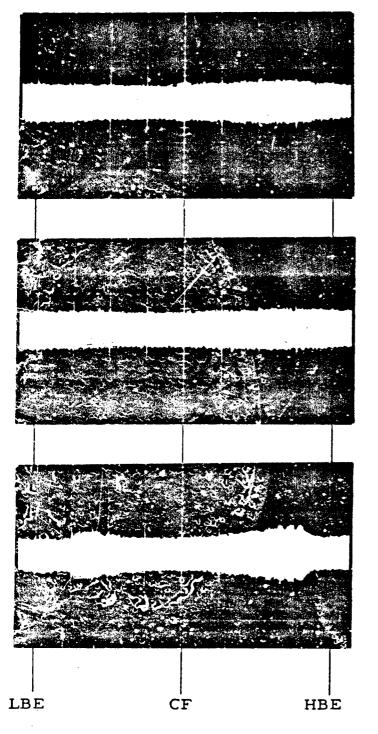
Channel 1, 16.0 kc ±2 kc RMS Level - 86 mv max.

Channel 2, 24.0 kc ±2 kc RMS Level = 94 mv max.

Channel 3, 32.0 kc ±2 kc RMS Level = 110 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-41
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;
SEARCH CHANNEL DR = 2; CHANNELS 1, 2, AND 3



Channel 4, 40.0 kc ±2 kc RMS Level = 97 mv max.

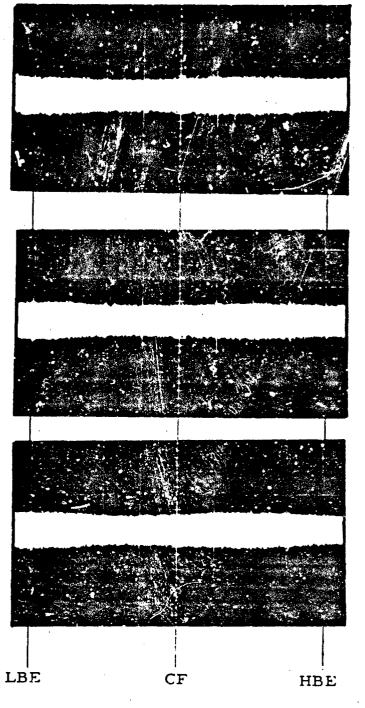
Channel 5, 48.0 kc ±2 kc RMS Level = 94 mv max.

Channel 6, 56.0 kc ±2 kc

RMS Level = 140 mv max.

Horizontal: 5 sec/cm Vertical: 2.5% FBW/cm

FIGURE II-3.3-42
VTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;
SEARCH CHANNEL DR = 2; CHANNELS 4, 5, AND 6



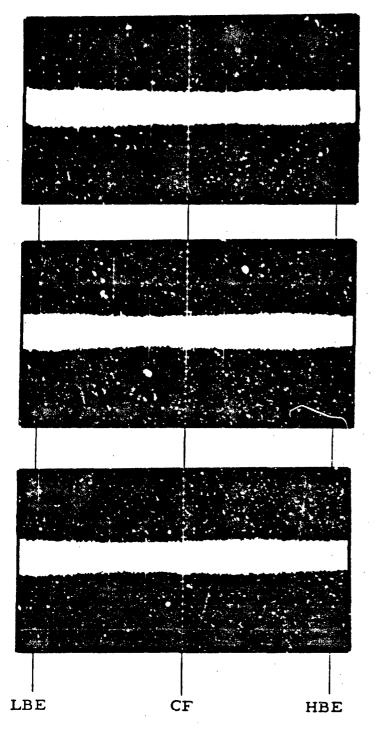
Channel 7, 64.0 kc ±2 kc RMS Level = 86 mv max.

Channel 8, 72.0 kc  $\pm$ 2 kc RMS Level = 85 mv max.

Channel 9, 80.0 kc  $\pm$ 2 kc RMS Level = 86 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-43
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;
SEARCH CHANNEL DR = 2; CHANNELS 7, 8, and 9



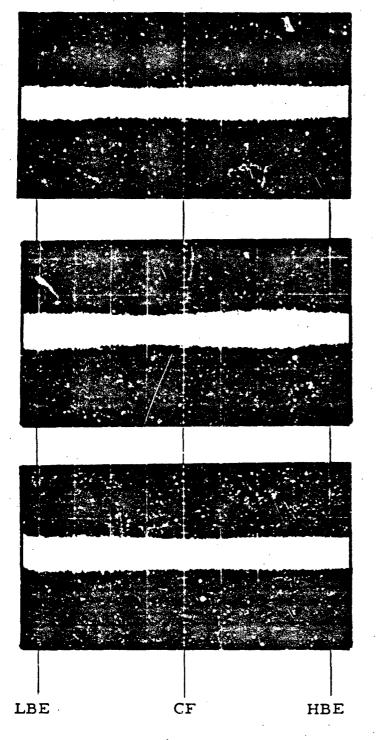
Channel 10, 88.0 kc ±2 kc RMS Level = 89 mv max.

Channel 11, 96.0 kc ±2 kc RMS Level = 87 mv max.

Channel 12, 104.0 kc ±2 kc RMS Level = 86 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-44
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI =20;
SEARCH CHANNEL DR = 2; CHANNELS 10, 11, AND 12



Channel 13, 112.0 kc ±2 kc RMS Level = 81 mv max.

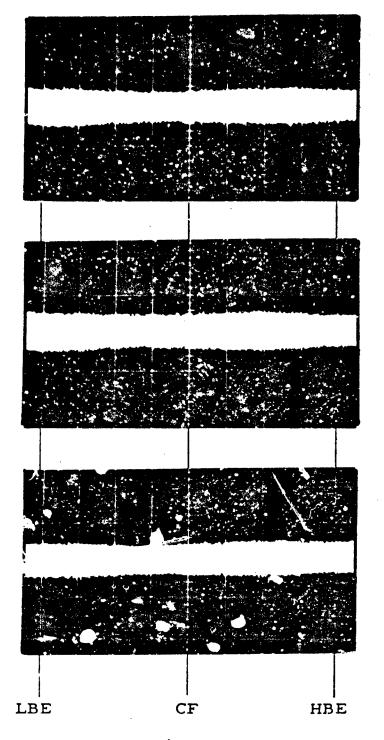
Channel 14, 120.0 kc ±2 kc RMS Level = 90 mv max.

Channel 15, 128.0 kc ±2 kc

RMS Level = 83 mv max.

Horizontal: 5 sec/cm

FIGURE II-3, 3-45
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;
SEARCH CHANNEL DR = 2; CHANNELS 13, 14, AND 15



Channel 16, 136.0 kc ±2 kc RMS Level = 85 mv max.

Channel 17, 144. 0 kc ±2 kc RMS Level = 86 mv max.

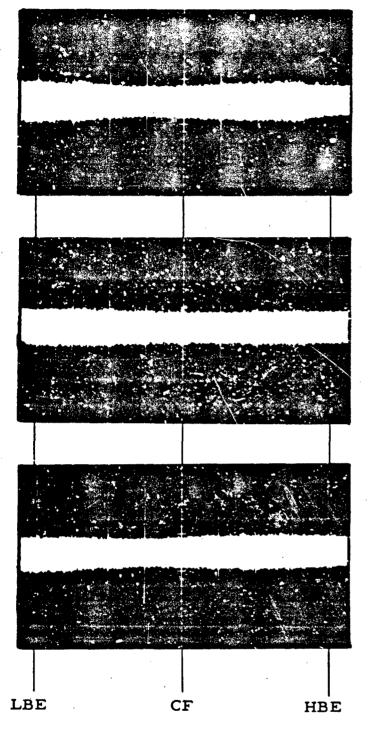
Channel 18, 152. 0 kc ±2 kc RMS Level = 81 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-46

NTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;

SEARCH CHANNEL DR = 2; CHANNELS 16, 17, AND 18



Channel 19, 160. 0 kc ±2 kc RMS Level = 91 mv max.

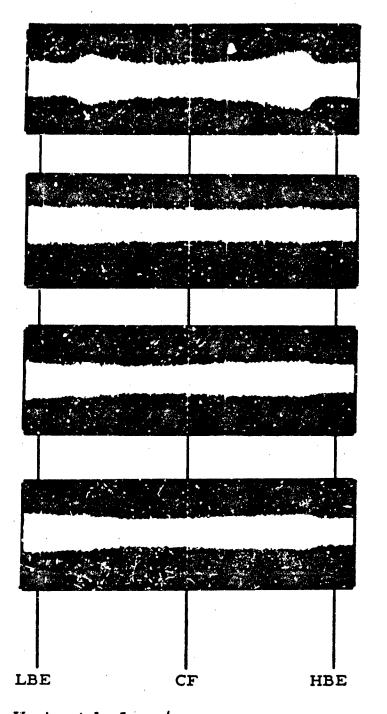
Channel 20, 168. 0 kc  $\pm$ 2 kc RMS Level = 85 mv max.

Channel 21, 176. 0 kc ±2 kc

RMS Level = 82 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-47
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;
SEARCH CHANNEL DR = 2; CHANNELS 19, 20, AND 21



Channel 6: 56.0 kc  $\pm$ 2 kc

RMS Level = 152 mv max.

Channel 10: 88. 0 kc ±2 kc

RMS Level = 93 mv max.

Channel 14: 120.0 kc ±2 kc

RMS Level = 92 mv max.

Channel 19:  $160.0 \text{ kc} \pm 2 \text{ kc}$ 

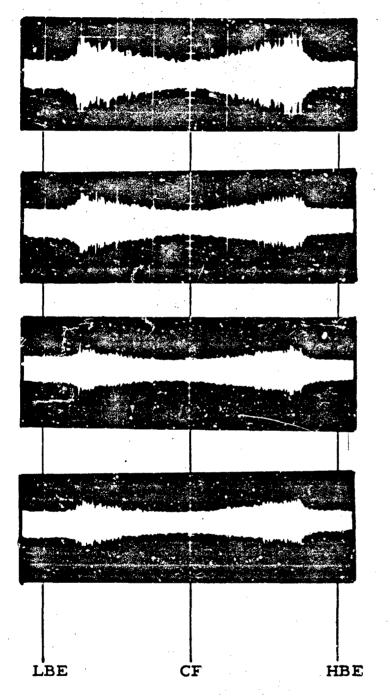
RMS Level = 94 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-48

INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 2;

SEARCH CHANNEL DR = 2; CHANNELS 6, 10, 14, AND 19



Channel 6, 56.0 kc ±2 kc RMS Level = 200 mv max.

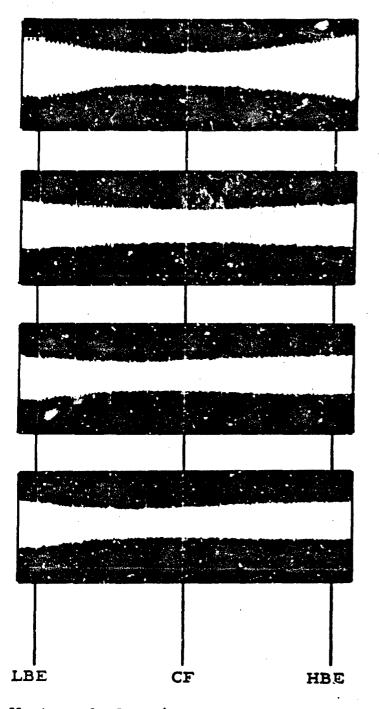
Channel 10, 88.0 kc ±2 kc RMS Level = 128 my max.

Channel 14, 120.0 kc ±2 kc RMS Level = 120 mv max.

Channel 19, 160. 0 kc ±2 kc RMS Level = 106 mv max.

Horizontal: 5 sec/cm Vertical: 2.5% FBW/cm

FIGURE II-3.3-49
INTERMODULATION TEST: CONSTANT BANDWIDTH MULTIPLEX,
VCO'S AT CENTER FREQUENCY; SEARCH CHANNEL DR = 2;
CHANNELS 6, 10, 14, AND 19



Channel 6: 56.0 kc ±2 kc

RMS Level = 285 mv max.

Channel 10: 88. 0 kc ±2 kc

RMS Level = 205 mv max.

Channel 14: 120.0 kc ±2 kc

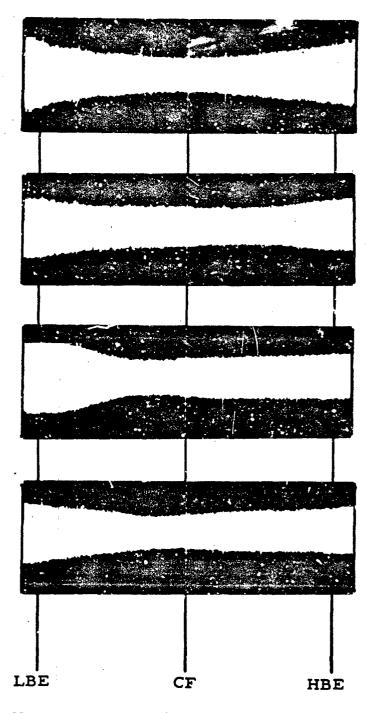
RMS Level = 200 mv max.

Channel 19:  $160.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 210 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-50
VTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;
SEARCH CHANNEL DR = 1; CHANNELS 6, 10, 14, AND 19



Channel 6:  $56.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 330 mv max.

Channel 10: 88.0 kc ±2 kc

RMS Level = 310 mv max

Channel 14:  $120.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 440 mv max

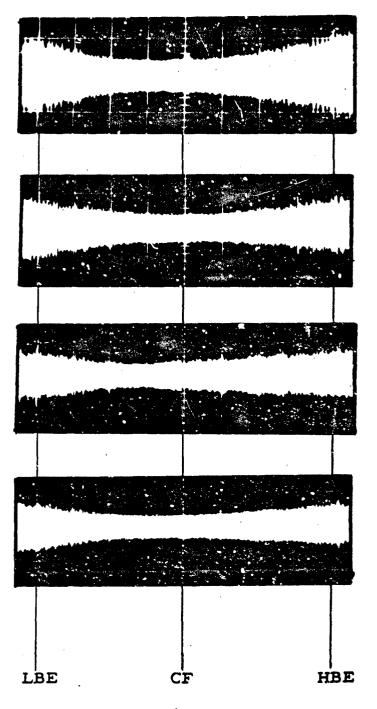
Channel 19: 160.0 kc ±2 kc

RMS Level = 300 mv max.

Horizontal: 5 sec/cm

Vertical: 5.0% FBW/cm

FIGURE II-3.3-51
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 1;
SEARCH CHANNEL DR = 1; CHANNELS 6, 10, 14, AND 19



Channel 6, 56.0 kc ±2 kc RMS Level = 330 mv max.

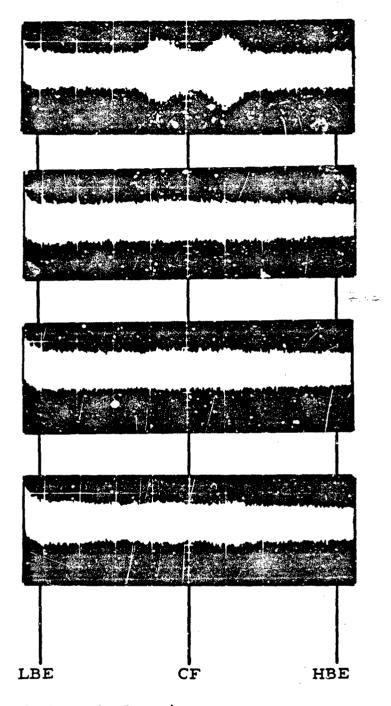
Channel 10, 88.0 kc ±2 kc RMS Level = 260 mv max.

Channel 14, 120, 0 kc ±2 kc RMS Level = 220 mv max.

Channel 19, 160. 0 kc ±2 kc RMS Level = 218 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-52
INTERMODULATION TEST: CONSTANT BANDWIDTH MULTIPLEX,
VCO'S AT CENTER FREQUENCY; SEARCH CHANNEL DR = 1;
CHANNELS 6, 10, 14, AND 19



Channel 6: 56.0 kc  $\pm$ 2 kc

RMS Level = 34 mv max.

Channel 10: 88. 0 kc ±2 kc

RMS Level = 17.5 mv max.

Channel 14: 120. 0 kc  $\pm$ 2 kc

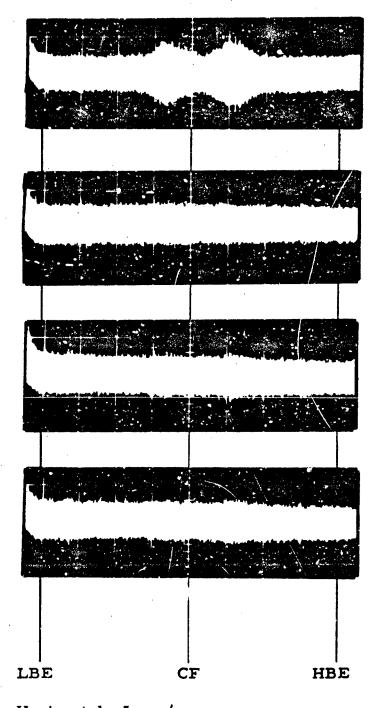
RMS Level = 18.6 mv max.

Channel 19:  $160.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 19.5 mv max.

Horizontal: 5 sec/cm Vertical: 0.5% FBW/cm

FIGURE II-3.3-53
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20;
SEARCH CHANNEL DR = 4; CHANNELS 6, 10, 14, AND 19



Channel 6: 56.0 kc  $\pm$ 2 kc

RMS Level = 32.0 mv max.

Channel 10: 88.0 kc  $\pm$ 2 kc

RMS Level = 18.0 mv max.

Channel 14: 120.0 kc ±2 kc

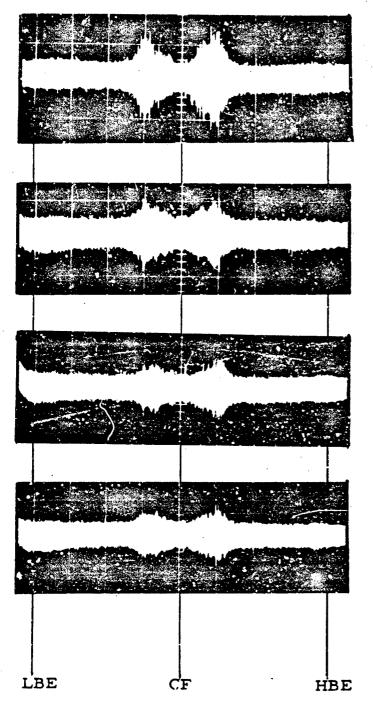
RMS Level = 19.2 mv max.

Channel 19:  $160.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 19.6 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-54
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 4;
SEARCH CHANNEL DR = 4; CHANNELS 6, 10, 14, AND 19



Channel 6, 56.0 kc ±2 kc RMS Level = 40.0 mv max.

Channel 10, 88.0 kc ±2 kc

RMS Level = 26.0 mv max.

Channel 14, 120. 0 kc ±2 kc

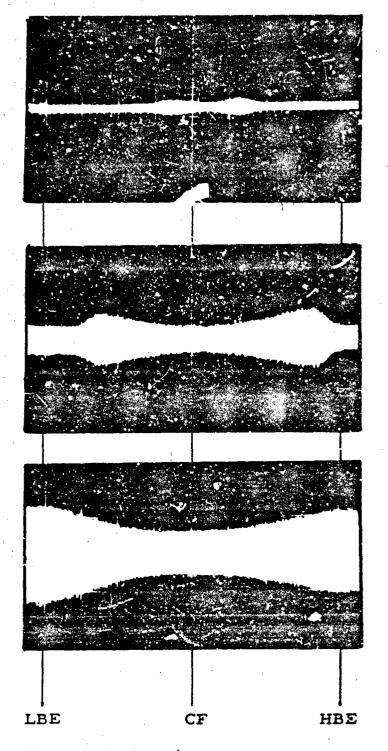
RMS Level = 26. 0 mv max.

Channel 19, 160. 0 kc ±2 kc

RMS Level = 23.6 mv max.

Horizontal: 5 sec/cm

FIGURE II-3.3-55
INTERMODULATION TEST: CONSTANT BANDWIDTH MULTIPLEX,
VCO'S AT CENTER FREQUENCY; SEARCH CHANNEL DR = 4;
CHANNELS 6, 10, 14, AND 19



Channel 6: 56.0 kc  $\pm$ 2 kc DR = 4

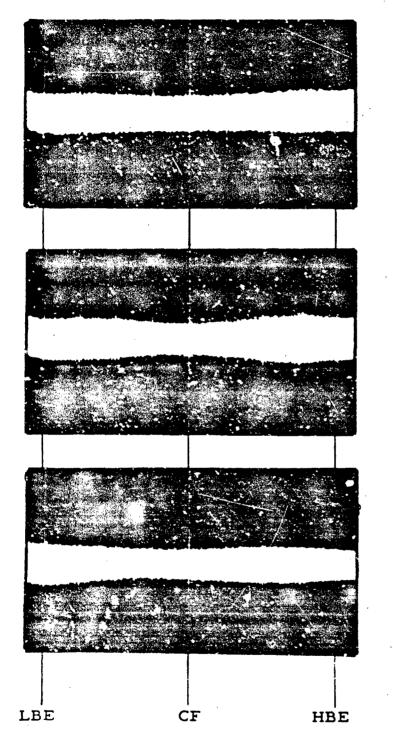
Channel 6: 56. 0 kc ±2 kc DR = 2

Channel 6: 56.0 kc ±2 kc DR = 1

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

FIGURE II-3. 3-56
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX,
DEVIATION RATIO COMPARISON, MI = 20;
SEARCH CHANNEL DR = 4, 2, AND 1; CHANNEL 6



Channel 3: 32.0 kc ±2 kc

RMS Level = 106 mv max.

Channel 6:  $56.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 126 mv max.

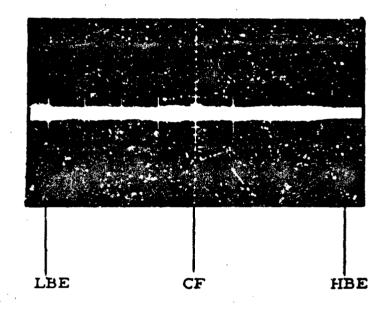
Channel 19:  $160.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 98 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

FIGURE II-3.3-57
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20,
WITH CONSTANT-AMPLITUDE, 18 DB/OCT OUTPUT FILTERS;
SEARCH CHANNEL DR = 2; CHANNELS 3, 6, AND 19



Channel 6, 56.0 kc ±2 kc

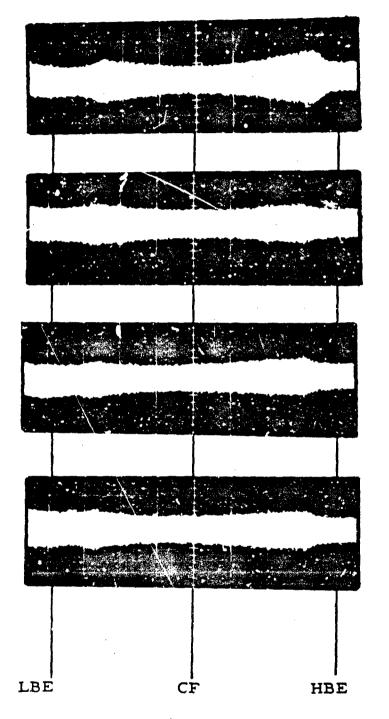
RMS Level = 30 mv

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

FIGURE II-3.3-58

INTERMODULATION TEST: CONSTANT BANDWIDTH MULTIPLEX,
WITH RADIO FREQUENCY EQUIPMENT BYPASSED, MI = 20;
SEARCH CHANNEL DR = 2; CHANNEL 6



Channel 6:  $56.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 138 mv max.

Channel 10: 88.0 kc ±2 kc

RMS Level = 95 mv max.

Channel 14: 120. 0 kc ±2 kc

RMS Level = 95 mv max.

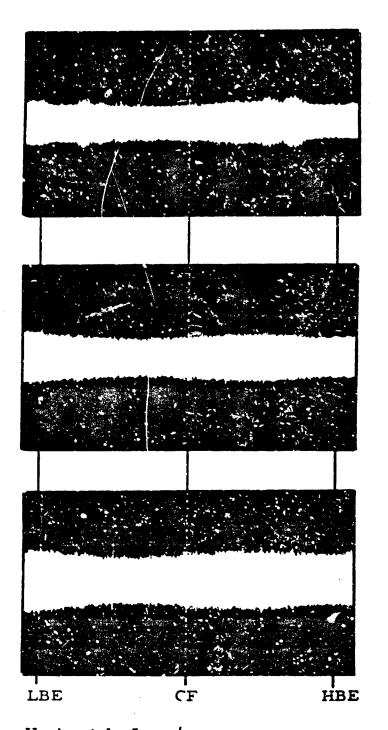
Channel 19:  $160.0 \text{ kc} \pm 2 \text{ kc}$ 

RMS Level = 95 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

FIGURE II-3. 3-59
INTERMODULATION TEST: CONSTANT-BANDWIDTH MULTIPLEX, MI = 20,
USING DEFENSE ELECTRONICS TMR-2A RECEIVER;
SEARCH CHANNEL DR = 2; CHANNELS 6, 10, 14 AND 19



Standard Intermodulation Test: Leach FM 200 replaced by EMR 246A Transmitter RMS Level = 134 my max.

Effect of IF Bandwidth: Nems-Clarke 1455A 500 kc IF replaced with Nems-Clarke Special 1703A 1.0 Mc IF Receiver RMS Level = 118 mv max.

Effect of Uncorrelated VCO Modulation: EMR 246A and 500 kc IF Nems-Clarke 1455A with VCO's individually modulated with 100 cps sources. RMS Level = 132 mv max.

Horizontal: 5 sec/cm

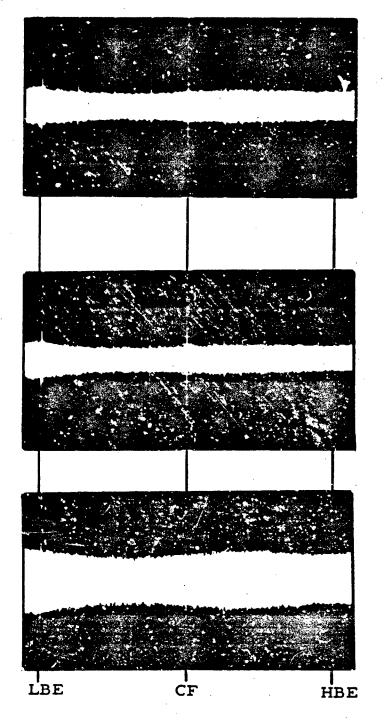
Vertical: 2.5% FBW/cm

Search Channel: CBW Channel 6, 56.0 kc ±2 kc, DR = 2

All Other Channels: MI = 2

FIGURE II-3, 3-60

INTERMODULATION TEST: CONSTANT BANDWIDTH MULTIPLEX USING EMR 246A TRANSMITTER; EFFECTS OF 1.0 MC IF BANDWIDTH AND SEPARATE 100 CPS SOURCES; CBW CHANNEL 6



Error Due to Receiver Noise: Search Channel Only Turned On RMS Level = 72 mv max.

Effect of a Reduced Number of Channels: EMR 246A and 500 kc IF Nems-Clarke 1455A with only 16 lower frequency VCO's individually modulated at 100 cps RMS Level = 60 mv max.

Effect of Reduced Transmitter
Deviation: EMR 246A and 500 kc
IF Nems-Clarke with transmitter
drive reduced by half; all 21
channels individually modulated
at 100 cps
RMS Level = 144 1 17 max.

Horizontal: 5 sec/cm

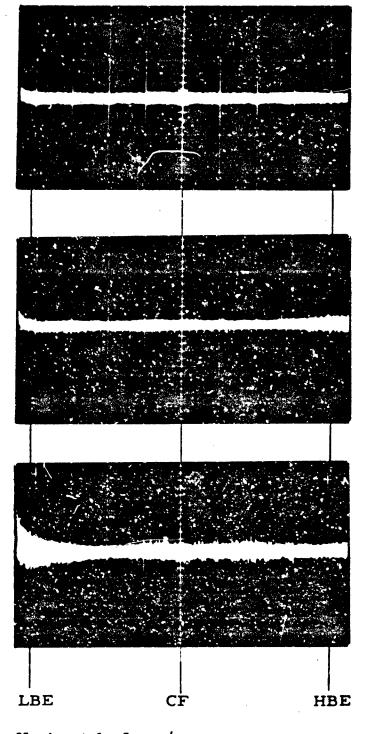
Vertical: 2.5% FBW/cm

Search Channel: CBW Channel 6, 56.0 kc ±2 kc, DR = 2

All Other Channels: MI = 2

FIGURE II-3, 3-61

INTERMODULATION TEST: CONSTANT BANDWIDTH MULTIPLEX USING EMR 246A TRANSMITTER; EFFECTS OF A REDUCED NUMBER OF CHANNELS AND REDUCED TRANSMITTER DRIVE; CBW CHANNEL 6



Channel 1, 0.40 kc  $\pm$ 7.5% RMS Level = 6.1 mv max.

Channel 2, 0. 56 kc ±7. 5%

RMS Level = 6. 2 mv max.

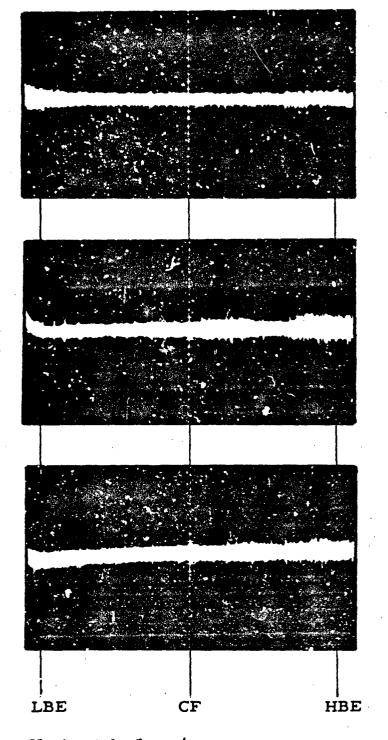
Channel 3, 0.73 kc  $\pm$ 7.5% RMS Level = 15 my max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3. 3-62
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 5; FBW CHANNELS 1, 2, and 3



Channel 4, 0. 96 kc  $\pm$ 7. 5% RMS Level = 9 mv max.

Channel 5, 1.30 kc  $\pm$ 7.5% RMS Level = 12 mv max.

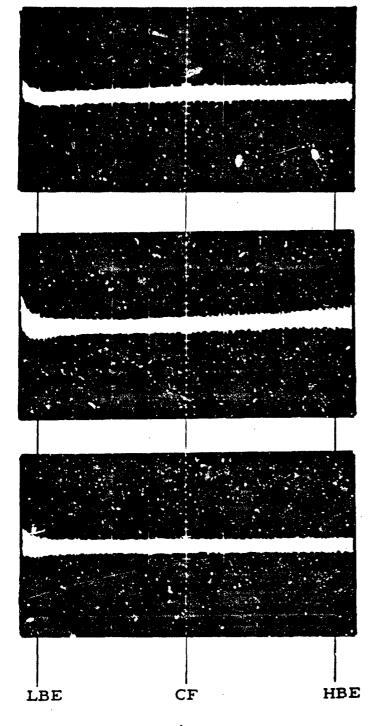
Channel 6, 1.70 kc  $\pm$ 7.5% RMS Level = 11 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3. 3-63
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 5; PBW CHANNELS 4, 5, and 6



Channel 7, 2.30 kc  $\pm$ 7.5% RMS Level = 6.5 mv max.

Channel 8, 3.00 kc  $\pm$ 7.5% RMS Level = 9 mv max.

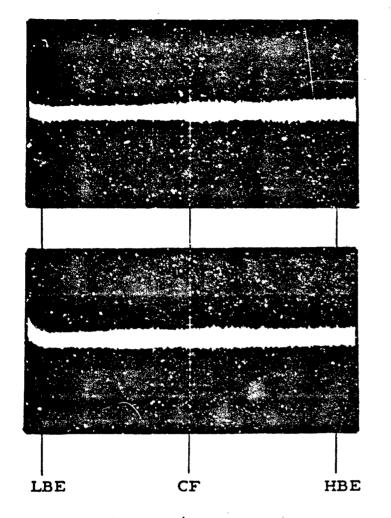
Channel 9, 3. 90 kc  $\pm$ 7. 5% RMS Level = 8 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3. 3-64
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 5; PBW CHANNELS 7, 8, and 9



Channel 10, 5.40 kc  $\pm$ 7.5% RMS Level = 10 mv max.

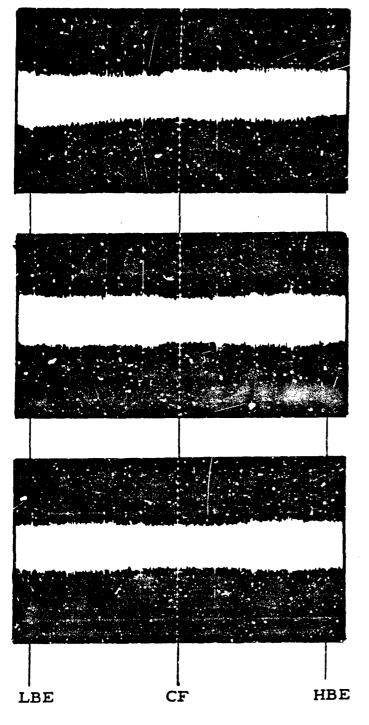
Channel 11, 7.35 kc ±7.5% RMS Level = 8.5 mv max.

Horizontal: 5 sec/cm

Vertical: 0.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3. 3-65
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 5; PBW CHANNELS 10 and 11



Channel 1, 16.0 kc ±2 kc RMS Level = 125 mv max.

Channel 2, 24.0 kc ±2 kc RMS Level = 130 mv max.

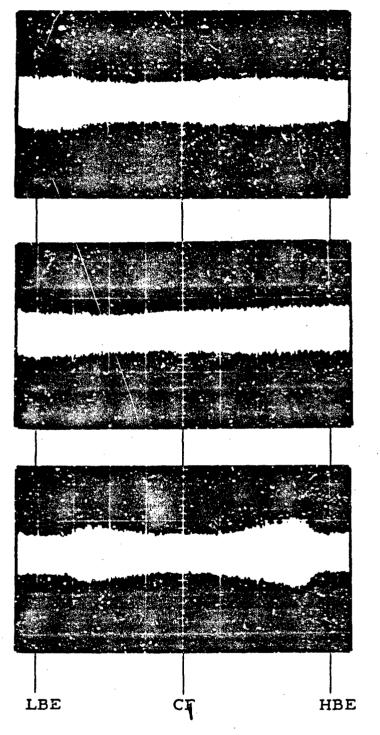
Channel 3, 32.0 kc ±2 kc RMS Level = 132 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

Channels deviated at one tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3.3-66
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 2; CBW CHANNELS 1, 2, and 3



Channel 4, 40.0 kc ±2 kc RMS Level = 130 mv max.

Channel 5, 48.0 kc ±2 kc RMS Level = 114 mv max.

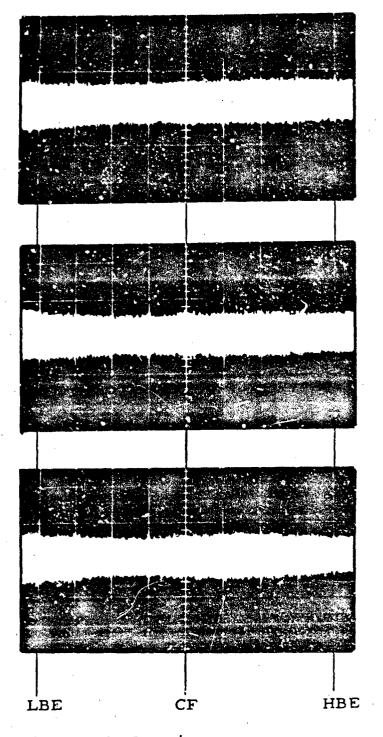
Channel 6, 56.0 kc ±2 kc RMS Level = 175 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

# FIGURE II-3. 3-67 INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX; SEARCH CHANNEL DR = 2; CBW CHANNELS 4, 5, and 6



Channel 7, 64.0 kc ±2 kc RMS Level = 97 mv max.

Channel 8, 72.0 kc ±2 kc RMS Level = 94 mv max.

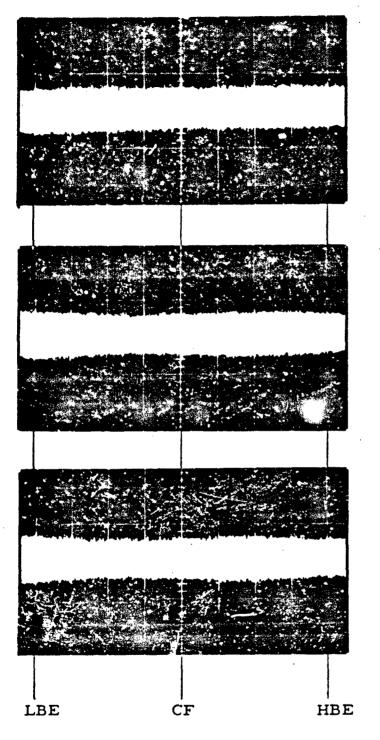
Channel 9, 80, 0 kc ±2 kc RMS Level = 100 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3. 3-68
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 2; CBW CHANNELS 7, 8, and 9



Channel 10, 88.0 kc ±2 kc RMS Level = 100 mv max.

Channel 11, 96.0 kc ±2 kc RMS Level = 102 mv max.

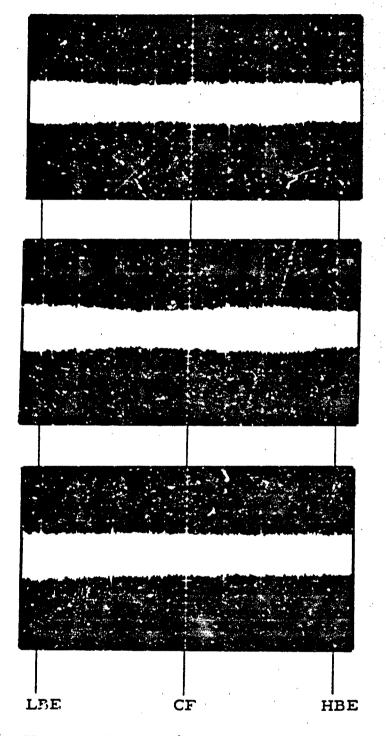
Channel 12, 104.0 kc ±2 kc RMS Level = 102 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3. 3-69
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 2; CBW CHANNELS 10, 11, and 12



Channel 13, 112.0 kc ±2 kc RMS Level = 92 mv max.

Channel 14, 120.0 kc ±2 kc RMS Level = 102 mv max.

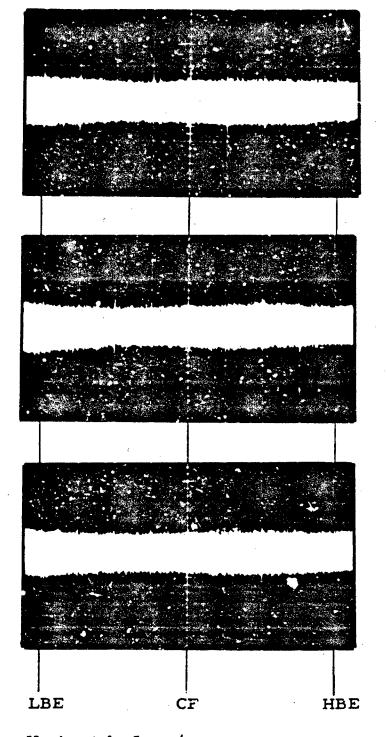
Channel 15, 128.0 kc ±2 kc RMS Level = 95 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps. whichever is larger.

FIGURE II-3. 3-70
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX;
SEARCH CHANNEL DR = 2; CBW CHANNELS 13, 14 and 15



Channel 16, 136.0 kc ±2 kc RMS Level = 102 mv max.

Channel 17, 144.0 kc ±2 kc RMS Level = 104 mv max.

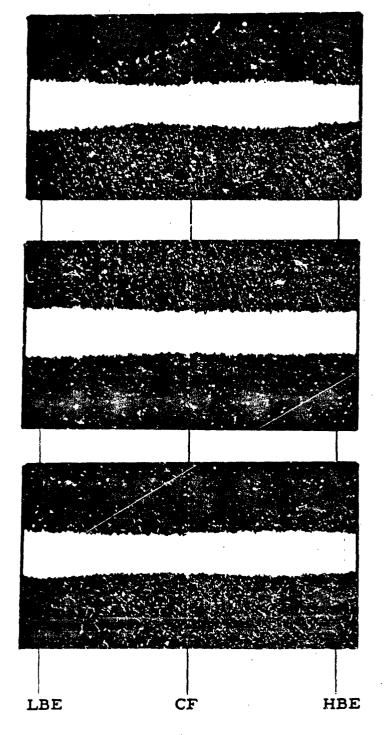
Channel 18, 152. 0 kc ±2 kc RMS Level = 100 mv max.

Horisontal: 5 sec/cm

Vertical: 2.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

# FIGURE II-3.3-71 INTLRMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX; SEARCH CHANNEL DR = 2; CBW CHANNELS 16, 17, and 18



Channel 19, 160. 0 kc ±2 kc RMS Level = 115 mv max.

Channel 20, 168. 0 kc ±2 kc

RMS Level = 109 mv max.

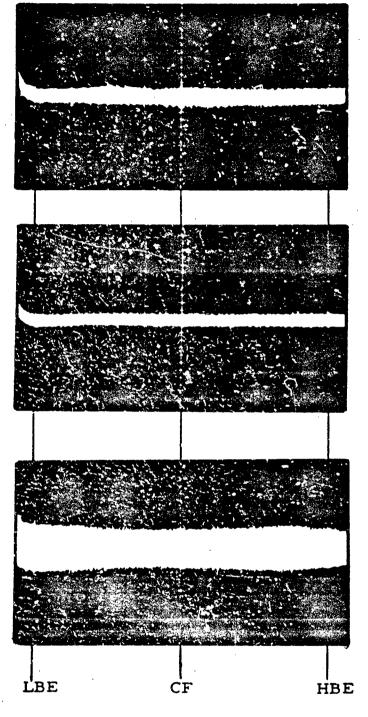
Channel 21, 176.0 kc ±2 kc RMS Level = 110 mv max.

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

Channels deviated at one-tenth nominal cutoff frequency or 5 cps, whichever is larger.

FIGURE II-3. 3-72
INTERMODULATION TEST: COMBINATIONAL BANDWIDTH MULTIPLEX
SEARCH CHANNEL DR = 2; CBW CHANNELS 19, 20, and 21



Channel 11, 7.35 kc  $\pm$ 7.5% DR = 5 RMS Level = 9.4 nsv max. Vertical = 0.5% FBW/cm

Channel 12, 10.5 kc ±7.5% DR = 5 RMS Level = 7.0 mv max. Vertical = 0.5% FBW/cm

Channel 1, 16.0 kc ±2 kc DR = 2 PMS Level = 155 mv max. Vertical = 2.5% FBW/cm

Horizontal: 5 sec/cm

Vertical: as specified

FIGURE II-3. 3-73
INTERMODULATION TEST: INSERTION OF 10.5 KC ±7.5%,
PBW CHANNEL 12, INTO COMBINATIONAL BANDWIDTH MULTIPLEX;
PBW CHANNELS 11 and 12 and CBW CHANNEL 1

#### 3.4 SYSTEM SIGNAL-TO-NOISE TEST

#### 3.4.1 General

The system signal-to-noise test consists of selecting particular receiver IF carrier-to-noise ratios and determining the subcarrier discriminator output signal-to-noise ratio. The test is accomplished with the pre-emphasis and transmitter deviation selected in the respective system test. The IF signal-to-noise level is determined by monitoring the IF at the predetection recording output. With an unmodulated of carrier input and the AGC externally held constant, the IF signal level is measured and then the noise is measured with the input carrier signal turned off.

During the initial system test, it was found that the IF output noise was a function of input signal level with the AGC voltage externally held at a constant value. Through the experiment it was determined that the IF amplifiers tended to saturate on large input signals thus suppressing the noise. The level that significant saturation took place was found to depend on the AGC voltage. With an AGC level of -4 volts, saturation was found to occur with IF output signal levels in excess of -17 dbm into 600 ohms or 110 mv rms. The manufacturer's specification on the predetection output level is 1.0v p-p or 350 mv rms. Thus, some saturation occurs at the specified level. In any event the maximum IF output signal should not exceed -17 dbm.

To obtain the desired IF signal-to-noise ratio, the noise is held constant and the input signal level adjusted. The test is made at IF signal-to-noise ratios of 4, 9, and 14 db. For the low signal-to-noise cases, the measurement of signal is difficult with an rms meter since both signal and noise are measured, i.e., the noise cannot be turned off. To provide accurate signal measurements, a frequency selective voltmeter is used to measure the signal level. Since the bandwidth of the frequency selective voltmeter is very narrow compared to the IF bandwidth, the signal level can be measured without the attendent noise background. For reference and to determine if saturation is occuring in the IF, the frequency selective voltmeter is tuned to 4.9 mc and the noise level noted with and without the rf carrier on. The block diagram for the test is shown in Figure II-3.4-1.

#### 3.4.2 Detailed Procedure

- a. Calibrate all VCOs.
- b. Deviate all VCOs to FBW at  $f_m$ , where  $f_m$  is the maximum modulating frequency for the particular deviation ratio.
  - c. Set receiver AGC voltage to -4 volts dc.

- d. Set IF signal-to-noise ratio to 4, 9, and 14 db. Check S/N with both Sierra frequency selective voltmeter and Fluke rms meter.
- e. Determine discriminator input signal-to-noise ratio by measuring the S/N ratio at the BPIF output. Measure signal with the search channel unmodulated. Measure the noise with all VCOs except the search channel operating in the multiplex and deviating FBW.
- f. Measure discriminator output noise with the search channel at center frequency and low bandedge.
- g. Modulate the search channel FBW at f<sub>m</sub> and null output with comparison signal. Measure rms level of null voltage. Also measure full scale modulating signal at nulling point.
  - h. With only the search channel in the multiplex, repeat f. and g., above.

#### 3.4.3 Results

Detailed conditions and actual measured data are contained in this volume in tables beginning with II. Summarizations of the data are contained in Volume I and have table or figure numbers beginning with I.

#### 3.4.3. i IRIG Baseband

The IRIG baseband, channels I through 18, was evaluated for signal-to-noise performance under the following conditions:

Test channels: 70 kc  $\pm$ 7.5%; 3 kc  $\pm$ 7.5%

Multiplex level: 1.0 volt rms

AGC voltage: -4 volts dc

Deviation ratio: 5

LPOF: Constant amplitude, 18 db/octave, nominal cutoff frequency for DR = 5

The results of the signal-to-noise test are shown in Table II-3.4-2 and summarized in Table I-3.5-2, Volume I. For each IF signal-to-noise ratio, the search-channel output noise is measured for two multiplex conditions and three deviation conditions. The two multiplex conditions are full multiplex and search channels only. The latter condition eliminates intermodulation noise. The three cases of search channel deviation include: center frequency, low bandedge, and FBW modulation at the maximum channel rate for the particular deviation ratio.

#### 3.4.3.2 IRIG Baseband--Wideband Channel

The IRIG baseband with a wideband (±15%) channel in the highest frequency position was evaluated under the following conditions:

Test channels: 70 kc ±15%; 3 kc ±7.5%

Multiplex level: 1.0 volt rms

AGC voltage: -4 volts dc

Deviation ratio: 5

LPOF: Constant amplitude, 18 db/octave, nominal  $f_c$  for DR = 5

The results are shown in Table II-3. 4-3 and summarized in Volume I, Table II-3. 5-3. Pages 4 and 5 of Table II-3. 4-3 are data that was taken at a later date for recheck and additional data.

#### 3.4.3.3 IRIG Baseband--Deviation Ratio of 1 and 2

The IRIG baseband, channels 1 through 18, were operated at deviation ratios of 1 and 2 and the signal-to-noise performance desermined under the following conditions:

Test channels: 70.0 kc  $\pm$ 7.5%; 22.0 kc  $\pm$ 7.5%; 7.35 kc  $\pm$ 7.5%; 3.0 kc  $\pm$ 7.5%; 960 cps  $\pm$ 7.5%

Multiplex level: 1.0 volt rms

Deviation ratio: 1 or 2

AGC: -4 volts dc

LPOF: Constant amplitude, nominal cutoff frequency for the particular deviation ratio for DR = 1, 18 db/octave.

The results for DR = 1 are shown in Table II-3.4-4 and the results for DR = 2 are shown in Table II-3.4-5. The results for both deviation ratios are summarized in Table I-3.5-4 of Volume I.

#### 3.4.3.4 Expanded Proportional-Bandwidth Baseband

The expanded baseband, channels I through 21, was evaluated for signal-to-noise performance under the following conditions:

Test channels:  $165 \text{ kc} \pm 7.5\%$ ;  $124 \text{ kc} \pm 7.5\%$ ;  $93 \text{ kc} \pm 7.5\%$ ;

70 kc  $\pm$ 7.5%; 3 kc  $\pm$ 7.5%

Multiplex level: 750 mv rms

Deviation ratio: 5

AGC voltage: -4 volts dc

LPOF: Constant amplitude 18 db/octave, nominal cutoff frequency for DR  $\approx 5$ 

The results of the signal-to-noise test are shown in Table II-3.4-6. The results are summarized in Table I-3.5-5. Page 5 of Table II-3.4-6 was additional data taken for recheck and verification at a later date than the original data.

#### 3.4.3.5 Expanded Proportional-Bandwidth Baseband--Wideband Channel

The expanded baseband, channels 1 through 19 and wideband channel H, was evaluated for signal-to-noise performance under the following conditions:

Test channels:  $165 \text{ kc} \pm 15\%$ ;  $93 \text{ kc} \pm 7.5\%$ ;  $70 \text{ kc} \pm 7.5\%$ ;  $3 \text{ kc} \pm 7.5\%$ 

Multiplex level: 630 my rms

Deviation ratio: 5

AGC voltage: -4 volts dc

LPOF: Constant amplitude, 18 db/octave, nominal cutoff frequency for DR = 5

The results are shown in Table II-3. 4-7 and summarized in Table I-3. 5-6. The data shown on page 5 of Table II-3. 4-7 was taken at a later date for recheck and for additional data.

#### 3.4.3.6 Constant-Bandwidth Baseband

The constant-bandwidth baseband, channels 1 through 21, was evaluated under the following conditions:

Test channels:  $56 \text{ kc} \pm 2 \text{ kc}$ ;  $88 \text{ kc} \pm 2 \text{ kc}$ ;  $120 \text{ kc} \pm 2 \text{ kc}$ ;  $160 \text{ kc} \pm 2 \text{ kc}$ 

Multiplex level: 360 mv rms

Deviation ratio: 2, also 4 and 1 on the 120 kc ±2 kc channel only

AGC voltage: -4 volts dc

LPOF: Constant amplitude, 42 db/octave, nominal cutoff frequency for specified deviation ratio.

The results are shown in Table II-3, 4-8 and summarized in Tables I-3, 5-8 and I-3, 5-9.

#### 3. 4. 3. 7 Combinational-Bandwidth Baseband

The combinational-bandwidth baseband, IRIG channels I through 11 and constant-bandwidth channels I through 21, was evaluated under the following conditions:

Test channels:  $3 \text{ kc} \pm 7.5\%$ ;  $56 \text{ kc} \pm 2 \text{ kc}$ ;  $88 \text{ kc} \pm 2 \text{ kc}$ ;  $120 \text{ kc} \pm 2 \text{ kc}$ ;  $160 \text{ kc} \pm 2 \text{ kc}$ 

Multiplex level: Total; 635 mv rms; IRIG channels; 210 mv rms, and CBW channels; 600 mv rms.

Deviation ratio: 2 on the constant-bandwidth channels and 5 on the IRIG channels

AGC voltage: -4 volts dc

LPOF: Constant amplitude, 42 db/octave for CBW channels and 18 db/octave for IRIG channels, nominal cutoff frequency for specified deviation ratio.

The results are shown in Table II-3.5-10 and summarized in Table I-3.5-11.

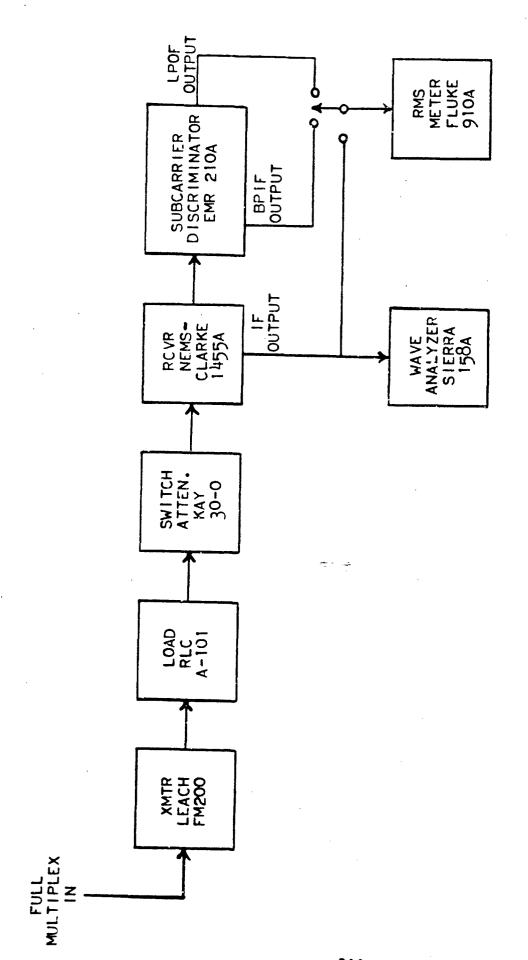


FIGURE 11-3, 4-1 SIGNAL-TO-NOISE TEST BLOCK DIAGRAM

### TABLE II-3.4-2 SIGNAL-TO-NOISE TEST DATA

System	Description: Stand	ard	18	RIG	Chan	ne/s.	DR-5
	1-To-Noise Ratio: 2	_					
Discrim	inator Full Scale Output:	5.0u	cms /4	14 UPF	0019	mar	2000
	Signal: -28.5db		Fluke:		Noise:		
	Noise: -53.5 db			Noise:	-30.	5 db	
Discrim	inator Channel: 18. 7	OKC		المال المراجعة			
	BPIF: Signal: -5.	db	Noise:_	-13.	6 db		4.516
	Full Scale Modulation A	t Summi	ing Point	: <u>2.4</u>	<u> </u>		
·	Output Noise:						
	Full Multiplex	CF:	650	mr			
		LBE:_	1.7				
	•	Modula	ated:	650 m	<u>,                                     </u>		
	Search Channel	Only:			•		
		CF:	650	my			
	•	LBE	475	Y			
	, <b></b>	Modula	ited:	450mv	<i>,</i>		
Discrim	inator Channel: 8 3	OKC					New Annual Control
	BPIF: Signal: -23	<u> </u>	Noise:_	- 26	16		28.026
	Full Scale Mcdulation A	Summi	ng Point:	3.4	14		
•	Output Noise:					-	
	Full Multiplex:	CF:	1.94		الكاملة الأدريج المستدرة الرسوية المحادية		
	•	LBE:_	3.6V				
,		Modula	ited: /	6 ×			· .
	Search Channel C	Only:					
		CF:	1.2	<u> </u>			-
		LBE:	3.0	/			
		Modula	tedi	1.44			

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# TABLE II-3, 4-2 (CONTID.) . SIGNAL-TO-NOISE TEST DATA

System	Description: Standa	rd 18 1RIG Channels, DR=5
IF Signa	1-To-Noise Ratio: 4d	Receiver AGC Voltage: -4,0 vdc
Discrim	inator Full Scale Output:	14.14UPP / 5.0 Urms (30,1 fm at 20)
	Signal: -26.5db	Fluke: Signal + Noise: -25.0db
•	Noise: - 53.5db	Noise: -30,6db
Discrim	inatur Channel: #18.7	OKC
	BPIF: Signal: -4.6	16 Noise: -17.0db -17.5db
	Full Scale Modulation A	t Summing Point: 2.5 urms
	Output Noise:	
	Full Multiplex:	CF: 144 Mugas
		LBE: 360 Murme
	·	Modulated: 2 65 murms (with 6 upp Soit
	Search Channel C	Only: Mull Point)
		CF: 130 muras
		LRE: 250 mu-
		M. Iulated: 65 muxme with Gupp Soit
Discrim	inator Channel: 18 3.1	OKC MUIT POINT)
•	BPIF: Signal: - 22.5	16 Noise: -30.5 db -32.0
	Full Scale Modulation A	t Summing Point: 2,4Vyms
	Output Noise:	
	Full Multiplex:	CF: 250 Muyns
		LBE: 1.35 urms
		Modulated: 3 90 mores (wich 6499 Sp.
	Search Channel (	Only: mull Point)
		CF: 160 muyms
	•	LBE: \$400 myyms
		Modulated: 85 murms
	•	1
	•	

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## TABLE II-3. 4-2 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Standard 18 1RIG Channels, DR=5	
IF Signal-To-Noise Ratio: lodb Receiver AGC Voltage: 40 ude	
Discriminator Full Scale Output: 5,00rms Hy.14uer @ O.1 Cm or 20e	الما
Sierra: Signal: -25.0db Fluke: Signal + Noise: -23.3dk	•
Noise: -53 db Noise: -310 db	
Discriminator Channel: 18.70 KC	كبيسم
BPIF: Signal: -4,4db Noise: -21,0db -21.	<u>3db</u>
Full Scale Modulation At Summing Point: 2,40 rms	
Output Noise:	
Full Multiplex: CF: //Omires	
LBE: 140 myms	
Modulated: 58 murms	
Search Channel Only:	
CF: 85 mirms	
LBE: 85 murms	خبينسه
Modulated: 45 mu ems	
Discriminator Channel: 8.3.0KC	
BPIF: Signal: -22,2db Noise: -34,0db -39.6	db
Full Scale Modulation At Summing Point: 2, 40 yms	منيس
Output Noise:	
Full Multiplex: CF: 170 moves	
LBE: /80my rms	
Modulated: 75 myras	
Search Channel Only:	
CF: 95 muyms	
LBE: //Q.muyms	
Modulateds 50 milyms	

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Date 1-4-65 Name W. Bishop

# TABLE II-3. 4-2 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System I	Description: Standa	-1 18 1RIG	Channels	DR=5
IF Signa	1-To-Noise Ratio: 9 d	Receiver AGC	Voltage:	Dude
	inator Full Scale Output:		P @ alfm	or 20cg
	Signal: -21.5 db	Fluke: Signa		
	Noise: -54006	Noise	e: -30,5°d	<u> </u>
Discrim	inator Channel: 1/8.70	KC		
	BPIF: Signal: -3.1d	*	1.216	-24.816
	Full Scale Modulation A	Summing Point: 2.	4Vrme	
•	Output Noise:		* *	
	Full Multiplex:	CF: 47 murme		
		LBE: 45 muyns		
		Modulated: 25mu	(ms	·
·	Search Channel C	nly:		· ·
		CF: 42 muyms	الواند الأدار المساور والمساور	
		LRE: 39muyms		
		Modulated: 23 mu	YMS	
Discrim	inator Channel: 83.	OKC		
	BPIF: Signal: -2/15	16.215 Noise: -4/,	506	-51.01b
	Fuli Scale Modulation A	Summing Point: 2.	4 Urms	
	Output Noise:		•	
	Full Multiplex:	CF: 4/myrms		
		LBE: 44muym		
		Modulated: 2/mu	rms	
	Search Channel	only:		
		CF: 1/ muyms		·
		LBE: 12.5 muy		
		Modulatedi 8.5 m	1U Y M S	

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Nama W. Bishop Date 1-4-65

### TABLE II-3. 4-2 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

rstem	Description: Standa	ird	18 1K	16 CH	annels	DR=5
Signa	il-To-Noise Ratio: 14	1 06	Receive	r AGC Vo	ltage: - 4	Dude
iscrim	inator Full Scale Output	: 3.0u	Rm2/19	HUPP	Q O.I fm	or 20es
	Signal: -16.576		Fluke:		Noise: -/	
	Noise: -54.0db		<b>-</b>	Noise:	30.5	
iscrim	inator Channel: #/8	704	~			
	BPIF: Signal: -2.8d	b	Noise:_	- 28.12	4	-30.0
	Full Scale Modulation A	t Summ	ing Point:	2,41	YMS	
	Output Noise:			•		
	Full Multiplex:	CF:	26 mu	Y M S	•	
		LBE:	25ml	<u> </u>		
				muem		
	Search Channel			······································		
		CF:_	22 MUY	<b>M</b> 3		
			21 mux			
		Modul	ated: /3	. 8 myr	m.t.	
scrim	instor Channel: #8 3.	OKC		_		
	BPIF: Signal: -2/.3	db	Noise:	-42.0	dh	-56.01b
	Fuli Scale Modulation A	t Summ	ing Point:	2.44	275	
•	Output Noise:			•		
,	Full Multiplex:	CF:	9,5 mus	ms		
		LBE:_	11.5 mus	ms .		
	,			Murm	<u> </u>	
	Search Channel C					
	•	CF:_3	.Ome	m.1		
			32 mux			
		Modula	ted: 6.0	myrms		
				•		

Date 1-4-65 Name W. Rishop -216-

# TABLE II-3. 4-3 SIGNAL-TO-NOISE TEST DATA

System Description: Chann	els 1-16 Narrow + E. DR=5
IF Signal-To-Noise Ratio: 4	db Receiver AGC Voltage: - 4.0 ydc
Discriminator Full Scale Output	10 UPP
Sierra: Signal: -28,2db	Fluke: Signal + Noise: -26.2db
No.se: -54 db	Noise: - 32.0 dh
Discriminator Channel: E. 7	
PPIF: Signal: -1.8d	b Noise: MM - 13.7db umm - 13.7dl
	t Summing Point: 3.6 Vrns
Output Noise:	
Full Multiplex:	C1: 270mvrms
•	LRE: 600 Murms
	Modulated: 700 muyms
Search Channel	Onl.:
	CF: 270myrms
	IBE: LOUDMUYMS
	Modulated: 700 myrms
Discriminator Channel: 3.0 /	sc ± 7.5%
BPIF: Signal: -24.1	adb Noise: MM -29.0db umm-29.5db
Full Scale Modulation A	t Summing Point: 3.6 Jyms
Output Noise:	
Full Multiplex:	CF: 900 mur-s
	LBE: 2.0 Urms
	Modulated: 2. 4 yrms
Search Channel	Only:
Tex =132 Set for gain	CF: 250 murms.
of 10 therefore recorded	LBE: /, S Vrms
xlues are 10 of	Modulated: 1.7 Vyms
ictual value read	
in meter.	
. /	Date 1-13-65 Name W. Bishop
1cf 5	-217-

# TABLE II-3. 4-3 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

item Description: Channe	15 1-16 Ylarrow + E. DR=5
Signal-To-Noise Ratio: 7 d	
scriminator Full Scale Output:	100PP
rra: Signal: -23,5db	Fluke: Signal + Noise: -23.0db
Noise: -55.5db	Noise: -32,5-66
criminator Channel:	70HC = 15%
•	16 Noise: MM -21.1db umm -21.1db
Full Scale Modulation At	Summing Point: 3.6 Uyms
Output Noise:	
Full Multiplex:	CF: 48 Muxme
	LBE: 37 Myzns
÷ v≥ T	Modulated: 58 Muyuni
Search Channel C	
	CF: 40 Muams
	LBE: 35 myyms
	Modulated: 55 myrms
criminator Channel: 3.0 Kg	
	Noise: MM - 41 db umm - 42.5-db
Full Scale Modulation At	Summing Point: 3, 6 y - 15
Output Noise:	
Full Multiplex:	CF: 49 murms
	LBE: 45-Myrms
	Modulated: 65myyms *
Search Channel O	
-6 =122 = 1 0	CF: 18 myrms
ek. =/32 Set for in of 10 Therefore	LRE: 16 myrms
corded values are	Modulated: 27 Myrms *
s of actual value	
ad on meter.	·
2 of 5	Date 1-13-105 Name W. Bishop

# TABLE II-3, 4-3 (CONT'D.) SIGNAL-10-NOISE TEST DATA

System Description: Channels 1-16 Narrow + E. DR=5
IF Signal- In-Norse Ration 14db Receiver AGC Voltage: - 4. Oude
Discriminator Full Scale Output: 100PP
Sierra: Signal -18.5 db Fluke: Signal + Noise: -18.5 db
Noise: -56.0 db Noise: -32.5 db
Discriminator Channel E. 70KC ± 150%
BPIF: Signal: +0.5db Noise: MM -26.3db umm -26.5
Full Scale Modulation At Summing Point: 3.6 Urms
Output Noise:
Full Multiplex: CF: 18 myrms
LBE: 18 murme
Modulated: 39 murms
Search Channel Only:
CF: 17.0 murms
LBE: 16.9 mysme
Modulated: 38 murns
Discriminator Channel: 3,0 kc +7.5%
BPIF. Signal: -23.0db Noise: MM -42.5db umm-49.5
Full Scale Modulation At Summing Point: 3,6 Urms
Output Noise:
Full Multiplex: CF: 7.5 murms
LBE: 8,5 myrms
Modulated: 20 myrms
Search Channel Only:
Type 132 (Tex) Set IRF: 5- Own
Con using al 10 There
fore recorded values Modulated: 11 milyms
are to of actual
value read on meter
Date /-/3-65 Name W. Bishai
3, 4.5

## TABLE II-3. 4-3 (CONT'D.) SIGNAL-FO-NOISE TEST DATA

Sustain December 01	1 Nomes 4 F
System Description: Chame 15 1-1  IF Signal-to-Noise Ratio As Liced	AGC Voltage - 4/0 udc
	70 KC = 15.96 (=/N)c=14db
BPIF: Signal +0.3 / Noise: Full Mult.	-26.6d Search Ch. Only -27.0d)
Deviation Ratio	db:
LPOF Cutoff Frequency	7/00 634
Full Bandwidth Voltage	· 100 20 +13.4db
Output Noise: Full Multiplex	
Search Channel Only	. 16.5 mym1 -33.5db
Channel No Channel Frequency_	10 Kc = 15.0/a (5/N)c = 1/db
BPIF: Signal 10.1 de Noise: Full Mult.	
Deviation Ratio	
LPOF Cutoff Frequency	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	
	(41)
Channel No. F Channel Frequency	7 12xc2 150% (5/N) c= 7 db
BPIF: Signal -0.3 d Noise: Full Mult.	
Deviation Ratio	
LPOF Cutoff Frequency	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	. 33mu27,4db
Channel No Channel Frequency_	7 ONC2150/4 (5/N)c = 6db
	-18.5 db Search Ch. Only-19.1 db
Deviation Ratio	. 2100 eps dbi
LPOF Cutoff Frequency	
	. 10 UPD +13.4 db
	. 5-4 myrms -23,2db
Scarcia Chamier Chity	27,000
Channel No. E Channel Frequency	70KC =15% (5/N/k = 4db
BPIF: Signal - 2.1 dh Noise: Full Mult.	-14.9 db Search Ch. Only-15, 6 db
	5
LPOF Cutoff Frequency	2/00 aps db;
·	· 10 UPP +13.4db
	115 muras -16.7 ds
Search Channel Only	100 muns -17.6ds

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Name W. Bishop Date 2-9-65

### TABLE II-3. 4-3 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channels 1-16 / IF Signal-to-Noise Ratio 2 db	Varrow + E
IF Signal-to-Noise Ratio 2 db.	AGC Voltage -4.0 Ude
Channel No. E Channel Frequency	70 tc ±1590
BPIF: Signal - 3.4 dh Noise: Full Mult.	-12.2 dh Search Ch. Only -12.8 dh
Deviation Ratio	
LPOF Cutoff Frequency	2100cos db:3
Full Bandwidth Voltage	
Output Noise: Full Multiplex	420 murms -5.4dh
Search Channel Only	400musm: -6.0 db
,	
Channel No. Channel Frequency	
BPIF: Signal Noise: Full Mult.	Search Ch. Only
Deviation Ratio	
LPOF Cutoff Frequency.	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	•
Search Channel Only	
Channel No. Channel Frequency  BPIF: Signal Noise: Full Mult.	
BPIF: Signal Noise: Full Mult.	Search Ch. Only
Deviation Ratio	
LPOF Cutoff Frequency	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Output Noise: Full Multiplex	
Channel No Channel Frequency	
. BPIF: Signal Noise: Full Mult.	Search Ch. Only
Deviation Ratio	
LPOF Cutoff Frequency	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	
Channel No. Channel Frequency	
Channel No. Channel Frequency  BPIF: Signal Noise: Full Mult.	Search Ch. Only
Deviation Ratio	Search Ch. Only
LPOF Cutoff Fraquency	
Full Bandwidth Voltage	
Full Bandwidth Voltage Output Noise: Full Multiplex.	
Search Channel Only	
observation only	
•	

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Name (1). Bishop Date 2-9-65

# TABLE 3.4-4 SIGNAL-TO-NOISE TEST DATA

System Description: Channe   1-1:	7 PBW
IF Complete Noise Patie 2 10	AGC Voltage - 4/1/1
IF Signal-to-Noise Ratio 206	7,000
Channel No. 18 Channel Frequency_	70kc + 7.5%
BPIF: Signal -6.3db Noise: Full Mult.	-12.746 Search Ch. Only -14.746
Deviation Ratio	. /
LPOF Cutoff Frequency	
Full Bandwidth Voltage	Davison
Output Noise: Full Multiplex	3/00
Output Note: Full Multiplex	214.3
Search Channel Only	· \$100 W.7
Channel No. /4 Channel Frequency_	22kc 17.5%
BPIF: Signal -/3.5kc Noise: Full Mult.	-17 Coli Search Ch. Only-19 1-16
Deviation Ratio	17,080 solven em em <u>17,3917</u>
LPOF Cutoff Frequency	165000
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	. 4200 mV
<i>1</i> 1	- 2/-/: 47/-
Channel No. // Channel Frequency_	1.35 Ke = 1.5%
BPIF: Signal -19.566 Noise: Full Mult.	-21,5db Search Ch. Only -23.0d6
Deviation Ratio	·
LPOF Cutoff Frequency	
Full Bandwidth Voltage	. 20V B-10
Output Noise: Full Multiplex	. 6500 mV
Search Channel Only	
Thannel No. 8 Channel Frequency_	3kc ± 7.5%
BPIF: Signal - 23.5 do Noise: Full Mult.	-26.5 db Search Ch. Only-28.5 db
Deviation Ratio	. /
LPOF Cutoff Frequency	
	. 20V p-p
•	- and the
Search Channel Only	
Jenich Ghallach Ghay	
Channel No. 4 Channel Frequency	9/1000 +752
BPIF: Signal -28.0db Noise: Full Mult.	-715 Jh Search Ch Only-775 //
	-37.5 go out en om om 55,500
Deviation Ratio	·
Full Bandwidth Voltage	2016-10
Output Noise: Full Multiplex	4500 mV
Search Channel Only	3000 MV
	· ···
· .	1
10f4 -222	_
1057	<b>~</b> • • · · · · · · · · · · · · · · · · ·
	pulan
///	7.7.1.1.7.8.4.201 Date - 1-1.5

### FIGURE II-3. 4-4 CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channel 1-18 PBW
IF Signal-to-Noise Ratio 4db AGC Voltage -4.0Vdc
Channel No. 18 Channel Frequency 70 kc 1.5%  BPIF: Signal -4.316 Noise: Full Mult17.216 Search Ch. Only -19.36  Deviation Ratio
Channel No. 14 Channel Frequency 22 ke + 7.5%  BPIF: Signal - 14.3db Noise: Full Mult 20.5db Search Ch. Only - 24.0a  Deviation Ratio
Channel No.   Channel Frequency 7.35 kc 1.25%  BPIF: Signal -18.5db Noise: Full Mult25.5db Search Ch. Only -28.5d  Deviation Ratio
Channel No. 8 Channel Frequency 3kc ±7.5%  BPIF: Signal -22 5.16 Noise: Full Mult30.046 Search Ch. Only -34.04  Deviation Ratio
Channel No. 4 Channel Frequency 960 cps ± 7.5%  BPIF: Signal - 27.0 db Noise: Full Mult 36. 36 Search Ch. Only - 39.0 db  Deviation Ratio

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Name WR4/1901 Date 1-6-65

### FIGURE II-3. 4-4 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channel 1-18	PBW
IF Signal-to-Noise Ratio 9 db	AGC Voltage -4.0Vdc
Channel No. 18 Channel Frequency	70 Kc = 7.5%
BPIF: Signal -2,7db Noise: Full Mult.  Deviation Ratio	-24.0db Search Ch. Only -25.4db
LPOF Cutoff Frequency	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	. 450mV
Channel No. 14 Channel Frequency	22kc ± 7.5%
BPIF: Signal -9.866 Noise: Full Mult.	
Deviation Ratio	
LPOF Cutoff Frequency	. 1650cps
Full Bandwidth Voltage	.201 u-u
Output Noise: Full Multiplex	
Search Channel Only	
·	
Channel No. // Channel Frequency BPIF: Signal - 16.5db Noise: Full Mult.	7.35 Kc 17.5%
BPIF: Signal -16.56b Noise: Full Mult.	-39.0 db Search Ch. Only - 49.0 db
Deviation Ratio	, /
LPOF Cutoff Frequency	551 cps
Full Bandwidth Voltage	261p-p
Output Noise: Full Multiplex	500 mg
Search Channel Only	
Channel No. Channel Frequency  BPIF: Signal -21.0db Noise: Full Mult.	3 KC I 7.5 %
	- ya,uah staren en. omy-sa.uah
LPOF Cutoff Frequency	
	20Vp-p
	450 mr
Search Channel Only	. KO mv
Channel No. 4 Channel Frequency_	960 cps = 7.5%
BPIF: Signal -25.0dh Noise: Full Mult.	-47.006 Search Ch. Ouly 60.006
Deviation Ratio	- /
LPOF Cutoff Frequency	72 6 105
Full Bandwidth Voltage	
	350ml
•	822 mV
Continue Charmer Chary	
<b>7</b> C	
3 of 4 -224-	
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Name WRH/MDL Date 1-6-65

#### FIGURE II-3. 4-4 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channel 1-18  IF Signal-to-Noise Ratio 14 db	PBW AGC Voltage - 4.0Vdc
7788	ACIC Voltage 4.0Vac
Channel No. 18 Channel Frequency BPIF: Signal - 2,5 db Noise: Full Mult Deviation Ratio	27.8 db Search Ch. Only -30.60
LPOF Cutoff Frequency	. 20V
Output Noise: Full Multiplex Search Channel Only	· 300 mv
Channel No. 14 Channel Frequency BPIF: Signal -9.5db Noise: Full Mult	22 Kc ± 7,57%
LPOF Cutoff Frequency	1650 000
Output Noise: Full Multiplex.	.20 V p-p
Search Channel Only	.103 mr
Channel No. // Channel Frequency  BPIF: Signal -/6.3db Noise: Full Mult.  Deviation Ratio.  1 POF Cutoff Frequency  Full Bandwidth Voltage  Output Noise: Full Multiplex.	-46.866 Search Ch. Only -57.26 • 551 cps • 20 Y p-p • 130 my
Search Channel Only	
Deviation Ratio.  LPOF Cutoff Frequency  Full Bandwidth Value	-44.0db Search Ch. Only-62.0db . 1 . 225 cps
Output Nisicas Full Made at	. 20 V p-p . 170 mV . 22 mV
Deviation Ratio.  LPOF Cutoff Frequency Full Bandwidth Voltage	72cps 201 p-p

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Name WRH/MDL Date 1-6-65

### FIGURE II-3. 4-5 SIGNAL-TO-NOISE TEST DATA

System Description: Channel 1-18,	PBM
IF Signal-to-Noise Ratio 2db	AGC Voltage - 4.0 Vdc
Channel No. 18 Channel Frequency	
BPIF: Signal -6.3db Noise: Full Mult.	-13.7db Search Ch. Only -14.7db
Deviation Ratio	. 2
LPOF Cutoff Frequency	. 2625 cps
Full Bandwidth Voltage ,	· 20/w-0
Output Noise: Full Multiplex	· ROCKOMY
Search Channel Only	. 2210 mV
Channel No. 14 Channel Frequency_	つつひょうフリグ
BPIF: Signal -/3.5.16 Noise: Full Mult.	-176 1/ Search Ch. Only -190 1/
Deviation Ratio	
LPOF Cutoff Frequency	. 825 cps
Full Bandwidth Voltage	· 201p-p
Output Noise: Full Multiplex	· 3200 mv
Search Channel Only	. 2400 mv
Channel No. // Channel Frequency	7.35 Ke = 7.5%
BPIF: Signal -19.566 Noise: Full Mult.	-21,566 Search Ch. Only-23.0dh
Deviation Patie	
LPOF Cutoff Frequency	. 276005
Full Bandwidth Voltage	201n-n
Output Noise: Full Multiplex	4000
Search Channel Only	3510 411
Channel No. 8 Channel Frequency	76. ±759
BPIF: Signal -23.5d6 Noise: Fuli Mult.  Deviation Ratio	-20.306 Search Ch. Only 20.306
LPOF Cutoff Frequency	
	20V pp
Output Noise: Full Multiplex	space mr
Search Channel Only	3000 mx
	2/1 - +7 5 67
Channel No. 4 Channel Frequency	
BPIF: Signal -28.0db Noise: Full Mult.	-31.5db Search Ch. Only -33.5-16
Deviation Ratio	2
	36005
Full Bandwidth Voltage	2010-0
Output Noise: Full Multiplex	3000 mr
	2500 my
,	
10f4	
-226-	•

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### FIGURE II-3. 4-5 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channel 1-18 F	LJ LJ
IF Signal-to-Noise Ratio 4db	AGC Voltage - 4.0 Vdc
Channel No. // Channel Frequency_ BPIF: Signal -4346 Noise: Full Mult. Deviation Ratio	-17.266 Search Ch. Only -19.066 · 2 · 2625 · 20V p-p · 350m/
Channel No. 14 Channel Frequency BPIF: Signal -14.3db Noise: Full Mult. Deviation Ratio	-21.5db Search Ch. Only -24.1db · 2 · 825 · 115 · 2010 my · 1000 my
Channel No. // Channel Frequency BPIF: Signal -/1.5dh Noise: Full Mult. Deviation Ratio	-25.5 db Search Ch. Only -29.5 db -276 c.ps -2010 -19 -1600 my
Output Noise: Full Multiplex	-30.016 Search Ch. Only -34.016
Channel No. Channel Frequency  BPIF: Signal -27.0dc Noise: Full Mult.  Deviation Ratio	-36.0db Search Ch. Only-39.0db · 2 · 36 cps · 20Vpp · 1100 My

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### FIGURE II-3. 4-5 (CONT'D.) SE NAL-FO-NOISE LEST DATA

System Description:	Charnel 1-18	PEW
IF Signal-to-Noise Rat		AGC Voltage -4.01/2
Deviation Ratio LPOF Cutoff Freque Full Bardwidth Volt Output Noise: Full	Channel Frequency  b Noise: Full Mul-  nev	. 24.306 Search Ch. Only-25.466 . 2 . 2625 cps . 201 cp
Deviation Ratio LPOF Cutoff Freque Full Bandwidth Volta Output Noise: Full	db Noise: Full Mul	133.5de Scarch Ch. Onle-42.2de 2. 825 cps 20V p-p -192 mr
BPIF: Signal -16.5 Deviation Ratio LPOF Cutoff Freque Full Bandwidth Volta Output Noise: Full 1	do Noise: Full Mul	21/03 250mv
Deviation Ratio	oncy	142.0 db Search Ch. Only-56.0 db 2 1/3 spx 20/ spx 20/ spx
Deviation Ratio LPOF Cutoff Freque Full Bandwidth Volta Output Noise: Full N	ncy	960 cps ± 7.5%  -47.066 Search Ch. Only-60.066  2  -36cps  -182my  -50my

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Name WRH/MEL Date 1-6-65

# FIGURE II-3. 4-5 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channel 1-18 PBW  iF Signal-to-Noise Ratio 14 db AGC Voltage -4.01dc
if Signal-to-Noise Ratio 14 db AGC Voltage -4.0 Vdc
Channel Nc. 18 Channel Frequency 70 Ke \$\frac{1.575}{2.575}\$  BPIF: Signal - 2.5 db Noise: Full Mult27 8 db Search Ch. Only - 30.6 db  Deviation Ratio
Channel No. 14 Channel Frequency 22 kc ± 7.5 %  BPIF: Signal -9.5 db Noise: Full Mult38.4 db Search Ch. Cnly -45.2 db  Deviation Ratio
Channel No. // Channel Frequency 1.35 kc ± 7.5%  BPIF: Signal -16.345 Noise: Full Mult46.866 Search Ch. Only -57.266  Deviation Ratio
Channel No. 8 Channel Frequency Skc ± 7.5%  BPIF: Signal - 20.8 db Noise: Full Mult44.0 db Search Ch. Only -62.0 db  Deviation Ratio
Channel No. 4 Channel Frequency 960 - 275%  BPIF: Signal -24.8 db Noise: Full Mult49.0 db Search Ch. Only -63.0 db  Deviation Ratio

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Name WRH, MDL Date 1-6-65

### FIGURE II-3.4-6 SIGNAL-TO-NOISE TEST DATA

System Description: Standard IRIG + 93.124 \$ 165 KC 175% CA
System Description: Standard 1RIG + 93, 124 # 165 KC 175 % CA  IF Signal-to-Noise Ratio 4 db AGC Voltage - 4. Oude
Channel No. 2 Channel Frequency 3.0 KC : 7.5%  BPIF: Signal -25db Noise: Full Mult26.2 Search Ch. Only -27.8  Deviation Ratio
LPOF Cutoff Frequency
Full Bandwidth Voltage
Channel No. 18 Channel Frequency 70 KC 77.5%  BPIF: Signal -10.5 de Noise: Full Mult12.21 Search Ch. Only -13.5 de Deviation Ratio
LPOF Cutoff Frequency
Output Noise: Full Multiplex
Channel No. 19 Channel Frequency 93 KC 27.5%  BPIF: Signal-(9.84), Noise: Full Mult//. 7 Search Ch. Only -/2,54)  Deviation Ratio
1 POF Cutoff Frequency
Output Noise: Full Multiplex
Channel No. 20 Channel Frequency 124 KE 27.5%  BPIF: Signal -6,466 Noise: Full Mult1066 Search Ch. Only -10,466
Deviation Ratio
Output Noise: Full Multiplex
Channel No. 21 Channel Frequency 165 KC ± 7.5%  BPIF: Signal-4,21 Noise: Full Mult8.0 db Search Ch Only -8.0 db  Deviation Ratio
LPOF Cutoff Frequency
Output Noise: Full Multiplex

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### FIGURE II-3. 4-6 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Standard 1R16  IF Signal-to-Noise Ratio 9db	+93,124\$1654c ±7.5% Cha AGC Voltage - 4. Dude
Channel No. Channel Frequency  BPIF: Signal - 25. Noise: Full Mult  Deviation Ratio	5- 45 cps CA 10 upo 65 murms
Channel No. 25   8   Channel Frequency 7  BPIF: Signal - 11, 6   Noise: Full Mult  Deviation Ratio	20.6d Search Ch. Only -21.7db 5 1050 cps CA 1048P 154 myrms
Channel No. #19 Channel Frequency C BPIF: Signal -5.46 Noise: Full Mult Deviation Ratio	5- 1395-cps CA 100PP 92 murms
Channel No. 20 Channel Frequency BPIF: Signal-5.5db Noise: Full Mult Deviation Ratio LPOF Cutoff Frequency Full Bandwidth Voltage Output Noise: Full Multiplex Search Channel Only	1860 cps CA 100 pp 140 myms
BPIF: Signal -2.7db Noise: Full Mult Deviation Ratio	3- 2475-695 CA

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Name W. Bishon Date 1-27-65

### FIGURE II-3. 4-6 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Standard 1816 + 93, 1248/65 KC ±7.5% Channels IF Signal-to-Noise Ratio 14db AGC Voltage - 4. Oudc
Channel No. Channel Frequency 3.0 KC ±7.5%  BPIF: Signal -24.7d Noise: Full Mult42.5d Search Ch. Only -56.8d Deviation Ratio
Output Noise: Full Multiplex
Channel No. 78 Channel Frequency 70 KC ±7.5%  BPIF: Signal -//.5db Noise: Full Mult25.7db Search Ch. Only -26.6db  Deviation Ratio
Full Bandwidth Voltage
Channel No. 19 Channel Frequency 93KC ±7.5%  BPIF: Signal - 5.0 db Noise: Full Mult23.2 db Search Cn. Only -23.6 db  Deviation Ratio
Full Bandwidth Voltage
Channel No. 20 Channel Frequency 124 KC ±7.5%  BPIF: Signal - 5.23 Noise: Full Mult 20.01 Search Ch. Only - 20.34 Deviation Ratio
LPOF Cutoff Frequency
Channel No. 2 Channel Frequency /65KC ± 7.5%  BPIF: Signal -26db Noise: Full Mult/7.1 db Search Ch. Only-/7.0 db  Deviation Ratio
Full Bandwidth Voltage

3.15

### FIGURE II-3, 4-6 (CONTID.) SIGNAL-TO-NOISE TEST DATA

BPIF: Signal -24.6db Noise: Full Mult Deviation Ratio LPOF Cutoff Frequency	5- 45.05 CA 10080 6.5 muyms
Deviation Ratio  LPOF Cutoff Frequency  Full Bardwidth Voltage  Output Noise: Full Multiplex.  Search Channel Only.	-42.5-db Search Ch. Only -54.5-
Deviation Ratio LPOF Cutoff Frequency Full Bandwidth Voltage Output Noise: Full Multiplex. Search Channel Only.	5- 45.05 CA 10080 6.5 muyms
Full Bandwidth Voltage Output Noise: Full Multiplex	10000 6.5 murms
Full Bandwidth Voltage Output Noise: Full Multiplex	10000 6.5 murms
Search Channel Only	<u>6.5 murms</u> 3.5 murms
Search Channel Only	3.5 murms
nannel No. 78 Channel Frequency	70 KC + 750%
BPIF: Signal -//, 5 db Noise: Full Mult Deviation Ratio	
LPOF Cutoff Frequency	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	41 murms
nannel No. #19 Channel Frequency	93 KC +7.5%
PPIF: Signal - 5.0db Noise: Full Mult	
Deviation Ratio	
LPOF Cutoff Frequency	1375 EPS C/7
Full bandwidth Voltage	70075
Output Noise: Full Multiplex,	· A B M J F M S
Search Channel Only	a worms
	124KC ±7.5%
BPIF: Signal - 5, 2dh Noise: Full Mult	23.6dh Search Ch. Only-24.7db
Deviation Ratio	. 3
LPOF Cutoff Frequency	-1860 cps C2
Full Bandwidth Voltage	· /0 UPB
Output Noise: Full Multiplex	- 32 myrm3
Search Channel Only	· 7d myrms
annel No. #21 Channel Frequency	165 KC + 7.5-96
BPIF: Signal - 2.4 db Noise: Full Mult.	21.4db Search Ch. Only-21.4db
Deviation Ratio	
LPOF Cutoff Frequency	
Fall Bandwidth Voltage	· 10 J P P'
Output Noise: Full Multiplex	43 murms
Search Channel Only	. 4/murms

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Name W. Bishop Date 1-27-65

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## FIGURE II-3. 4-6 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Seandard IRIG .  IF Signal-to-Noise Ratio (HS 100000)	+ 93, /24, \$165 KC 17.5% AGC Voltage - 4 0, dc
Channel No. 21 Channel Frequency	165 KC ± 7.50% (5/4) = 11db
BPIF: Signal-2.6 db Noise: Full Mult.	Search Ch. Only -12,7db
Deviation Ratio	. 3
LPOF Cutoff Frequency	. 2475 eps CH
Full Bandwidth Voltage	· 10 upp +13.42
Output Noise: Full Multiplex	
Search Channel Only	
Channel No. 21 Channel Frequency  REPIF: Signal (17/1) Noise: Full Mult	165 FC ±7.5 % (5/x)c = 9db
BPIF: Signal -2.7 1b Noise: Full Mult.	Search Ch. Only - 12.3
Deviation Ratio	· 5
LPOF Cutoff Frequency	. 2475 CP. CA
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	. 136 murms - 15.0db
Channel No. 2/ Channel Frequency_	165 KC = 7.5% (5/2) c= 6db
BPIF: Signal - 3.0db Noise: Full Mult.	Search Ch. Only -10.6 db
Deviation Ratio	. 1
LPOF Cutoff Frequency	7475-605 (4
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	. 230 murms -10.5 db
Search Channel Only	· A DO MINAMS - IU. D & B
Channel No. 21 Channel Engagement	165 KC + 7.5% (3/4) = 4db
Channel No. 2 Channel Frequency  BPIF: Signal 3.7 db Noise: Full Mult.	Search Ch. Only - 9, 0 d/
	Search Ch. Only -7.042
Deviation Ratio	. 2475 · · · · · · · ·
LPOF Cutoff Frequency	
Full Bandwidth Voltage	· 10 upp + 13.4db
Output Noise: Full Multiplex	
Search Channel Only	. 620 muyms -2.0db
	1 1 1 ( ) ( ) ( ) ( ) ( ) ( ) ( )
Channel No. 21 Channel Frequency	
BPIF: Signal -2, L Noise: Full Mult.	Search Ch. Only -12.7
Deviation Ratio	. 5
	2475
Full Bandwidth Voltage	100PP +13,4db
Output Noise: Full Multiplex	
Search Channel Only	. 130 my vms -15.6db
	[NO Modulation Input to any
•	(vco
5-65 · -234-	•
<i>5.</i> <sup>+3</sup> -234-	

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## FIGURE II-3, 4-7 SIGNAL-FO-NOISE TEST DATA

System Description: Channel 1-19 4H  IF Signal-to-Noise Ratio 4db	Proportional Bandwidth  ALIC Volkage - 4.0 Vdc
Channel No. H Channel Frequency	
BPIF: Signal-0.1 D Noise: Full Mult.	
Deviation Ratio	
LPOF Cutoff Frequency	
Full Bardwidth Voltage	10werp
Output Noise: Full Multiplex	1150 my
Search Channel Only	1100 mv
Channel No. 19 Channel Frequency	93 kc = 7,5%
BPIF: Signal -9.546 Noise Full Mult.	-12.4db Search Ch. Only -12.6db
Deviation Ratio	5
LPOF Cutoff Frequency	1400 CRS CA
Full Bandwidth Voltage	IOVOLO
Output Noise: Full Multiplex	- 750mv
Search Channel Only	. 660my
Channel No. 18 Channel Frequency	70kc = 7,5%
BPIF: Signal -11.8db Noise: Full Mult.	-13,9db Search Ch. Only -14,7db
Deviation Ratio	5
1.POF Cutoff Frequency	1050cps CA
Full B <b>andw</b> idth Voltage	NVp-p
Output Norse: Full Multiplex	1500my
Search Channel Only	. 1200 mv
Channel No. 8 Channel Prequency	3.0kc \$7.5%
BPIF: Signal -25.5db Noise: Full Mult.	-29.446 Search Ch. Only -31.8do
Deviation Ratio	
LPOF Cutoff Frequency	45 cps CA
Full Bandwidth Voltage	10Vp-p
Output Noise Full Multiples	1100 mV
Search Channel Only	600 mV
Channel No Channel Frequency_	
DPIF: Signal Noise: Full Mult.	Search Cli. Only
Deviation Ratio	•
LPOF Cuton Frequency	• · · · · · · · · · · · · · · · · · · ·
Full Bandwidth Voltage	•
Output Noise: Pull Mulliplex	
Search Channel Only	

10f5

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1 me WSB/MDL Date 2-1-6,5

# FIGURE II-3. 4-7 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

	raportional Bandwidth
IF Signal-to-Noise Ratio 9 db A	THE TOTAL
Channel No. H Channel Frequency 163  BPIF: Signal Odb Noise: Full Mult7.  Deviation Ratio	950ces CA
Search Channel Only	
Channel No.   9   Channel Frequency   9   BPIF: Signal   10   Noise: Full Mult.   17   Deviation Ratio	5 KC = 7.5000 1400 Search (h. Oniy - 17.200 100 cps CA 100 Cps CA
Search Channel Only 1	ZOMV
Channel No.   8   Channel Frequency   70   BPIF: Signal   -12.9d   Noise: Full Mult26   Deviation Ratio	2.2d Search (h. Only -20.4db
Channel No. Channel Frequency 3 BPIF: Signal - 25.845 Noise: Full Mult 4/Deviation Ratio	15 cus CA
Channel No. Channel Frequency  BPIF: Signal Noise: Full Mult.  Deviation Ratio	

2 of 5

# FIGURE II-3. 4-7 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channel 1-19+H	Proportional Bandwidth
IF Signal-to-Noise Ratio 14db	ACC Voltage -4.0Vdc
Channel No. # Channel Frequency_	165kc ±15%
BPIF: Signal +0.6de Noise: Full Mult.	-11.3db Search Ch. Only - 1/3dl
Deviation Ratio	. 5
LPOF Cutoff Frequency	
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	
Channel No. 19 Channel Frequency_	076, ±7.52
Channel No. 9 Channel Frequency BPIF: Signal -9.26 Noise: Full Mult.	-Olla Search Ch. Only -Olla
Deviation Ratio	5
LPOF Cutoff Frequency	
Full Bandwidth Voltage	INVan
Output Noise: Full Multiplex	
Search Channel Only	
Channel No. 18 Channel Frequency_	70ke 17.5%
BPIF: Signal 12.10 Noise: Full Mult.	-24,1db Search Ch. Only -24,30
Deviation Ratio	
LPOF Cutoff Frequency	
Full Bandwidth Voltage	10 V p-p
Output Noise: Full Multiplex	· 102m/
Search Channel Only	100 mx
Channel No. 8 Channel Frequency	3.0Kc =7.5%
BPIF: Signal - 74,600 Noise: Full Mult.	-42, db Search Ch. Only -52.5
Deviation Ratio	· <u>5</u>
LPOF Cutoff Frequency	45cps CA
Full Bandwidth Voltage	10/p-p
Output Noise: Full Multiplex	. 9.0my
Search Channel Only	. 5, 2mv
Channel No. Channel Frequency	
Channel No. Channel Frequency BPIF: Signal Noise: Full Mult.	Search Ch. Only
Deviation Ratio	
LPOF Cutoff Frequency	•
Full Bandwidth Voltage	•
Output Noise: Full Multiplex	
Search Channel Only	

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# FIGURE 11-3.4-7 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

System Description: Channe / 1-197	H Proportional Bandwidth AGE Voltage -4.0 Vdc
IF Signal-to-Noise Ratio 19db	ACC Voltage - 7.0 V dc
Channel No. H Channel Frequence BPIF: Signal +0.9db Noise: Full M Deviation Ratio	ult15.7db Search Ch. Only-15.7db
LPOF Cutoff Frequency	. 4950 eps CA
Output Noise: Full Multiplex	· <u>- 61 mv</u>
Channel No. 19 Channel Frequence BPIF: Signal - 2.24 Noise: Full M Deviation Ratio	ult25.3db Search Ch. Only -25.5db
LPOF Cutoff Frequency Full Bandwidth Voltage	· · 1040-0
Search Channel Only  Channel No. // Channel Frequence	28,5 mv
BPIF: Signal -11.6de Noise: Full Me Deviation Ratio	ult2866 Search Ch. Only -28.766
LPCF Cutoff Frequency Full Bandwidth Voltage Output Noise: Full Multiplex	· 10/10-10
Search Channel Only	. 56 mv
Channel No. B Channel Frequence BPIF: Signal - 23,9 & Noise: Full Mu	y 3.0kc ±7.5%  ult42 db Search Ch. Only -53 db
Deviation Ratio	
Output Noise: Full Multiplex Search Channel Only	· 5.8 mv
Channel No. Channel Frequence	Y
BPIF: Signal Noise: Full Ma	ait. Search Ch. Only
Deviation Ratio	• •
LPOF Cutoff Frequency	•
Full Bandwidth Voltage	, .
Output Noise: Full Multiplex	• •
Search Channel Only	*

4 of 5

# FIGURE II-3. 4-7 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

	AGC Voltage - 1/20 AGC
F Signal-to-Noise Ratio (45 Kisted)	
Channel No Channel Frequency Noise: Full Mult.	165 KC = 13 % (3/N)c= 11
BPIF: Signal - O Noise: Full Mult.	Search Ch. Only -9.5
Deviation Ratio	•
LPOF Cutoff Frequency	. 4950cps CA
Full Bandwidth Voltage	
Output Noise: Full Multiplex	•
Output Noise: Full Multiplex	· 13801403 -15da
Channel No. L.J. Channel Frequency BPIF: Signal Odb Noise: Full Mult.	16512 + 15% (7) 6 70h
BPIF: Signal Odk Noise: Full Mult.	Search Ch. Only - '/ ', s
Deviation Ratio	
LPOF Cutoff Frequency	443:300 60
LPOF Cutoff Frequency	· 1000 + 124ab
Output Noise: Full Multiplex	
Search Channel Only	· 25010/15
Channel No. H Channel Frequency BPIF: Signal -0.1db Noise: Full Mult.	1/10- +15-3/ (5/4) = 6 3/4
DDIE Signal Odd Noigh Full Mult	Search Ch. Only - 5°C //
Deviation Patie	bearen en. omy -57577
Deviation Ratio	·
LPOF Cutoff Frequency	· 777 5 cps
Full Bandwidth Voltage	· 10 1134 db
Output Noise: Full Multiplex	•
Search Channel Only	· /d5muy0.512
	11 - 11 - 1 ( + 1) ( + 1)
Channel No. H Channel Frequency BPIF: Signal -0.4 db Noise: Full Mult.	1:3 +15 : (4/1) c - 11e
	Search Ch. Only - 2 12 ,
Deviation Ratio	•
LPOF Cutoff Frequency	
Full Bandwidth Voltage	LUUPP +13.4dk
Output Noise: Full Multiplex	
Search Channel Only	1250 muxmi +4.246
Channel No. Channel Frequency BPIF: Signal Noise: Full Mult.	
BPIF: Signal Noise: Full Mult.	Search Ch. Only
Deviation Ratio	•
LPOF Cutoff Frequency	•
Full Bandwidth Voltage	
Output Noise: Full Multiplex	
Search Channel Only	
Tour on The many &	

Name W. Bishop Date 2-9-65-

# TABLE II-3.4-8 SIGNAL-TO-NOISE TEST DATA

1

•	÷	+	. 2	ا ا انت					,	į		
3.00	System: LONSLONE DAM DINAM(S/N)c:	777	ひとこ	5) 12:10	- 1 1	000	AGC: -4,0V		Output FBW Signal:	W Signal:	5,5	apm
	CHANNEL	EL				INPUT				OUTPUT	JUT	
					Notes	180	(N/S)	M.	••ioN	•	P(N/S)	P(N
£		ă	LPOF	Signal dbm*	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db
	Measurenents	200	to make	de 11.1	th d		cham.	2. /2	7 60	center	Freshe	Series S
0	560kc	7	1.0 kc	-15.2	22/-	-17.6	4.	7. 7	7.8	7.4	ス・ジ・	79.
10	88.0kc	33	1.3kc	-14.5	1.2%	-16.4	2.4	7.7	6.8	6.6	3.2	3.4
14	120.0kc	7	1. J. Kc	8.41-	-17.5	-175	2,7	2.7	6.9	6.4	3.	3.
61	160.0kc	K	1.0kc	-15.5	-18.5	-18.5	3.0	3.0	6.3	6.3	3.7	3.7
14	120.0 kc		2.Ckc	-/4.8	-17.5		2.7		7:11		-111	
61	120.0 kc	7	.). 5 Kc	8%/-	-17.5		2.7	-	4.4		5.5	
	Measurchichts made	ن ع	nts m		11210	test	1.	channel	ati	aigh b	$z_{ii}d$	: 26/6
14	120.0kc	3	1.0 kc	-14.8	-175		2.7		15.4	,	-0.4	,
14	120.0 kc	_	2.0kc	87/-	521-		2.7		13.3	-	-33	
11	120.0kc	7	-0.5 k.	8.41	-175				8.0		2 O	
	Measuremiles	7.778	para :	24	10	250	chu	7/1	usca	pool		
14	14.J.JKC	13	1.0kc -1	·	-125		K.7.		11.2	1	2%	1
///	120,0 kc	`	40	];	14		7.7	!	13. )		۲. ۲.	
[///]	- 1	4	1.5.4	127	321		\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \	ţ	9.5		7.7	

1 ct 7

Syste	System: Constant Bandwidth	4	bandwid!	1	(S/Mc: 7.0db	1	AGC: -401		Output FBW Signal:	3W Signal	10.0	4mqp
	CHANNEL	EL		,		INPUT				OUTPUT	PUT	
					Noise	180	(N/S)	Ę.	Noise	:	/s)	F(N/S)
ż	Frequency	DR	LPOF	Signal dbm*	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Bearch Chennel Only db
	Test c	127	Test channel at	U	enter	Fresu	-resuency:					
૭	56.0 kc 2	4	1.0kc	-16.6	-21.7	-21.7	5.7	5.1	2.0	2,0	80	8.0
0	88.0 kc	B	1.0kc	-15.3	-30.4	-20.4	5.1	2.1	1.0	1.0	9.0	0.0
14	123.0 kc	B	1.0 kc	-75.3	-2.2,5	-20.5	5.2	5:5	1.5	1.5	8.5	8.5
61	160.0 kc	3	1.0kc	-15.9	-21.3	-21.3	4.4	4.4	6.8	0.8	9.2	9.3
14	120.0 kc	_	2.0kc	-15.3	-30.5		5.2	}	7.6		2.4	ļ
14	120.0 kc	7	0.5kc -15	-/5.3	-20.5		5.3	1	-1.0	1	0.9	ļ
	Test channel at	han	nel at	high	ban	deade	٠,	•				
//	120.0 Kc	K	1.0kc		-20,5	ار	5.2	1	9.0		1.0	
14	120.0kc	`	2.0kc	-15.3	-20,5	1	5.2	1	12.0	1	-2.0	
6/	120.0kc	7	0.5kc -15.3	-15.3	-20.5	1	5.2		6.2		3.8	1
	Test channel modular	han	ow lad	<b>T</b> .	:pə	,						
14/	123.3 kc	K	1.0kc -15.3	-/5.3	-20.5		5:2		7.8		2.2	
14	1230,050	\	4.0 kc	/57.3	-20.5	1	5.23		10.0		0.0	
14.	7.	7	27.7%	1.5	-20.5		5.2	1	4.5	, and .	1,,	

\*db reference its one milliwatt into 600 ohms.

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CHANNEL  CHANNEL  No. Frequency  No. Frequency  Test ch el at centrer trepering dbm*  Toolo ke 2 1.0 ke -15.7 -23.1 -23.1  14 120.0 ke 2 1.0 ke -16.3 -23.8 -23.8  14 120.0 ke 2 1.0 ke -15.8 -23.1 -23.1  14 120.0 ke 2 1.0 ke -16.3 -23.8 -23.8  14 120.0 ke 2 1.0 ke -16.3 -23.8 -23.8  14 120.0 ke 2 1.0 ke -16.3 -23.8  14 120.0 ke 2 1.0 ke -15.8 -23.1 -23.1  15 15 15 15 15 15 15 15 15 15 15 15 15 1	Full Multiplex dbm*  -23.1  -23.1  -23.1	oarch tannel Only bm* x-1/c 24,5 24,5 23,1	(S/M) <sub>s</sub> Full Charletplex Char	arch annel while the state of t	Full Multiplex dbm*	N D		(S/N) <sub>d</sub> Search Channel only db //2,5 //3,5 //3,5
Post   Frequency   Signal   Multiplex   Channel   Chan	Full Multiplex dbm*  7	oarch tannel Only Ibm* 24,5 24,5 23,1 23,1	2	arch annel anly db	Full Multiplex dbm*  -2,5  -3,5		(S/ Full Multiplex db /2,5 /3.5	Search Channel Only db //3.5
LPOF   Signal   Multiplex Only	Full Multiplex dbm*  74.5  -23.1  -23.1  -23.1				Full Multiplex dbm*  -2,5  -3,5		Full Multiplex db /2,5 /3.5	Search Channel Only db /2,5 /3.5
Test chiniel at conter trepuring  56.3 ke 2 1.0 ke -17.0 -24.5  88.0 ke 2 1.0 ke -15.7 -23.1 -23.1  120.0 ke 2 1.0 ke -15.8 -23.1 -23.1  120.0 ke 2 1.0 ke -16.3 -23.8  120.0 ke 1 2.0 ke -15.8 -23.1  120.0 ke 1 2.0 ke -15.8 -23.1  Test channel at high kixindedie	-23.1 -23.1 -23.1 -23.1				-3.5 -3.5 -3.5	dbm* -2.5 -3.5	12,5 13.5 12.5	12,5 13.5 13.5
56.3 kc 20 kc -17.0 -24.5 -24.5 88.0 kc 20 kc -15.7 -23.1 -23.1 120.0 kc 20 kc -16.3 -23.8 -23.8 120.0 kc 20 kc -16.3 -23.8 -23.8 120.0 kc 1 2.0 kc -15.8 -23.1 120.0 kc 1 0.5 kc -15.8 -23.1 Test channelt high k.xiidedije	-23.1 -23.1 -23.1 -23.1	<b>7</b> :	7377		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-2.5 -3.5	12.5	13.5
88.0 kc 2 1.0 kc -15.7 -23.1 -23.1 120.0 kc 2 1.0 kc -15.8 -23.1 -23.1 160.0 kc 2 1.0 kc -16.3 -23.8 -23.8 120.0 kc 1 2.0 kc -15.8 -23.1	-23.1 -23.1 -23.8 -23.1	-23.1 -23.1	7.7.7	122	13.5	-3.5	13.5	13.5
120.0 kc 2 1.0 kc -15.8 -23.1 -23.1 160.0 kc 2 1.0 kc -16.3 -23.8 -23.8 120.0 kc 1 2.0 kc -15.8 -23.1 120.0 kc 4 0.5 kc -15.8 -23.1 Test channel at high kandedge	-23.1 -23.8 -23.1	23.1	7.3	-	-3.5		72.5	13.5
160.0 kc 2 1.0 kc -16.3 -23.8 -23.8 120.0 kc 1 2.0 kc -15.8 -23.1 120.0 kc 4 0.5 kc -15.8 -23.1 Test channel at high kandedge	-23.8	23.8	7.7		•	-3.5	111	2
120.0 kc 1 2.0 kc -15.8 -23.1 — 120.0 kc 4 0.5 kc -15.8 -23.1 — Test channel at high kandedge			·	0.7	14.0	0%-	14.0	2
4 0.54c -15.8 -23.1		1	7.3	[	3.2		80.00	
et high kendedge		1	7.3		9.6	ŀ	19.8	1
	Ernd	edije:						
14 120.0Kc 2 1.0Kc -15.8 -23.1 -		<u> </u>	7.5		4.4		5.6	;
14 120.0kc 1 2.3kc -15.8 -23.1 -	1	1	7.3		1.8		6.7	1
17 120.04c 4 0.54c -15.8 -23.1 -		1	30 %	1	1.5	1	8.5	
Test channel modulated:	7				,			
		1	7.3	1	7.7		7.9	*
14 1230kc 1 2.0kc -15.1 -23.1		-	73	-	5.3	(	4.7	,
14 123.24c 4 254c 15.5 -23.1 -	::		7.3		-1.5	i	11.5	1

\*db referenced to one milliwatt into 600 ohms.

Name; 2. 6. ... Date: 3-25-65

Syste	system: Constant Bendungth	الد	Barrelmist		(s/N)c: 15.0 db	_	AGC: -40V	10	Output FB	Output FBW Signal: 10.0	10.0	4pm*
	CHANNET	73				INPUT				OUTPUT	PUT	
					Noise	981	•(N/S)	٤	Notes	0 0	/s)	P(N/S)
ź	Frequency	DR	LPOF Frequency	Signal dbm*	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplez db	Search Channel Only db	Full Multiplex db:n*	Search Channel Only dbm*	Full Multiplex	Search Channel Only
	Test channel	22	110/21	cente	170	. C. J. COMOV.	10/2					
v	56.0kc	रि	kc	1	-27.2		12.0	10.0	6.9-	-7.0	16.9	17.0
0/	88.0kc	B	1.0kc	-15.9	-25.6	-25.7	~~	2.8	7.6	-7.7	17.6	17.7
Ξ	120.0 Kc	R	1.0kc	-16.0	-25.6 -25.6	-25.6	'3 %	9.6	-6.8	6.5	16.8	19
9	160.0 kc	R	1.0kc	-16.6	-26.3	-26.3	V.9.	9.7	-7.3	-73	17.3	17.3
Ξ	120,0 Kc	~	2.04c	-16.0	-25.6	-	0;		0.0	1	001	
7.	120.0 kc	7	0.5kc	-16.0 -25.6	-25.6		9.6		-18.0	1	28.0	1
	Test channel	me	1 at	dient	5.2460	3,96:					,	
Ξ	120.0kc	n	1.0kc	-16.0	-25.6	71	9.6	1	-2.5		15.77	1
Ξ	120.0kc	~	2.0kc	-16.0	-25.6	-	9.6		3.2	1	00.00	1
<u>z</u>	120.0kc	7	0.540 -16.0	16.0	6.55.		0.		-72		/7.2	
	Test channel modula	14 11	ou for	dela	19.							
2	120.0kc	N	1.0 Ac	-16.0	-25.6	1	9.	;	011-		14.0	1
H	123.40	\	2.0kc -16.	16.5	- Y		9.0	j	0.7		33	İ
7	2.2.04c	7	0.5kc -1:	1 1	V. 33		19		-10:0		20.0	

			-									
	CHANNEL	Er [				INPUT				OUTPUT	TUc	
					Noise		*(N/S)	<b>5</b>	Noise	8.9	/s)	P(N/S)
				ı	11 - 3	Search	:	Search	:	Search		Search
			LPOF	Signal	r u.u Multinlex	Channel	Full	Channel	Full Multiples	Channel	Full	<u>ပ</u>
ટું	Frequency	DR	Frequency		dbm*	dbm*	đb	dp (	dbm*	dbm*	dp dp	<u>}</u> &
	Test a	chamie	De lon	conter	+ 10%	الماري: الماري الماري: الماري	.K. M.					
હ	56.0kc	7	1.0 kc	-173	-30,7	-30.8	13.4	13.5	7,01-	1.2.7	20.1	んだ
2	88.0 Kc	റ	1.0 kc	-/6.1	-230	-230	12.9	12.4	-11.3	-11.3	21.3	21,3
7	120.0kc	Ŋ	1.Jkc	-16.2	-29.1	-29.2	12.4	13.3	-10.6	-10.6	30,00	23.6
61	160,0kc	B	1.0kc	-16.9	-29.9	-30,0	13.0	13.1	-10.9	-11.1	20.9	21.1
*	120.0kc	`	2.0 kc -16,2 -29.	-16.2	-29.1	1	12.9		-3.9		13.9	l
*	123.0kc	7	0,540	-16,2	-29.1	(	12.9	-	-22.5	1	32.5	l
	Test channe	ואווה	at high		Annabe	·. .v						
5/	120.0 kc	7	1.0kc		-29.1		12.9	1	-10.5	1	20.5	
7.1	120.0kc	~	2.0kc	-16.2	-24.1		12.9	1	-1.9		6%	·
2.	120.0kc	7	0,5 Kc	-16.2	1.62-		12,9	1	-22,5	1	32.5	-
	Test chamic	2111	mobilar	ated								
2	120.0 kc	N	1.0kc	-4.2	-29.1		12.9	i	-11.0		21.0	
	120.0 Kc	`	2.0 kc	-16.2	1.72-	-	12.9		-3,3	4	13.3	
	120,0kc	7	2,5%	-14.2	-21.1		12.9		-22.5		32. 1	<u>!</u>

\*db referenced to one milliwatt into 600 ohms.

Name: (1987) 121 Date: 3-25 65

TABLE II-3.4-8 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

Syste	System: Constant Janlo 111	7	1. Glac		(S/Mc: 21.0 Jb AGC: -4.0V	980	AGC: -4	10,	Output FE	Output FBW Signal: 10.0	10.0	*m49
	CHANNEL	73				INPUT				OUTPUT	PUT	
					No	Noise	(S/N).	Î.	No	Noise	/8)	P(N/S)
<b>.</b>	Frequency	DR	LPOF Frequency	Signal dbm*	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db
	12 test ch	channe	10/ 25	100	tor	freg	fr equancy	.,				
<b>9</b>	56.0kc 2	N	1.0kc	-17.4	-33.0	-33.2	15.6	15.8	-13.1	-13.1	23.1	23.1
0	88.0 kc	7	1.0 kc -16.	-16.2	-31.5	-31.7	15.3	15,5	-13.5	-13,7	23.5	73.7
2	120.0 kc	77	1.0K1	16.4	-31.5	-31.7	12:1	15,3	-13.0	-/3./	23.0	23.1
61	160.0 kc	Ŋ	1.0 kc -16.9	-16.9	-32,2	-32.2	15,3	15.3	1.21-	-13.4	73.1	23.4
17	120,0 kc		2.0 kg	-16.4	-31.5	İ	15.1		-6.3		16.3	
7.	120.0kc	3	1.5 kc	16.4	-31.5	1	15:1	(	-24.9	1	34.9	
	Test chame	am	el at	- hig	بدرا	1. Lade	 01		'			
1	120,0 kc	Н	1.0 kc	-16,4	1	1	12:1	į	- 13.1		23.1	
I	120.0 kc	_	2.0kc -16.	-16,4	-31,5	{	15.1		14.0	i	14.0	1
7	123.0 kc	7	0,546 -16.	16.4	5.18-	1	12:1	1	-24.9		34.9	-
	Test channel	271	el modula	ulate	```					,		
4/	120.0 kc	n	10kc	- 16.4	-31.5	İ	5.	1	-13.6		23.6	l
1.1	120.0 Kc	_	2.0 Kc	16.31	-31.5		1.5.1		-5.6		15.6	- (
7.	1230kc	7	ask:	1,'91-	-31.5	,	15,1		-23.9	-	33.4	1

(S/M).	P(N/c)	Search Full Channel Multiplex Only	-	27.0 27.0	27.1 27.4	26.3 26.6	26.6 26.8		38.4		26.5	17.2	38.6		220	18.3	36.5
		Channel Only dbm*		-17.3	-17.4	-16.6	-16.8	-	1						1		
Noise		Full Multiplex dbm*		-17.0	1.7.1-	-16.3	-16.6	-9.3	-28.4		-16.5	-7,2	-38.6		CZ1-	0.8-	-26,5
(S/N)	8,	Channel Only db		19.2	18.9	18.6	18.8	}	1		1	[			-		
/s)		Full Multiplex db	;	18,7		18,3	18,4	18.3	18,3		18,3	18,3	18.3		18.3	2.31	18.5
Noi se	Search		fre-jonnay:	-36.7	-35.2	-35,1	-35.9	1	l	cdye:	,	1	į.			1	(
Š.		Full Multiplex dbm*	14 - 1a	-36.2	-34.8	-34.8	-35,5	8'18-	348-	barndedges	-34,8	2.48-	248-		-34.8	-348	-34.8
	4	Signal dbm*	cent	1.0kc -17.5	-16.3	-16.5	1.7.1	-16.51	16.5	4	ما <u>ق</u>	-165	-16.5	modulate	-16,5	-16.5	-16.5
		LPOF Frequency	el at	1.0 Kc	1.016	1.0kc	1.0kc	2.0kc -16	0.544-16.5	el at	1.0 kc	2.0 kc	0.5kc -16.5		1.0kc	2.0kc	J.5kc
		DR	run Lun	N	Ŋ	7	Ŋ	-	ゴ	ann	U	-	2	Zhn	Ŋ	_	7
		Frequency	Test channe	56.0kc	88.0kc	120.0kc	160.0 kg	120.0 kc	120.0KC	Test channel	120.0 kc	120.0 kg	120.0 ke	Test chainel	120.0 kc	120.0 kc	120.0kc
		%		9	0	I	<u>-</u>	<u> </u>	I		エ	<u> </u>	7.		7	<u></u>	三

\*db referenced to one milliwatt into 600 ohms.

Name; 4/58/1/1 L Date: 3-25-65

Syste	System: Cambin it iona	47	iona		(s/Mc: 6.0db	1	19C: -4.0V	101	Output FE	Output FBW Signal: 16.0	. 76.0	4pm*
	CHANNEL	VEL				INPUT				TUATUO	PUT	
					No.	Noise	8(N/S)	Z.	No	Noise	/s)	P(N/S)
ટ્રે	Frequency	DR	LPOF Frequency	Signal dbm*	Full Mukiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dhm*	Search Channel Only	Full Multiplex	Search Channel Only
`	Test channel	43	mel at	Cent	4 10	vaus.	10				3	8
	56.JK.	7		1.87-	-2/2	-22.6	3.6	4.5	6.0	4.4	4.0	5.6
9 :	88.0 kc	n		-18,2	-22.4	-23.1	4.2	4.9	m m	1.5	6.7	8.5
<i>Y</i> !	120.0 kc	<u>u</u>	1.040	ンメノー	-23.8	-23.8	8.7	4.8	3.5	2,3	6.5	ノン
6 0	160.0kc	7	1.0 Kc	-186	-25.1	-24.8	5.5	5,2	2.2	<b>L</b> 3.7	7.80	(A)
8	5,0 kc	را د	4578	-15:4	-36.6	-28.4	10.2	13.5	-19.7	-22,2	27.7	32.2
	Test	cha	channel	r t	bundedges	sopo.						
74	120.0 Kc	7	1.0kc -19.0		-23.8		4.8	1	75.5	1	2.5	
00	3.0 kc	5	4545 -154		-26.6	-	10.2		-200	]	33.0	1
,	Test channel modula	ur	nel m	dulas	; pu						,	
7.7	120.0kc	N	1.0kc -19.0		-23.8		4.8		7.2		2,0	
00	3.0 kc	40	45cps	-15.4	-26.6		13,2	1	-21.0		31.0	
							,					
					·							
									•		-	

1.U. I NIOO) 4-2-6-11 31711111

SIGNAL-TO-NOISE TEST DATA

Syste	System: Combinations	to	ono/	s)	(S/M)c: 9.0db		AGC: -4.7V	1	Output FBW Signal: 10.0	W Signal:	10.0	4pm*
	CHANNEL	EL				INPUT				OUTPUT	TUG	
					Noire	9.1	(N/S)	3.	Noise	0	P(N/S)	P
ż	Frequency	DR	LPOF Frequency	Signal dbm*	Full Multiplez db:n*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex	Search Channel Only
	Test channel	177	101	cent	center frequen	coner	U)					
૭	56.0 kc	4	1.0kc	-19.2	-27.2	-28.0	0.0	% %	14.0	-5:5	0.41	15.5
0	88.0 kc	N	1.040	-18.0	-26.5	-26.8	8.5	\$5. \$2.	-5.8	6.6	15.8	16.6
<u> </u>	120.0kc	B	1.0kc	-18.5	-27.0	-27.0	8.5	8.5	12.11	-4.8	7.3	12.00
= 0	160.0kc	ત્ર	1.0 kc	-19.0	-27.8	-27.5	80	8.5	44-	-5.0	14.41	15.0
<b>20</b>	3.0kc	P)	45cps	14.2	-34.3	-42.8	20.1	28.6	-32.0	-375	42.0	475
	Test channel at band	anr	el at		sakpa							
14	120.0kc	8	1.0kc	-18.5	0.72-		8,5	!	0.8		2.2	)
∞	3.0 kc	6	45cps	-/42	-34,3	1	28		-32.0		42.0	
,	Test channel modulat	なな	er mo	Julat	ip:							
14	120.0 kc	8	1.0kc	-185	-27.0		2.5		-1.0		11.0	
80	3.0 kc	70	245.75	-14.2	-34.3		20.7		-31.0		41.0	1
	,				,					,		<del>7-</del> 8-9-9
								-		,		

20K7

Name: 1.74 7/12 Date: 3-20-05

TABLE II-3.4-9 (CONT'D.)

	ole in the second second		0710-1		S/N)c: //	9000	(S/N)c: /2.046 AGC: -4. JV	. JV	Output FI	3W Signal	Output FBW Signal: /J.	4pm*
	CHANNEL	EL				INPUT				OUTPUT	PUT	
-					No	Noise	(N/S)	N).	No	Noise	/s)	P(N/S)
			LPOF	Signal	Full Multiplex	Search Channel Only	Full	Search Channel Only	Full	87 C	Full	00
į	Frequency	Щ.	Frequency	dbm*	dbm*		đĐ	g g	dbm*	db *	dp	<u> </u>
	Test channel	han	the at		center fragional	Mac. I a	CV.					
9	56.0 kc	7	1.0 Kc	-19.0	-36.1	-30.6	/ '.'	11.6	100	8.8-	18.6	18.8
0	88.0 kc	7	1.0 kc	-17.9	-24.1	-29.1	1.2	11.2	-9.2	96-	.0.6/	13.6
7	120.0kc	<u>n</u>	1.0 kc	-18.2	-29.4	-29.4	11.2	1.2	7.4	-77	17.4	7.27
2	160.0kc	n	1.0kc	-18.8	-30.0		7.2	11.2	42-	187	11.5	: &
8	3.0 kg	2	45 cps	-13.8	-35.8	1	22.0	38.2	-39.7	7 7% -	1.67	
	Test channel it	AN	hel it	purg	bund cdoe:	,				j j		9 9
74	120.0 Kc	4	1.0kc	-18,2	-29.4	·	1.2	1	15.0	-	15.0	
٠	3.0 Kc	15	450,15 - 13.8	-13.8	-35.8		22.3		-43.5	1	なって	
	Test chamel	1211.	5111 Jo	_	€.						) )	
1-;	123.0 kc	N	1.0 kc	-18.2	7,85-	(	7.7		-8.0		18.0	
い	3.0kc	2	450,15	-13.8	-358	1	22,0		-36.5		% .y	
	·					·						
						<del>, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>						

No. Frequency DR Friquency dbm* Full Channel  Test Chi. Inc.   at cc. (Cr. tf.)  6 56.0kc 2 1.3kc -19.0 -33.0 -33.1  19 120.0kc 2 1.0kc -18.8 -30.6 -31.6  19 120.0kc 2 1.0kc -18.8 -32.5 -32.5  7 Fest Cha. Inc.   at ba. Inclage  19 120.0kc 2 1.0kc -18.3 -31.8  Test Cha. Inc.   at ba. Inclage  Test Cha. Inc.   at ba. Inclage  Test Cha. Inc.   at ba. Inclage  Test Cha. Inc.   at ba. Inclage  Test Cha. Inc.   at ba. Inclage  Test Cha. Inc.   at ba. Inclage  Test Cha. Inc.   at ba. Inclage  Test Cha. Inc.   at ba. Inc.   at ba. Inclage  Test Cha. Inc.   at ba.			INPUT				OUTPUT	PUT	·
Frequency DR Friquency Signal Multiplex  Test chii IIc   at cell condition  56.0 kc 2 1.3 kc -19.0 -33.0  88.0 kc 2 1.0 kc -18.8 -33.6  120.0 kc 2 1.0 kc -18.8 -32.5  3.0 kc 2 1.0 kc -18.9 -32.5  755 co co co co co co co co co co co co co	·	Noi	0	(S/N) <sub>s</sub>	5.8	No	Noise	/S)	P(N/S)
Frequency DR Friquency dbm* dbm* dbm*  Test chi, 110°   at conform  56.0 kc 2 1.3 kc - 19.0 - 33.0  88.0 kc 2 1.0 kc - 18.3 - 31.8  120.0 kc 2 1.0 kc - 18.8 - 32.5  3.0 kc 2 1.0 kc - 18.8 - 32.5  Test (ha. 10 kc - 18.3 - 31.8  3.0 kc 2 1.0 kc - 18.3 - 31.8  3.0 kc 2 1.0 kc - 18.3 - 31.8  3.0 kc 2 1.0 kc - 18.3 - 31.8  3.0 kc 5 45 cys - 13.6 - 36.1  7 cot channel modula ted: 120.0 kc 2 1.0 kc - 18.3 - 31.8  3.0 kc 5 45 cys - 13.6 - 36.1		Full	Search Channel	Full	Search Channel	Full	Search	Full	Search
Test chained at center 56.0ke 2 1.3ke -19.0 -33.0 88.0ke 2 1.0ke -18.3 -31.8 120.0ke 2 1.0ke -18.8 -32.5 3.0ke 2 1.0ke -18.8 -32.5 3.0ke 2 1.0ke -18.3 -31.8 3.0ke 2 1.0ke -18.3 -31.8 3.0ke 2 1.0ke -18.3 -31.8 3.0ke 5 45eps -13.6 -36.1 7 est chained modula ted: 120.0ke 2 1.0ke -18.3 -31.8 3.0ke 5 45eps -13.6 -36.1		Multiplex dbm*	Only dbm*	Multiplex db	Only dh	Multiplex dbm*		Multiplex db	Only db
56.0kc 2 1.3kc -19.0 -33.0 88.0kc 2 1.0kc -18.3 -31.8 120.0kc 2 1.0kc -18.8 -32.5 3.0kc 5 45eps -13.6 -36.1 7.0 okc 2 1.0kc -18.3 -31.8 3.0 kc 2 1.0kc -18.3 -31.8 120.0 kc 2 1.0kc -18.3 -31.8 3.0 kc 5 45eps -13.6 -36.1 3.0 kc 5 45eps -13.6 -36.1 3.0 kc 2 1.0kc -18.3 -31.8 3.0 kc 5 45eps -13.6 -36.1	ŀ	New York	froit	نازرر					
88.0 kc 2 1.0 kc -17.8 -30.6 120.0 kc 2 1.0 kc -18.8 -32.5 3.0 kc 5 45eps -13.6 -36.1 7 cst (2.0 kc 2 1.0 kc -18.3 -31.8 3.0 kc 2 1.0 kc -18.3 -31.8 7 cst (2.0 kc 2 1.0 kc -18.3 -31.8 3.0 kc 5 45eps -13.6 -36.1 7 cst (2.0 kc 2 1.0 kc -18.3 -31.8 3.0 kc 5 45eps -13.6 -36.1 3.0 kc 5 45eps -13.6 -36.1	1.3 kc -19.0	-33.0	-33,/	14.0	14.1	1.5	-11.7	21.5	27.18
120.0kc 2 1.0kc -18.3 -31.8 160.0kc 2 1.0kc -18.8 -32.5 3.0kc 5 45eps -13.6 -36.1 75st (13.1.10) at 61.11st 120.0kc 2 1.0kc -18.3 -31.8 3.0kc 5 45eps -13.6 -36.1 120.0kc 2 1.0kc -18.3 -31.8 3.0kc 5 45eps -13.6 -36.1 3.0kc 5 45eps -13.6 -36.1		-30.6	-31.6	12.8	13.8	-12.0	-12,3	22.0	22,3
166.0kc 2 1.0kc -18.8 -32.5 3.0kc 5 45eps -13.6 -36.1 75st (h3.1.10) 2 1.0kc -18.3 -31.8 3.0kc 5 45eps -13.6 -36.1 720.0kc 2 1.0kc -18.3 -31.8 3.0kc 5 45cps -13.6 -36.1 3.0kc 5 45cps -13.6 -36.1		-31.8	-31.8	13.5	13.5	-10.0	-10,2	20.0	20.2
3.0 kc 5 45eps - 13.6 Test (2 1.0 kc - 18.3 3.0 kc 5 45eps - 13.6 Test channel modula 120.0 kc 2 1.0 kc - 18.3 3.0 kc 5 45eps - 13.6			-325	137	13.7	-10.1	-10.5	20.1	20.5
Test (23.110   at 6 120.0 kc 2 1.0 kc - 18.3 3.0 kc 5 45eps - 13.6 Test channel modula 120.0 kc 2 1.0 kc - 18.3 3.0 kc 5 45eps - 13.6	45eps -13.6	1.98-	-55.1	22.5	22.5	-46.3	-49.5	56.3	59.5
120.0 kc 2 1.0 kc - 18.3 3.0 kc 5 45eps - 13.6 Test chammed modula 120.0 kc 2 1.0 kc - 18.3 3.0 kc 5 45eps - 13.6	6 78 /or	2 11.10	796						
3.0 kc 5 45eps -13.6 Test channel modula 120.0 kc 2 1.0kc -18.3 3.0 kc 5 45cys -13.6	1.0kc -18.3	-31.8	1	13.5	(	10,87	1	20.8	
Test chaunel modula 120.0 kc 2 1.0kc -18.3 3.0 kc 5 45cys -13.6	45cps -13.6			22.5		-45.2	1	55.2	•
3.0 kc 5 45cys -13.6	model	tod:							
3.0 kc 5 45cps -13.6	<u> </u> 22	-31.8		13.5		-12.0	-	22.0	:
	45cys -13.6	-36.1		22.5	1	-38.0	1	48.0	1

Name; 4.1. 1.1. L. Date: 3-20-65

TABLE II-3.4-9 (CONT'D.) SIGNAL-TO-NOISE TEST DATA

Syste	System: Combinations	341	) ruc	ت ا	(S/N)c: 18.0	8.0	AGC: -40K	ンア	Output F1	3W Signal	Output FBW Signal: 13.C	₹pm*
	CHANNEL	EL		·		INPUT				OUT	OUTPUT	
<del>Paratan</del>	· · · · · · · · · · · · · · · · · · ·				%	Noise	/s)	(S/N) <sub>8</sub>	No	Noise	/S)	P(N/S)
ź	Frequency	DR	LPOF Frequency	Signa! dbm*	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex	Search Channel Only
	Test channel	amy	at	cent	1	frequency:	۲۶:					
9	56.0 kc	7	1.0 kc -	18.4	-36.3	-36.7	17.4	17.8	1:51-	-15.4	130	25.4
0	88.0 kc	3	1.0 kc -1		7.8 -35.0 -35.2		17.2	17.4	-15.7	-16.0	25.7	260
エ	120.0 kc	4	1.0 kg	-18.2	-35.2	-35.4	17.0	17.2	-13,7	-13.9	737	23.9
<u>6</u>	160.0 kc	4	1.3 kg	-18.8	-35.8	-360	17.0	17.2	-13.6	-/4.3	23.6	24.3
∞	3.0 kg	6	45cps	-13.5	-36.0	-55.4	12.5	41.9	-48,0	-49.9	58.0	59.9
·	Test channel at	٠ ۲		bandedge:	dge:							
Σ	56.3 kc	<b>(</b> ;	1.0 kc	-18.2 -35.2	-35.2		17.0		-14.3		24.3	
80	3.0 kc	5	45 cps	-13.5	-36.0		12,5		-460		560	
	Test channel	77	•	madulated.	ed:							
<u> </u>	56.0 kc	B	1.0 kc	-13.2	-35,2	1	17.0		15.4		25.4	1
<b>~</b>	3.0 kc	لم	45cps	-13.5	-36.0	1	12.5	1	-38.0		48.0	Ì
											1	

Syste	System: Symbinational	tion	12 N	s)	/Mc: 21.	900	(S/M) = 21.0db AGC: -4.0V		Output FBW Signal: /J, )	W Signal:	13.0	*mdb
	CHANNEL	EL	·			INPUT				OUTPUT	-UT	
					Noise	8.0	8(N/S)	5	Noise	981	(S/N) <sub>3</sub>	; 5
ř.	Frequency	DR	LPOF Frequency	Signal dbm*	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Soarch Channel Only db
	Test charmel	प्रकृत	herl at	Cent	t de	raguer cy:	cy:					
<i>v</i>	56.0kc	И	1.0kc	-18.8	-363	-39.0	19.5	20.2	-17.5	2:4-	27.5	27.50
0,	88.0 kc	u	1.360	8'Li-	-37.1	-37.5	19.3	147	-17.9	-18,5	27.9	25.52
14	120.0 hc	7	1.0kc	-18.2	-37.4	-37.8	19.2	17.6	-15,9	£'91-	25.9	26.3
61	160.0 kc	N	1.0 kc	-18.9	-374	-384	19.0	19.5	-15.8	-16.5	25.8	26.5
<b>b</b> 0	3.0 kc	Ŋ	45cps	-13.4	-36.0	-55.2	22.6	41.8	0.84-	- 50.0	58,0	60.0
	Test chammel at bandedge:	any	el at	band	salpe:							
*	120.0 kg 2		1.040	-18.2	-374		19.2		-16.6		26.6	
00	3.0 kc	4	45 475	-13.4	-36.0	1	22.6		0.94-	1	56.0	
	Test c	har	Test channel modulat	dulat	od;	,	·					
*/	120.0 kc	ī	1.0/10	-18.2	428-		19.2		-17.6		27.6	
00	3.0Kc	ہا	5.1054	-13.4	-36.0		22.6	1	-38.0		48.0	(1, <u>11, 1, 1</u>
. /												
		- حداظیہ سند								,		

< of 2

Name; 4:16/11. L Date: 3-26-65

Syste	System: Combinational	tion	Mal	(s)	/Mc: 24	(S/Mc: 240db AGC: -4.0V	AGC: -4	ĺ	Output FBW	W Signal:	Signal: 10.0	4mdb
,	CHANNEL	EL				INPUT				OUTPUT	uT	
				·	Notes	981	8(N/S)	Z) 8	Noise	96	P(N/S)	P (S
ż	Frequency	DR	LPOF Frequency	Signal dbm*	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Search Channel Only db	Full Multiplex dbm*	Search Channel Only dbm*	Full Multiplex db	Soarch Channel Only db
	test channel	ANN A	at	center	İ	frequency:						
9	56.0 kc	И	1.0 kc	8.81-	3.04-	-412.3	22.0	23,5	-26.5	-21.3	30.5	31.3
0	88.0 kc	п	1.0kc	8.61-	-36.8	-40.8	22.3	23.0	-21.0	-22.0	31.0	32.0
ĭ	120.0 kc	α	1.040	-18.2	-40.5	-41.3	22.0	23.1	-14.0	8.61-	24.0	29.8
6	160.0 kg	q	1.0 kc	18.80	-40.6	-43.0	21.8	23.3	18.9 - 19.7	-14.4	28.9	29.9
∞ .	3.0 kc	b	45-6/25	-13.3	-36.0	-54.5	22.7	41.2	-48.0	-50.0	58.0	60.09
	Test channe	LNN	l at	bandedge:	واطه:			,				
三	123.0 kg 2	n	1.0kc	-18.2	-40.2		22,0		-198		24,8	
<b>∞</b>	3.0 Kg 5	5	45cps	-13.3	-36.0		722		-46.0		56.0	
,	Test channel modulated:	MME	model	at ed:				•				
<u> </u>	120.0 kg	u	1.0kc	-18.2	- 40,2		22.0		-20.5		30.5	İ
c.	3.0kg	5	45cps	-13.3	ن ئۇن ·		7.22		-38.2		48.2	
			,									
Mantal Children							İ					And the second second

7 Jo /

Name: 458/12/2 Date: 3-2-65

#### 3.5 SYSTEM ERROR TEST

#### 3.5.1 General

The system error test uses a null technique to measure any variation between the system input and output. In essence, the input to the VCO of the particular channel under test is delayed and compared to the subcarrier discriminator output signal. The test is first performed by adjusting the system gain and delay (phase shift) for a null between the system input and output at a low modulating frequency. The frequency of the modulation is then increased and the null maintained by adjusting only the phase shift. The rms as well as the peak-to-peak magnitude of the null is then measured as total system error at several points within the data passband. The test is repeated and gain as well as phase shift is adjusted for a null at the same positions in the data passband. This latter measurement removes the effect of any system filter rolloff that occurs as the modulation frequency is increased.

The block diagram of the test is shown in Figure II-3.5-1. The phase and amplitude adjustment network would normally be placed in the comparison signal path; however, due to the difficulty of adjusting phase shift without attendant amplitude changes, it is necessary to use the configuration shown in Figure II-3.5-1. In this configuration, the all-pass phase network is driven from the low output impedance of the subcarrier discriminator and drives the high input impedance of the differential amplifier. The output-level control of the discriminator is used to adjust system gain. Thus, in this manner the system input signal is unaltered prior to the comparison with the system output.

In order to improve the signal-to-noise ratio through the differential amplifier, the amplifier is operated with a calibrated gain of 10. Since the amplifier output noise is independent of gain setting, this procedure improves the obtainable null voltage. The measured value of rms and peak-to-peak level are then divided by ten. In addition to the test with the full multiplex, the tests are repeated with only the channel under test in the multiplex. This technique isolates the effect of intermodulation on the system error.

### 3.5.2 Detailed Procedure

- a. Calibrate all VCOs.
- b. Deviate all VCOs full bandwidth at maximum rate for a deviation ratio of 5.
- c. Adjust the discriminator for approximately ±5 volts, i.e., 10 volts peak-to-peak with full bandwidth deviation.
- d. Establish IF signal-to-noise ratio greater than 20 db to assure that the receiver and discriminator are operating above threshold.

- e. Operate the AGC in its normal mode, but measure and note the level. This level can be used as a check on the actual input carrier level.
- f. Measure the residual system output rms and peak-to-peak noise voltage at the nulling point with the seach channel unmodulated. Repeat this measurement with only the search channel in the multiplex, i.e., with all other VCOs turned off. These readings of minimum attainable system noise serve as a lower limit on the null voltage possible.

(The following steps should be performed on the search-channel VCO with the complete multiplex operating and then repeated for the search channel only i.e., with all other VCOs turned off.)

- g. Set the level, R1, of the comparison modulating signal to the exactly 10 volts peak-to-peak. Adjust, R2, the input to the search-channel VCO for a full-bandwidth deviation.
- h. Establish a null by adjusting the phase shift and discriminator output control for a null at a sufficiently low modulating frequency to avoid all system rolloffs. The frequency used in the test is 0.3 f<sub>m5</sub>, where f<sub>m5</sub> is the maximum frequency for a deviation ratio of 5 operation of the search channel under test. Measure the peak-to-peak and rms null voltage at the output to the differential amplifier. If a gain of 10 in the differential amplifier is used, divide the output readings by 10.
- i. Change the modulating frequency to 0.5  $f_m$  where  $f_m$  is the maximum modulation frequency for the particular deviation ratio and channel under test. Obtain a null by operating only the phase adjustment.
  - j. Repeat step i. for a modulating frequency of 1.0 fm.
- k. Repeat steps i. and j. for null voltages where both the phase and amplitude adjustments are made to obtain a null. Record both the rms and peak-to-peak levels of the null voltage.

## 3.5.3 Results

Details of the tests and measured data are included in this volume in figures and tables numbered with II. Summarized test results are presented in Volume I in figures and tables numbered with I.

## 3.5.3.1 IRIG Baseband

For the IPIG 18-channel  $\pm 7.5\%$  system operating at a deviation ratio of 5, the system error was obtained for the following conditions:

Test channels: 70 kc ±7.5%; 3 kc ±7.5%

Multiplex level: 1.0 volt rms

IF S/N: 39 db

Deviation ratio: 5

LPOF: Constant amplitude, 18 db/octave, nominal sutoff frequency for DR = 5

The test data is shown in Table II-3.5-2 and summarized in Tables I-3.6-2 and I-3.6-3.

#### 3.5.3.2 IRIG Baseband--Wideband Channel

The IRIG baseband, channels I through 16 and E, was evaluated for system error under the following conditions:

Test channels: 70 kc  $\pm 15\%$ ; 3 kc  $\pm 7.5\%$ 

Multiplex level: 1.0 volt rms

IF S/N: 39 db

Deviation ratio: 5

LPOF: Constant amplitude, 18 db/octave, nominal cutoff frequency for DR = 5

The test data is shown in Table II-3.5-3 and summarized in Tables I-3.6-4 and I-3.6-5.

#### 3.5.3.3 IRIG Baseband--Deviation Ratios 1 and 2

The IRIG baseband, channels 1 through 18 operating at a deviation ratio of 1 and 2, was evaluated for system error under the following conditions:

Test channels: 70.0 kc  $\pm$ 7.5%; 22.0 kc  $\pm$ 7.5%; 7.35 kc  $\pm$ 7.5%; 3.0 kc  $\pm$ 7.5%; 960 cps  $\pm$ 7.5%

Multiplex level: 1.0 volt rms

IF S/N: 39 db

Deviation ratio: 1 or 2

LPOF: Constant amplitude, 18 db/octave, nominal cutoff frequency for DR = 1 or 2

The test data shown in Table II-3.5-4 and summarized in Tables I-3.6-2 and I-3.6-3. The low deviation ratios increased the system output noise sufficiently to require the null to be obtained first with only the search channel VCO in the multiplex. The corresponding full multiplex reading was then made at the same amplitude and phase settings after turning on the remaining VCOs. The voltage level at null was often such that a gain of 10 in the differential amplifier was not used.

## 3.5.3.4 Expanded Baseband

The expanded baseband, channels I through 21, was evaluated for system error under the following conditions:

Test channels:  $165 \text{ kc} \pm 7.5\%$ ;  $125 \text{ kc} \pm 7.5\%$ ;  $93 \text{ kc} \pm 7.5\%$ ;

70 kc  $\pm$ 7.5%; 3 kc  $\pm$ 7.5%

Multiplex level: 750 mv rms

IF S/N: 39 db

Deviation ratio: 5

LPOF: Constant amplitude, 18 db/octave, nominal cutoff frequency for DR = 5

The test data is shown in Table II-3.5-5 and summarized in Tables I-3.6-4 and I-3.6-5.

## 3.5.3.5 Expanded Baseband--Wideband Channel

The expanded baseband, channels I through 19 and H, was evaluated for system error under the following conditions:

Test channels:  $165 \text{ kc} \pm 15\%$ ; 93 kc  $\pm 7.5\%$ ; 70 kc  $\pm 7.5\%$ ;

 $3 \text{ kc} \pm 7.5\%$ 

Multiplex level: 630 mv rms

IF S/N: 39 db

Deviation ratio: 5

LPOF: Constant amplitude, 18 db/octave, nominal cutoff frequency for DR = 5

The test data is shown in Table II-3. 5-6 and summarized in Tables I-3. 6-4 and I-3. 6-5.

## 3.5.3.6 Constant-Bandwidth Baseband

The constant-bandwidth multiplex, channels I through 21, was evaluated for system error under the following conditions:

Test channels:  $56 \text{ k}^{\frac{1}{6}} \pm 2 \text{ kc}$ ;  $88 \text{ kc} \pm 2 \text{ kc}$ ;  $120 \text{ kc} \pm 2 \text{ kc}$ ;  $160 \text{ kc} \pm 2 \text{ kc}$ 

Multiplex level: 360 mv rms

IF S/N: 39 db

Deviation ratio: 2

LPOF: Constant amplitude, 42 db/octave, nominal cutoff frequency for DR = 2

The test data is shown in Table II-3.5-7 and summarized in Tables I-3.6-6 and I-3.6-7.

## 3.5.3.7 Combinational-Bandwidth Baseband

The combinational-bandwidth multiplex, IRIG channels I through II and constant-bandwidth channels I through 21, was evaluated for system error under the following conditions:

Test channels: 3.0 kc  $\pm 7.5\%$ ; 56 kc  $\pm 2$  kc; 88 kc  $\pm 2$  kc; 120 kc  $\pm 2$  kc; 160 kc  $\pm 2$  kc

Multiplex level: 635 mv rms; 600 mv rms for CBW channels and 210 mv rms for IRIG channels

IF S/N: 39 db

Deviation ratio: 2 for CBW channels, 5 for IRIG channels

LPOF: Constant amplitude, 42 db/octave in the CBW channels and 18 db/octave in the IRIG channels, nominal cutoff frequency for specific deviation ratio.

The test data is shown in Table II-3.5-8 and summarized in Tables I-3.6-8 and I-3.6-9.

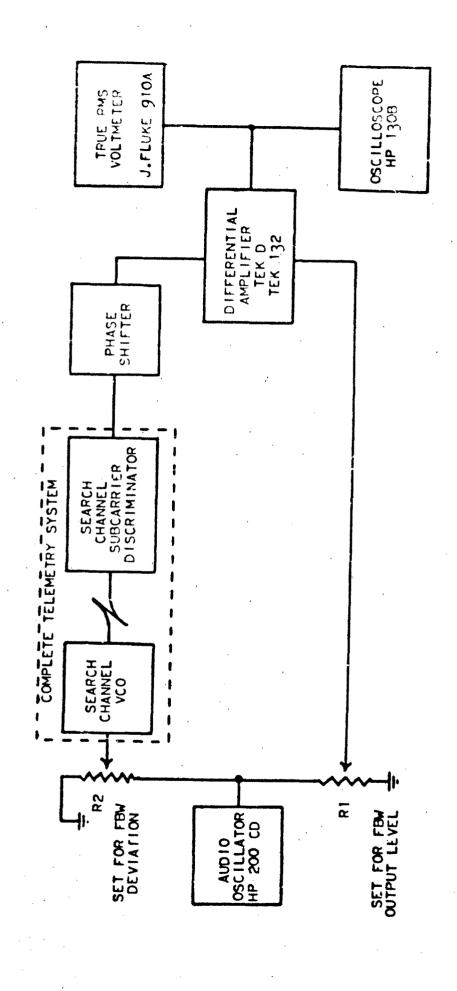


FIGURE II-3, 5-1 SYSTEM ERROR TEST BLOCK DIAGRAM

## TABLE II-3. 5-2 SYSTEM ERROR TEST DATA

System Description: IRIG Mulkiple	· Ch	annel	17	breuz	418,	DRSS
IF Signal-to-Noise Ratio: 39db						·
Discriminator Full Scale Output: 100	PP F	leceive <b>r</b>	AGC V	oltage:	5.20	dc_
Discriminator Channel: 70.0 KC ±			=5-		•	4
Residual Noise: Full Multiplex 8.4		Sear	ch Chai	nnel On	ly 2.9	ומצאפון
Full Scale Level at Summing Point:	3.6V	CMS	and _	10.5	1 VPP	
	3/5	توع	5-3	25.09	105	De15,
	0.	m	0.	m		m
Pull Mulaimlane	rms	mv p-p	rms	mv p-b	mv rms	mv p-u
Full Multiplex:	11119		23	140	242	750
Phase Null Only	20	120	23	140	18	100
Phase & Amplitude Null	1	120	-	770	10	1
Search Channel Only:			21	an	2.12	min
Phase Null Only	-		<del>                                     </del>	90	242	700
Phase & Amplitude Null	12	90	2/_	90	15.8	170
Discriminator Channel: 3.0 KC ±7.	5%	DR=4				
Residual Noise: Full Multiplex 60		Searc	h Chan	nel Onl	2.8	MYMS
Full Scale Level at Summing Point:			and _	10.8	•	nagagaid d'Albanda, sagandar più - 1 de
	1 /3	Eps.	72	cps	143	203
				_m		
Full Multiplex:	mv rms	mv p-p	rms	mv D-D	rms	mv p-p
•			17	60	190	580
Phase Null Only	11	10	16	60	10	40
Phase & Amplitude Null	16	60	10	-	,,,	10
Search Channel Only:				100	105	اءسما
Phase Null Only			15	30	190	280
Phase & Amplitude Null	14	50	14.3	30	17.3	170

Date 1-11-65 Name WS8 MDL

# TABLE II-3, 5-3 SYSTEM ERROR TEST DATA

System Description: IZIG Multiplex	Che	nnels	1 160	ough.	16 Ans	IE
IF Sign. 1-to-Noise Ratio: 39db						
Discriminator Full Scale Output: 10 V	<b>P</b>	Receiver	AGC V	oltage:	-5.2	Vdc
Discriminator Channel: E. 70kc1/5		_				
Residual Noise: Full Multiplex 7.			ch Cha	nnel On	ly 2.4	mu
Full Scale Level at Summing Point:	3,50	Yms_	and _	10.	2VPP	
	0.		0.		,	0 f
	mv	my	mv	mv.	mv	mic
Full Multiplex:	rms	p-p	rms	p-p	rms	<u> </u>
Phase Null Only			41	150	114	380
Phase & Amplitude Null	29	125	41	150	33	140
Search Channel Only:						
Phase Null Only			40	130	114	360
Phase & Amplitude Null	28	100	40	130	32	120
Discriminator Channel: 8, 3kc17.59	DR:	<u>. ح</u>				
Residual Noise: Full Multiplex 5	•		h Chan	nel Onl	4111	xms.
Full Scale Level at Summing Point:	3.5	Vrms	and _	10 4	100	-
	0.3	l f	0.	5 f	1.	01.
	mv	mv	mv	mv	miv	
Full Multiplex:	rms	p-p	rms	D-D	rros	
Phase Null Only			1603	70	116	360
Phase & Amplitude Null	14.5	70	13:3	60	8.5	40
Search Channel Only:				,	1,,,	
Phase Null Only			16	60	116	360
Phase & Amplitude Null	/3	60	15	60	7.5	30

Date 1-13-65 Name 58C/MPL

# TABLE II-3.5-4 SYSTEM ERROR TEST DATA

System Description: IPIC MULIN	YEX, CA	MAN SEZ	5 17	HROW	11 18,	DR:12	J
IF Signal-to-Noise Ratio: 39db					_		
Discriminator Full Scale Output: 101	JPO R	ecciver	AGC V	'cltage:	-5.2	Udc	
Discriminator Channel: 70.0KC +7.		) R=1				•	
Residual Noise: Full Multiplex	35 my	Sear	ch Cha	nnel On	11y 7.4	MUENS	,
Full Scale Level at Summing Point:	3.6 VY	m S	and _	10.4	VPP		
	3/5	eps im	262	Sim	525	0 1 0	
	nıv	mv	mv	mv	mv	mv	
Full Multiplex:	rms	p-p	rms	p-b	rms	D-D	
Phase Null Only			490	2500	118	1200	
Phase & Amplitude Null	122	1200	130	1000	118	900	
Search Channel Only:							
Phase Null Only			480	1600	18.0	120	
Phase & Amplitude Null	15.2	120	76	350	18.2	140	
Discriminator Channel: 70.0KC ± 7.	5% D	R=2					
Residual Noise: Full Multiplex 3	וחדיוות	Search	h Chani	nel Only	4.57	Mucms	
Full Scale Level at Summing Point:	3.6 V	<u>`m3</u>	and _	10.4	وول	,	
	3/50	ps m	13/3	c ps	262	5 603	
Full Multiplex:	mv	mv	mv	mv	mv	my	
·	rma	D-D	CAL CAL	5-0	ICA	D-D	
Phase Null Only	1/2		77	300	190	1000	
Phase & Amplitude Null	43	400	53	450	77	450	
Search Channel Only:							
Phase Null Only			85	321	186	600	
Phase & Amplitude Null	13.5	80	37	180	25	120	

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Date 1-11-105 Name W. Bishop

System Description: IPIG Waltigle	Char	nels	the	4418	DR:	142
IF Signal-to-Noise Ratio: 39db						
Discriminator Full Scale Output: 100	IPP F	Receiver	AGC V	'oltage:	-5.2	ude
Discriminator Channel: 7,35 KC 1						
Residual Noise: Full Multiplex 5/	•		— ch Cha	nnel On	ly 6. a	Murn
Full Scale Level at Summing Point:				10.4		,
		3cp3		5 in	7	/cps
	mv	mv .	mv	mv	mv	mv
Full Multiplex:	rms	p-p	rms	P-D	rms	P-0
Phase Null Only	PT 1	4.50	5/0	2000	/85	1000
Phase & Amplitude Null	7/	500	165	1000	100	600
Search Channel Only:						
Phase Null Only			500	1600	175	580
Phase & Amplitude Null	16.5	90	1144	650	45	200
Discriminator Channel: <u>7.35 たと ±7</u> .	5%.I	R=2				
Residual Noise: Full Multiplex 26	,		h Chani	nel Only	5.5	mur.
Full Scale Level at Summing Point:		rm3	and	10.4	1/00	
	33 0.3	Cps m	138	<b>CP3</b>	276	<u>کم ک</u>
	mý	mν	mv	mv	mv	mv
Full Multiplex:	Ims	D-D	rms	D-0	rms	1 -D
Phase Null Only			1/35	700	162	700
Phase & Amplitude Null	34	300	70	400	60	350
Search Channel Only:				į		İ
Phase Null Only			130	500	154	500
Phase & Amplitude Null	17	90	57	200	51	200
		•				

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Date 1-11-65 Name W. Bishop

System Description: ILIG Multiples	Chan	wels 1	Heren	AR.	DR:	42			
IF Signal-to-Noise Ratio: 39db						· · · · · · · · · · · · · · · · · · ·			
Discriminator Full Scale Output: 10Upp Receiver AGC Voltage: -5.2Udc									
Discriminator Channel: 22.0 KC ± 7.5% DR=1									
Residual Noise: Full Multiplex 55 ml/m Search Channel Only 4.5 ml/m									
Full Scale Level at Summing Point: 3.60Vrms and 10.40pp									
100 cps 825 cps 1650 cps									
	0.	3 f m	0.	5 t <sub>m</sub>	١.	0 f			
	mv	mv	mv	mv	mv	mv			
Full Multiplex:	rms	p-p	480	D-D	rms	D-D			
Phase Null Only		<u> </u>	1	1700	132	600			
Phase & Amplitude Null	67	500	136	600	85	400			
Search Channel Only:				<b>i</b> .					
Phase Null Only			475	1500	98	300			
Phase & Amplitude Null	15	60	121	450	45	150			
Discriminator Channel: 22.0KC ± 7.	5-90	DR=2							
Residual Noise: Full Multiplex 257	•		h Chan	nel Only	2.8m	Usems			
Full Scale Level at Summing Point:		• '		10.4	,				
	0.3	o eps	6.	acps	1.82	5cp3			
•	mv	mv	mv	mv	niv	my			
Full Multiplex:	rms	D-D	rms	מ-מ	rms	ט-ט			
Phase Null Only			143	500	200	700			
Phase & Amplitude Null	32	150	70	300	50	250			
Search Channel Only:			1000	1-26	200				
Phase Null Only			140	500	200	600			
Phase & Amplitude Null	15	60	58	200	41	150			

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Date 1-8-64 Name M. Longman

System Description: IPIG Multiple	1. Ch.	unels	174	rough	IN DA	2:14
IF Signal-to-Noise Ratio: 39db						
Discriminator Full Scale Output: 100	P	leceiver	AGC V	oltage:	-5.24	dc_
Discriminator Channel: 3.0 XC 17.5	%. D	P=/				
Residual Noise. Full Multiplex 83			- ch Cha	nnel Ön	ly <b>5.5</b>	MUTH
Full Scale Level at Summing Point:				10.8		
<del>-</del>		c,e m	0.	3cps 1m	22	Seps 0 m
	mv	ימו	my	mv	mv.	mv
Full Multiplex:	rms	p-p	rms	p-b	rms	p-p
Phase Null Only	1516		430	2000	410	1500
Phase & Amplitude Null	180	1500	160	800	145	600
Search Channel Only:		Carried State State State State State State State State State State State State State State State State St			_	
Phase Mull Only			410	1500	380	1200
Phase & Amplitude Null	18.5	80	70	300	25	100
Discriminator Channel: 30kc±75	%. D	R=2	_			
Residual Noise: Full Multiplex 257	,		h Chan	nel Only	4.40	Urms
Full Scale Level at Summing Point:	3.7Ux	m 7	and	10.8U	912	
		c PI		c ps		0 t
Tall Malain	mv	mv	mv	mv	mv	rnv
Full Multiplex:	rms	n-n	tms	D-D	///D	D-D
Phase Null Only	42		126	400	178	600
Phase & Amplitude Null	73	300	50	200	42	250
Search Channel Only:			,			
Phase Null Only			120	360	14/3	480
Phase & Amplitude Nul	13	60	32	130	17.5	75

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Date 1-11-65" Name E80/MDL

System Description: IRIC Multiple	1, C	SHEET	SIA	مودوم	JP P	<i>P=1</i> +2			
IF Signal-to-Noise Ratio: 39db									
Discriminator Full Scale Output: 100	00 F	Receiver	AGC V	oltage:	-5:21	1de			
Discriminator Channel: 960 cps t7	5%	DR=							
Residual Noise: Full Multiplex 67	, ,			nnel On	ly 8.5	MUm			
Full Scale Level at Summing Point:	3.6 V	YM3	and	10.4	1000				
5eps 36eps 72eps									
	mv	mv	mv	mv	mv	mv			
Full Multiplex:	rms	p-p	rms	p-p	rms	0-0			
Phase Null Only			410	2000	350	1600			
Phase & Amplitude Null	140	1600	130	1200	120	1000			
Search Channel Only:									
Phase Null Only			400	1320	335	1000			
Phase & Amplitude Null	16	80	48	200	23	140			
Discriminator Channel: 960 cps ±23	-06	DR=2							
Residual Noise: Full Multiplex 21 x	1Uxm2	Search	h Chani	nel Only	6.2 m	2Vxm3			
Full Scale Level at Summing Point:	56V	cm3	and _	10.4	100				
	0.3	f m	0.	<b>ep3</b> 5 f	3.	0 m			
Toll Modernian	mv	mv	mv	mv	mv	mv			
Full Multiplex:	Ims	D-D	ine	0-D	ITA	0-0			
Phase Null Only	77	400	125	300	/35	600			
Phase & Amplitude Null	33	700	37	350	37	300			
Search Channel Only:	_		120	, la A	10.0				
Phase Null Only	100	0.0	120	400	125	450			
Phase & Amplitude Null	17	70	20	100	17	80			

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Date 1-11-64 Name W. Bishop

## TABLE II-3. 5-5 SYSTEM ERROR TEST DATA

System Description: Expanded Mo	Hicks	Chan	nels	1 14	0094 2	2/
IF Signal-to-Noise Ratio: 39db					, 	
Discriminator Full Scale Output: 10	PP F	Receiver	AGC V	oltage:	-5.11	ide
Discriminator Channel: 165 KC 1	7.5%.	DR-3				
Residual Noise: Full Multiplex 8,	_			nnel On	ly 5.4	mum
Full Scale Level at Summing Point:				3.51		
742cps 1238cps 2475						
	· · ·	<mark>'¹</mark> m		m L		0 I <sub>m</sub>
Full Multiplex:	mv rms	mv p-p	rms	mv p-b	mv rins	mv p-p
Phase Null Only			165	140	165	530
Phase & Amplitude Null	13	100	15.5	110	15-	110
Search Channel Only:						
Phase Null Only			15	90	164	520
Phase & Amplitude Null	10.5	70	14	80	13	80
Discriminator Channel: 124 KcT	75%	DR=	<u> </u>			
Residual Noise: Full Multiplex 16	_ ′			nel Only	50m	Wrm3
Full Scale Level at Summing Point:	100	00	and _	3.5°U	YM S	
	<b>5.3</b>	fm	93	eps m	186	0 c p 3
Endl Madainless	mv	mv	mv	mv	mv	mý
Full Multiplex:	rms	D-D	Ims	D-D	rms	D-D
Phase Null Only	10/		29	160	8/	350
Phase & Amplitude Null	18	120	21	140	16.5	120
Search Channel Only:			;			
Phase Null Only			27	140	80	275
Phase & Amplitude Null	15-	80	18	100	13	80
			1			

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System Description: Expended Mu	tiple	s, Ch	ARRE	51	Parceya	21
IF Signal-to-Noise Ratio: 39db					·	
Discriminator Full Scale Output: 100	PP_F	Receiv <b>er</b>	AGC V	oltage:	-5./0	1dc
Discriminator Channel: 93KC ±7.5	% I	DR-5			·	
Residual Noise: Full Multiplex 6.2	MUYH	ns Scar	ch Cha	nnel Or	ity <u>4.0</u>	<i>THYMS</i>
Full Scale Level at Summing Point:	100p	ρ	and _	3.50	rms	
	426	c.p.s	700 cps		140	Ocps
·	mv	m mv	mv	my	mv	my
Full Multiplex:	rms	p-p	rms	p-p	rins	р-р
Phase Null Only	_		29	160	83	300
Phase & Amplitude Null	14.4	100	19	100	16	100
Search Channel Only:						
Phase Null Only			28	120	83	275-
Phase & Amplitude Null	12-2	70	17	80	13.2	70
Discriminator Channel: 70 KC ±7.5	-0/0 >	DR= 5	5			
Residual Noise: Full Multiplex 12		Searc	h Chan	rel Only	15,2m	1Urms
Full Scale Level at Summing Point:	DUP	0	and	3.5°L	18-15	
	3/5 0.3	im_	<b>37.</b>	Seps m	1.0 na	
Full Multiplex:	mv rms	mv g-g	mv	mv n-n	mv rms	mv p-p
Phase Null Only			24	160	82	350
Phase & Amplitude Null	16	140	15-	120	14	100
Search Channel Only:						
Phase Null Only			22	100	80	275
Phase & Amplitude Null	11	80	11	60	9	60
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System Description: Expanded Mul	Pelen	Chis	nels	1 Th.	rough	2/_
IF Signal-to-Noise Ratio: 39 db						
Discriminator Full Scale Output: 100	P P	Receiver	AGC V	oltage:	-5.10	de
Discriminator Channel: 3.0 KC ±7.5	, ,					
Residual Noise: Full-Multiplex 5.5	. /			nnel Or	ly <b>3.0</b> )	Myrms
Full Scale Level at Summing Point:			and 、			
	, ,	<b>CP3</b>		cps	1/57	0 f
	mv	niv	mv	mv	mv	mv
Full Multiplex:	rms	p-p	rms	p-p	rms	D-D
Phase Null Only		70	10	80	100	325
Phase & Amplitude Null	15	70	12.5	70	9	50
Search Channel Only:						
Phase Null Only			14	70	100	325
Phase & Amplitude Null	9.5	60	11	60	7	40
Discriminator Channel:			·			
Residual Noise: Full Multiplex		Searc	h Chanr	iel Onl	·	
Full Scale Level at Summing Point:			and			
	0.3	f m	0.5	5 f m	ì.	0 t
Full Mulainton	mv	mv	mv	mv	mv	my
Full Multiplex:	rms	D-D	rms	p-p	rnis	p-p
Phase Null Only						
Phase & Amplitude Null					· · · · · · · · · · · · · · · · · · ·	
Search Channel Only:						
Phase Null Only						
Phase & Amplitude Null			<u> </u>			<u> </u>

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# TABLE II-3. 5-6 SYSTEM ERROR TEST DATA

System Description: Expended Me	Miplex	Chy	egels	1 Horn	mb 19	and t
IF Signal-to-Noise Ratio: 39db						
Discriminator Full Scale Output: 10	Vpp F	Receiver	AGC V	oltage:	-5:/	UJC
Discriminator Channel: 165 KC ±1	5-0%	DR=	5-			
Residual Noise: Full Multiplex 8	5mu-	ns Sear	ch Cha	nnel Or	aly_ <b>7.</b> \$	Myrm
Full Scale Level at Summing Point:					Urm	
	148	Sups	247	Sept		Deps,
•	(1,,	m	0.	m m		. U fm
Full Multiplex:	rms	mv p-p	rms	mv p-p	rins	p-p
Phase Null Only			2).5	140	150	500
Phase & Amplitude Null	17.5	120	20	120	14	100
Search Channel Only:						
Pháse Null Only			20	120	150	300
Phase & Amplitude Null	17	120	18.5	110	13	90
Discriminator Channel: 93KC±7.	5% I	)R=5	•			
Residual Noise: Full Multiplex 9.0	MUYMS	Searc	h Chan	nel Onl	7.5 m	lym s
Full Scale Level at Summing Point:				3337		
	42e		700	) <b>ep</b> 2	14	oocps
		m		m		m
Full Multiplex:	mv rms	mv. .p.p	rms	mv n-n	mv rms	mv p-p
Phase Null Only			32	180	92	350
Phase & Amplitude Null	17	120	22	120	18	120
Search Channel Only:						
Phase Null Only			31	140	92	300
Phase & Amplitude Null	15	100	20	100	16	100
	•					

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# TABLE II-3. 5-6 (CONT'D.) SYSTEM EFROR TISI DATA

System Description Expeded Multip	Ves .	CHIANE	15 14	rough	19 1	41
IF Signal-to-Noise Ratio: 39db		والمتعددة والمتعدد والمتعد			r dog gerind differentiation of most training to confidence	analysistem only -100
Discriminator Full Scale Output: 100	<b>22</b> _F	eccive <b>r</b>	AGC V	oltage:	-5.10	1dc
Discriminator Channel: 70 KC 17.						,
Residual Noise: Full Multiplex 7.5	Smur	Sear	ch Cha	nuel-On	1 6.5	nu
Full Scale Level at Summing Point:		_			-Urm	
	3/5	ces m		seps		0 c p \$
	nev	mv	mv	1771	mis	m
Full Multiplex:	rms	p-p	107	p-b	213	701
Phase Null Only			107	400	212	70
Phase & Amplitude Null	13	100	15	110	12.4	96
Search Channel Only:						١.
Phase Null Only			105	350	212	65
Phase & Amplitude Null	10	70	12.5	80	9.5	60
Discriminator Channel: 30KC ± 7.	50/0	DR=	<u>ر ح</u>			
Residual Noise: Full Multiplex <u>5.0</u>	,			nel Only	3.0m	747
Full Scale Level at Summing Point:	1000		and _	<u>3,55</u>	Urms	,
	0.	Sep3	<b>22.</b> 5	cps 5 i	4/5	-EP3
Full Multiplex:	mv	mv	mv	mv	mv	7713
•	rms	D-D	20	100	94-	ا روز
Phase Null Only	12	80		100	10	221
Phase & Amplitude Null	/3	80	15	90	10	00
Search Channel Only:	1_					
Phase Null Only			19	90	95	301
Phase & Amplitude Null	15	50	114	70	9	50

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# TABLE II-3. 5-7 SYSTEM ERROR TEST DATA

System Description: Constant	Bo	indu	ideh	Noli	tiples	
IF Signal-to-Noise Ratio: 39 db						
Discriminator Full Scale Output: 10 41	!	Receiver	AGC V	oltage:	-5.0	ode
Discriminator Channel: 14, 120KC				,		
Residual Noise: Full Multiplex 31	,			nnel On	Ly 26,	21 V 2000
Full Scale Level at Summing Point:	10 up	ρ	and	3.54	Jurns	1
	300		500			) /c 0 (
	mv	mv	mv	mv	mv	mv
Full Multiplex:	rms	D-D	rms	p-b	rms	D-D
Phase Null Only			175	740	238	850
Phase & Amplitude Null	57	350	158	750	35	250
Search Channel Only:						
Phase Null Only			175	740	235	800
Phase & Amplitude Null	54	320	158	700	31	215
Discriminator Channel: 19,160 Kg	c + 2 /	KC. DA	6.2			
Residual Noise: Full Multiplex 30	nvrms	Searc	h Chan	nel Only	25m	Vens
Full Scale Level at Summing Point:	_		and _	3.54	lyms	
•	0.3	3 f m	0.5	o f m	1.	0 f <sub>m</sub>
	mv	mv	mv	mv	mv ·	mv
Full Multiplex:	rms	D-D	rms	D-D	rms	p-p
Phase Null Only			203	800	194	700
Phase & Amplitude Null	63	3400	180	800	34	250
Search Channel Only:		÷		,		
Phase Null Only			202	00 <i>8</i>	194	700
Phase & Amplitude Null	60	380	179	800	30	200

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# TABLE II-3. 5-7 (CONT'D.) SYSTEM ERROR TEST DATA

System Description: Constant	Ban	dwidz	ch !	Multi	plex	manada a sa sa sa sa sa sa sa sa sa sa sa sa
IF Signal-to-Noise Ratio: 39 db				iannatuuraan maatiin on aan aan		disconnection de
Discriminator Full Scale Output: 1001	<u>و و</u>	Recuver	AGC V	oltage:	-5.0	ide
Discriminator Channel: 6.56 KC				, alternative and the second and the		
Residual Noise: Full Multiplex 3/				ngel On	lv 25.	5mh
Full Scale Level at Summing Point:	1048	Ρ	and 💆	3.54	Urm:	
	<b>300</b>	} <b>* P\$</b> } f	<b>50</b>	0 eps . 5 1	1	0 f
	mv	mv	mv	my	mv	m۷
Full Multiplex:	rms	p-p	rms	D-D	rins	D-D
Phase Null Only			145	740	245	1000
Phase & Amplitude Null	55	450	128	700	48	400
Search Channel Only:	1					
Phase Null Only			134	600	244	850
Phase & Amplitude Null	42	300	120	540	30	220
Discriminator Channel: 10.88 KG	: +2K	C, DI	R-2			
Residual Noise: Full Multiplex 32				nel Only	25m	lxmx
Full Scale Level at Summing Point:	DUPP		and	3.54	Urms	
· .	<b>300</b>	of Tr	<b>5</b> 00	leps 5 i m	1.0 1.	KC 0 t
P 11 34 14: 1	mv	mv	mv	mv	mv	my
Full Multiplex:	rms	D-D	rms	P-D	rms	.D-D
Phase Null Only	1415		150	750	192	700
Phase & Amplitude Null	45	300	114	300	37	280
Search Channel Only:	1					
Phase Null Only			146	680	190	700
Phase & Amplitude Null	39	250	110	450	27	200

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# TABLE II-3, 5-8 SYSTEM ERROR TEST DATA

System Description: Cambina	tiona	1 1	maria	14 A	loffip	KE A
IF Signal-to-Noise Ratio 39 db						
Discriminator Full Scale Output: 10	uPP_F	Receiver	AGC V	oltage:	-5.2	ude
Discriminator Channel: 6 CBW					,	
Residual Noise: Full Multiplex 4					ly /5"	Albana
Full Scale Level at Summing Point				3.54		
*	300	LP3	500		. 1.0	O I
	my	mv	mv	mv	mv	mv
Full Multiplex:	rms	p-p	rms	D-D	rms	D-D
Phase Null Only			170	300	270	1100
Phase & Amplitude Null	125	650	135	760	55	300
Search Channel Only:						
Phase Null Only			135	550	240	800
Phase & Amplitud Null	110	450	110	460	25	140
Discriminator Channel: 10 CBW	88 KC	±240	, DR	: 2		
Residual Noise: Full Multiplex					15 m	zmi.
Full Scale Level at Summing Point				3.54		
	3006	f m	0.	eps 5 f m		0 f
Full Multiplex:	rav	mv	mv	my	mv	mv
•	rms	D-23	Ims	D-D	tms	D-D
Phase Null Only			150	800	200	850
Phase & Amplitude Null	85	400	115	300	42	200
Search Channel Only:		i :				
Phase Null Only			140	600	180	600
Phase & Amplitude Null	74	300	110	350	20	100

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# TABLE II-3. 5-8 (CONT\*D.) SYSTEM ERROR TEST DATA

System Description: Combine	•	Pana	est d/h	אטוא	Ziy/e	unimidalisma
IF Signal-to-Noise Ratio: 39db			A C * C * 1 *			. 1 . 1 .
Discriminator Full Scale Output:						NAC.
Discriminator Channel: 14 CB			•			-
Residual Noise: Full Multiplex_	40 murm	Sear	tch Cha	nnc1 Or	LOM	<u>Vrmi</u>
Full Scale Level at Summing Po	int: 100 pp	- 	_ and 🚨	3.54	Urms	
	300		576	<b>ept</b> 5 3	1.0	6 0 f m
	ms	mv	my	ms	mix	mv
Full Multiplex:	rins	p-p	rms	D-D	rins	D-1
Phase Null Only			190	800	265	1000
Phase & Amplitude Null	148	650	160	700	44	257
Search Channel Only:						
Phase Null Only			190	700	270	950
Phase & Amplitude Null	142	550	155	550	25-	100
Discriminator Channel: 19 CBW	,160KC	take	· DA	2=2		-
Residual Noise: Full Multiplex_	45 MV cmi	Searc	h Chan	nel Onl	15.5	22 km s
Full Scale Level at Summing Pos	int: 1008			3541		
	, 3000	.ps	500	· pr	1.	OAC
	0.3	m	-	m	1.	0 1
Full Multiplex:	rms	mv p-p	rms	mv p-p	rms	D-D
Phase Null Only			220	900	240	950
Phase & Amplitude Null	140	700	190	800	57	300
Search Channel Only:						
Phase Null Only			198	700	205	700
•		600	190	700	27	100

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# TABLE II-3, 5-8 (CONT'D.) SYSTEM ERROR TEST DATA

Discriminator Full Scale Output:	10UPP F	Receives	r AGC V	oltage	-5.2	Vdc
Discriminator Channel: 8 PBU			_			
Residual Noise: Full Multiplex			•		nly 3 »	1 V x m s
Full Scale Level at Summing Po			_ and _			
	0.	i m	23.	<b>5 i</b> m	45	. 0 f
E.A. Mulainland	mv	mv	mv	mv	mv	mv
Full Multiplex:  Phase Null Only	rms	P-D	17.5°	80	145	450
	14- 4-	60	17.5	80		
Phase & Amplitude Null	13.5	60	17.5	00	12	50
Search Channel Only:			17.5	on	142	Man
Phase Null Only	15	1-0	17.5	70	142	400
Phase & Amplitude Null			17.5			100
iscriminator Channel:					-	
Residual Noise: Full Multiplex_		Searc	h Chan:	iel Onl	У	··· <del>··································</del>
Full Scale Level at Summing Poi	nt:		_ and _			
•	0.3	f m	0.5	o f m	1.	0 f
<b></b>	mv	mv	mv	mv	mv	ทาง
Full Multiplex:	rms	D-D	rms	D-0	rms	p-p
Phase Null Only					ļ	
Phase & Amplitude Null						<u> </u>
Search Channel Only:						
Phase Null Only						
Phase & Amplitude Null						

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### 3.6 TAPE-RECORDER ERRORS

### 3.6.1 General

The tape-recorder error test was made to determine the effect of post-detection recording on the system performance. The test was accomplished using the system block diagrams shown in Figure II-3.0-1 for the proportional basebands, and Figures II-3.0-2 and II-3.0-3 for the constant- and combinational-bandwidth basebands. In all cases the mixer amplifier de-emphasizes the receiver output and adds the reference tone to the total multiplex. The de-emphasis network was a simple RC network in the input of the mixer amplifier driven by the receiver output. In all cases the level of the reference oscillator signal is twice the level of the highest frequency channel in the multiplex.

To determine the effect of the addition of the tape recorder, the system was first operated with the tape recorder bypassed, i.e., the mixer output feeding directly into the remainder of the ground system. The discriminator cutput noise is measured and then the tape recorder was included in the system and the test repeated. Measurements were made with and without tape-speed compensation for the test channel unmodulated at center frequency and at bandedge.

In addition to the test for increase in channel output noise due to the inclusion of the tape recorder, the intermodulation test (Section 3.3) was repeated on the constant- and combinational-bandwidth multiplexes with the tape recorder included in the system.

# 3.6.2 Detailed Procedure for Tape-Recorder Error Test

- a. Calibrate all VCOs.
- b. Deviate all channels, with the exception of the test channel, full bandwidth at the maximum modulation frequency for the particular deviation ratio.
  - c. Allow the receiver AGC to assume normal operating condition.
  - d. The IF carrier-to-noise ratio should be greater than 20 db.
  - e. Set subcarrier discriminator output for 10 volts, peak-to-peak.
- f. Adjust the reference oscillator output for a level equal to twice the level of the highest channel in the multiplex.
  - g. Adjust the tape-recorder input and output for normal record level.
- h. Measure the rms discriminator output noise at center frequency and low bandedge with and without the tape recorder bypassed and also with and without tape-speed compensation.

## 3.6.3 Results of Tape Recorder Error Test

Measured data and experimental conditions described in illustrations numbered with II are included in this volume. Summarized data and conclusions are presented in Volume I in illustrations numbered with I.

### 3, 6, 3, 1 IRIG Baseband

The IRIG baseband channels 1 through 18 were evaluated for tape-recorder error. The detailed conditions were:

Test channels:  $70.0 \text{ kc} \pm 7.5\%$ ;  $3.0 \text{ kc} \pm 7.5\%$ 

Deviation ratio: 5

De-emphasis corner frequency: 4 kc

Discriminator full-bandwidth output: 10 volts peak-to-peak

Tape recorder: Mincom G107

Tape speed: 60 ips

Record level: 1.0v rms

IF S/N ratio: 39 db

Table II-3.6-1 shows the measured data for the IRIG baseband evaluation. A summary of the data is shown in Table I-3.7-1.

### 3.6.3.2 IRIG Baseband--Wideband Channel

The IRIG baseband containing a wideband channel in the highest frequency position was evaluated for tape-recorder error. The detailed conditions were:

Test channels:  $70 \text{ kc} \pm 7.5\%$ ;  $3 \text{ kc} \pm 7.5\%$ 

Deviation ratio: 5

De-emphasis corner frequency: 4 kc

Discriminator full-bandwidth output: 0 volts peak-to-peak

Tape recorder: Mincom G107

Tape speed: 60 ips

Record level: 1.0v rm.

IF S/N ratio: 39 db

Table II-3.6-2 shows the measured data for the wideband IRIG baseband evaluation. A summary of the data is shown in Table I-3.7-1.

### 3.6.3.3 IRIG Baseband--Deviation Ratio of 1 and 2

The IRIG baseband, channels I through 18 operating at deviation ratios I and 2, was evaluated for tape-recorder error. The detailed conditions were:

Test channels: 70.0 kc  $\pm$ 7.5%; 22.0 kc  $\pm$ 7.5%; 7.35 kc  $\pm$ 7.5%; 3.0 kc  $\pm$ 7.5%; 960 cps  $\pm$ 7.5%

Deviation ratio: 1 and 2

De-emphasis corner frequency: 4 kc

Discriminator full-bandwidth output: 10 volts, peak-to-peak

Tape recorder: Mincom G107

Tape speed: 60 ips

Record level: 1.0v, rms

IF S/N ratio: 39 db

Table II-3.6-1 shows the measured data for the 70 kc, 22 kc, 7.35 kc, 3 kc, and 960 cycle, respectively, for a deviation ratio of 1 and 2. The data is summarized in Table I-3.7-1.

## 3.6.3.4 Expanded Baseband

The expanded baseband, channels 1 t' rough 21, was evaluated for tape-recorder errors. The detailed conditions were:

Test channels:  $165 \text{ kc} \pm 7.5\%$ ;  $124 \text{ kc} \pm 7.5\%$ ;  $93 \text{ kc} \pm 7.5\%$ ;  $70 \text{ kc} \pm 7.5\%$ ;  $3 \text{ kc} \pm 7.5\%$ 

Deviation ratio: 5

De-emphasis corner frequency: 25 kc

Tape recorder: Mincom G107

Discriminator output FB': 10 volts, peak-to-peak

Tape speed: 60 ips

Record level: 1.0v, rms

IF S/N ratio: 39 db

Table II-3.6-3 shows the tape-speed errors for the expanded-baseband channels operating at a deviation ratio of 5. The data is summarized in Table I-3.7-2.

# 3.6.3.5 Expanded Baseband--Wideband Channel.

The expanded baseband was operated with a wideband channel in the highest frequency position. The tape-recorder errors were evaluated for channels I through 19 plus channel H. The detailed conditions were:

Test channels:  $165 \text{ kc} \pm 15\%$ ;  $93 \text{ kc} \pm 7.5\%$ ;  $70 \text{ kc} \pm 7.5\%$ ;

 $3 \text{ kc} \pm 7.5\%$ 

Deviation ratio: 5

De-emphasis corner frequency: 25 kc

Discriminator full-bandwidth output: 10 volts, peak-to-peak

Tape recorder: Mincom G107

Tape speed: 60 ips

Record level: 1.0v, rms

IF S/N ratio: 39 db

Table II-3.6-4 shows the performance of the expanded baseband including the wideband channel. The data is summarized in Table I-3.7-2.

### 3. 6. 3. 6 Constant-Bandwidth Baseband

The constant-bandwidth multiplex, channels I through 21, was evaluated for tape-recorder errors under the following conditions:

Test channels:  $56 \text{ kc} \pm 2 \text{ kc}$ ;  $80 \text{ kc} \pm 2 \text{ kc}$ ;  $120 \text{ kc} \pm 2 \text{ kc}$ ;

160 kc ±2 kc

Deviation ratio: 2

De-emphasis corner frequency: 40 kc

Discriminator full-bandwidth output: 20 volts, peak-to-peak

Tape recorder: Ampex modified FR 1400

Tape speed: 120 ips

Record level 0.5v, rms

IF S/N ratio: 39 db

The data is contained in Table II-3.6-5 and summarized in Table I-3.7-5.

### 3.6.3.7 Combinational-Bandwidth Baseband

The combinational-bandwidth multiplex, IRIG channels 1 through 11 and constant-bandwidth channels 1 through 21, was evaluated for tape-recorder errors under the following conditions:

Test channels:  $3.0 \text{ kc} \pm 7.5\%$ ;  $56 \text{ kc} \pm 2 \text{ kc}$ ;  $88 \text{ kc} \pm 2 \text{ kc}$ ;

120 kc ±2 kc; 160 kc ±2 kc

Deviation ratio: 5 for IRIG channels; 2 for CBW channels

Discriminator full-bandwidth output: 20 volts, peak-to-peak

De-emphasis corner frequency: 40 kc

Tape recorder: Ampex modified FR 1400

Tape speed: 120 ips

Record level: 0,5v rms

IF S/N ratio: 39 db

The data is contained in Table II-3.6-6 and summarized in Table I-3.7-6.

### 3.6.4 Tape-Recorder Intermodulation Test

The intermodulation test, described in Section 3.3, was repeated with the tape recorder in the system. All conditions for the test are identical to those given above in Section 3.6.3. The data photographs are shown in Figures II-3.6-7 through II-3.6-10 and summarized in Table I-3.7-6.

TABLE II-3, 6-1
TAPE SPEED ERROR TEST DATA

Syste	System Beacription: IPIC; 1-18:DE:51/ Discriminator Full Scale Output:	TPIC;	18:00	251 Disc	riminato	r Full Sca	ile Output	-1018	de	(S/N)c: 3946	3946
	Channel			>	Output Noise With Tape Recor	Noise Recorder		Wit	Output Noise Without Tape Recorder	Noise e Recorde	i.
				TSC	On	ISC Off	Off	TSC	TSC On	TSC Off	Off
ż	Frequency	LPOF	DR	CF	BEmv	CF	BEmv	CF mv	BE mv	CF	BE mv
/8	70KC ± 7.5% 5250	5250	1	202	315	204	250	601	210	901	012
8/	70KC±75% 2625	2625	8	80	150	95	011	42	50	39	84
<b>%</b>	70KC ±7,5% 1050	0.501	5,	22	22	35	33	9.5	25	95	95
14/	22KC+7591650	1650		130	200	130	200	89	90	89	96
*/	22K ±75%	825	7	09	80	09	80	32	36	32	36
<u>\</u>	735'KC 175%	551	-	85	/3	85	13	5.5	06	5.5	90
>	7.35KC =7.52 276	276	8	9.	43	45	46	25	26	25,	26
∞	3.0KC ±7.5% 225	225	_	105-	350	105	350	90	330	90	330
. ∞	3.0 KC #75% 112	112	6	32	70	38	75	23	65	23	65
·	3.0 KC : 7.5%	45-	5,	8	6	9/	11	5.5	7.5	5,5,	7.5
7	960cps:75%	72	\	08	300	0.8	300	70	300	20	300
4	4 960cms 175%	36	18	25-	5'5	25	55	/8	53	18	53

TABLE II-3, 6-2 TAPE SPEED ERROR TEST DATA

·					Output	Output Noise			Output Noise	Noise	
	Channel				With Tape	Recorder	L.	Wí	Without Tape Recorder	e Record	i e
				TSC	TSC On	TSC Off	Off	TSC	TSC On	ISC OU	Off
Š.	Frequency	LPOF cps	DR	CF	BEmv	CF mv	BE mv	CF	3 E	CF	BE
A	70 KC ± 15-%	2100	5	12	20	28	25	.00	85	∞	8.5
80	3.0KC ±7.5%	45	5-	7	01	15,	15,	ĵð.	*	,0	~
		٥									
									•	v	
		i į									
			_								
											,
										-	

Name CRI / Mail Date. 1

# TAPE SPEED ERROR TEST DATA

Syste	System Description: Expused: 1-21	Expansel	1-51		criminato	r Full Sc	ale Outpu	Discriminator Full Scale Output: 10UPP	0,0	(S/N)	776 2 : (N/S)
	Channel				Output With Tape	Output Noise 1 Tape Recorder		W	Output Noise thout Tape Reco	Output Noise Without Tape Recorder	10
,				TSC	TSC On	TSC	TSC Off	TSC	TSC On	TSC Off	Off
Š	Frequency	LPOF	DR	CF mv	BE mv	CF	BEmv	CF	BE mv	CF nv	BE
3	16576 +7.5% 2475	2475	15	8/	9/	30	22	8.5	7.5	8.5	7.5
20		0981	ۍ′	8/	/3	29	25-	13.5	6	13.5	6
6/	93KL ±75% 1400	1400	ۍ,	/5/	H	25-	25-	9.5	10	9.5	70
/8	70xct 7.5% 1050	1050	5,	14	15	25,	25	10.5	1	10.5	\ \ \
<b>∞</b>	3.0KC±7.5%	45	3,	5,	જ	17	11	3.5	6.5	3.5	6.5
,						٠.		٠.			
				,		·					
						·					

Name: WSB/MOL Date: 2-4-65

TABLE II-3, 6-4
TAPE SPEED ERROR TEST DATA

Output Noise With Tape Recorder Without Tape Recorder	TSC On TSC Off TSC On	CF BE CF BE CF BE CF mv mv mv mv	18 13 23 18 9.5 8.5	14 12.5 25 24 11 9.5	13 13 26 24 9.5 10 9.5	5.5 7.5 18 19 3.4 5.5 3.4				
Output N. With Tape R.	TSC On			<u> </u>						
		LPOF CP8 DR	950 5	400 5	050 5	45 5			***************************************	
Channel		Frequency	165 MC ±15% 4950	93KC ±75% 1400	70KC±75% 1050	3.0KC±75%	:		,	

1,011

# TAPE SPEED ERROR TEST DATA

Output Noise Without Tape Recorder	TSC On TSC Off	BE CF BE	58 60 58	62	69 63 69	65 64 65							
3	T.	CF m v	09	62	62	64						<u>.</u>	
ler	TSC Off	BEmv	82	84	82	85-	· · · · · · · · · · · · · · · · · · ·	anglis Simbogana		······································	· · · · · · · · · · · · · · · · · · ·		
Output Noise 1 Tape Recorder	TS	CF m	77	78	78	78			,				
Output With Tape	TSC On	BEmv	44	78	18	7.5			,	,	· · · · ·		
	Į.	CF	72	72	68	11							
		DR	8	8	8	7							
		LPOF	1000	1000	1000	1000			1.7				
Channel		Frequency	160KC ± 2KC	120KC ±2KC	88KC ± 24C 1000	56KC £2KC 1000						·	
		Š.	61	*	0/	9							

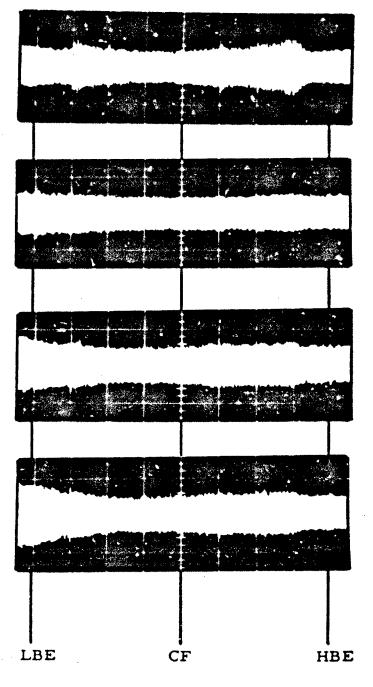
Name: WSB/MD1

702 Date: 3-30-65

TAPE SPEED ERROR TEST DATA

201		· -	1	<del></del>			<del></del>	<del></del>	
9,065 3901S)	Output Noise Without Tape Recorder	Off	B,E mv	85-	38	89	80	:	
Svatem Description: Lembert on Discriminator Full Scale Output: 200PD (SIN)		On TSC Off	CF	85-	82	83	80	6.3	
			BE mv	85	3,5	58	80	1	
	Output Noise With Tape Recorder Wit	Off TSC On	CF.	85	82	83	80	6.3	
			BE mv	80/	107	411	ره //	/37	
		On TSC Off	CF mv	011	106	811	801	12	
			BEmv	901	102	hol	801	7/	
Sec Dis		TSC	CF	108	16	46	95-	8.0	
1,00,1	DR			2	8	~	~	5,	
Central	LPOF			1000	0001	1000	1000	45,	
Description:	Channel		Frequency	160 NC±2 NC	120KC ±2KC 1000	88 NC = 2 NC 1000	56HZ \$2HC 1000	3.0 KC £7.5%	
System			Ž.	61	7	10	e	<b>∞</b>	

Name: (USB/11/04 Date: 3.30-65-



Channel 6, 56.0 kc ±2 kc RMS Level = 134 mv max. DR = 2

Channel 10, 88.0 kc ±2 kc RMS Level = 90 mv max. DR = 2

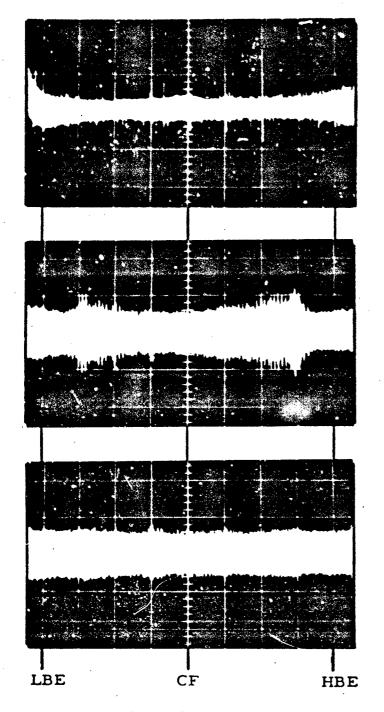
Channel 14, 120.0 kc ±2 kc RMS Level = 98 mv max. DR = 2

Channel 19, 160.0 kc ±2 kc RMS Level = 106 mv max. DR = 2

Horizontal: 5 sec/cm

Vertical: 2.5% FBW/cm

FIGURE II-3. 6-7
TAPE RECORDER INTERMODULATION TEST DATA:
CONSTANT BANDWIDTH MULTIPLEX



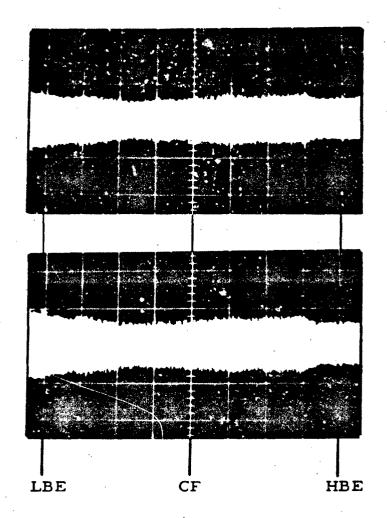
IRIG Channel 8, 3.0 kc ±7.5% DR = 5 RMS Level = 13.5 mv max. Vertical: 0.5% FBW/cm

CBW Channel 6, 56.0 kc ±2 kc DR = 2 RMS Level = 205 mv max. Vertical: 2.5% FBW/cm

CBW Channel 10, 88.0 kc ±2 kc DR = 2 RMS Level = 112 mv max. Vertical: 2.5% FBW/cm

Horizontal: 5 sec/cm

FIGURE II-3.6-8
TAPE RECORDER INTERMODULATION TEST DATA:
COMBINATIONAL BANDWIDTH MULTIPLEX, IRIG CHANNEL 8,
CBW CHANNELS 6 AND 10

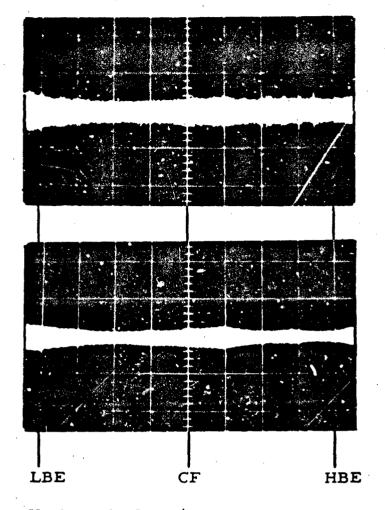


Horizontal: 5 sec/cm

CBW Channel 14, 120.0 kc ±2 kc DR = 2 RMS Level = 118 mv max. Vertical: 2.5% FBW/cm

CBW Channel 19, 160.0 kc ±2 kc
DR = 2
RMS Level = 136 mv max.
Vertical: 2.5% FBW/cm

FIGURE II-3.6-9
TAPE RECORDER INTEMODULATION TEST DATA:
COMBINATIONAL BANDWIDTH MULTIPLEX, CBW CHANNELS 14 AND 19



With Tape Recorder RMS Level = 71 mv max.

Without Tape Recorder RMS Level = 48 mv max.

Horizontal: 5 sec/cin

Vertical: 2.5% FBW/cm

Search Channel: CBW Channel 6, 56.0 kc ±2 kc, DR = 2

FIGURE II-3.6-10
TAPE RECORDER INTERMODULATION TEST DATA:
COMBINATIONAL BANDWIDTH MULTIPLEX,
NO RF LINK, CBW CHANNEL 6

### 3.7 PULSE MODULATION

# 3.7.1 PAM/FM/FM System Test

### 3.7.1.1 General

The PAM/FM/FM test was made to determine the system accuracy for pulseamplitude modulation (PAM). Since the system used in this evaluation program includes all equipment from the VCO input to the subcarrier discriminator output, errors due to sampling and data interpolation are not considered. The PAM error of interest is interchannel (pulse-to-pulse) crosstalk caused by various filters in the system and appearing as limited output rise and fall times. For example, if one pulse is at zero scale and the next at full scale, the output cannot rise to its new value instantaneously. A sampling detector was assumed in the decommutator; therefore, if the output reaches its full value (steady-state condition) within the pulse duration time no error is assumed, e.g., if the pulse can be sampled at its full height, no crosstalk error occurs. Thus, the crosstalk error test is reduced to determining at what degree the pulse reaches its full steady-state value. Since the worst-case crosstalk occurs when the output must traverse the greatest distance, the test PAM wave train consisted of a zeroscale pulse followed by three full-scale pulses and then another zero-scale pulse. The discriminator output was observed using a Tektronix type Z plug-in which allows the exact full-scale voltage to be subtracted from the pulse train and the resulting error examined. Data was recorded by photographing the oscilloscope display. The sampling time was periodic and positioned so that a minimum error would occur.

For each proportional-bandwidth baseband, the wideband channel was modulated with PAM at 900 sps for the IRIG baseband and 2100 sps for the expanded baseband. The subcarrier discriminator 18 db/octave LPOF was operated at its normal cutoff frequency for a deviation ratio of 5. This condition is approximately correct for sampling type decommutators. Figure II-3.7-1 shows the block diagram of the test setup.

### 3.7.1.2 Detailed Procedure

- a. Calibrate all VCOs.
- b. Deviate all channels with the exception of the test channel, full bandwidth at the maximum modulating frequency for a deviation ratio of 5.
  - c. Allow the receiver AGC to assume its normal operating condition.
  - d. The IF carrier-to-noise ratio should be greater than 20 db.
- e. Deviate the test channel full bandwidth at the appropriate pulse rate with the output of the PAM/PDM simulator.

- f. Set subcarrier discriminator output for 20v, peak-to-peak
- g. With a Tektronix type Z plug-in, determine the error from full scale at duty cycles of 40, 50, and 70%. (The PAM simulator does not have a 65% duty cycle position; therefore, 70% is used instead.)

### 3.7.1.3 Results

### 3.7.1.3.1 IRIG Baseband

The IRIG baseband channels I through 16 plus channel E were evaluated with PAM on channel E. The detailed conditions were:

Sample rate: 900 samples per second

Test channel: 70 kc ±15%

LPOP: 2100 cps constant delay, 18 db/octave type

Discriminator FBW output: 20v, peak-to-peak

IF S/N ratio: 39 db

Figure II-3.7-22 shows a photograph of the system input and output with no vertical scale expansion. Figure II-3.7-2b shows the discriminator output using the Tektronix type Z plug-in. The top trace is the system input and the bottom trace is the system output. The two middle traces are the system output minus full-scale voltage. The straight line thus represents zero error for full-scale modulation. The expanded PAM pulses are shown just below the zero reference line. Thus, using a sampling detector, an instantaneous sample could be taken anywhere within 50 µsec and produce an error less than 0.5% of FBW. The data in Figure II-3.7-3 shows the performance for 40% and 70% duty-cycle PAM.

## 3.7.1.3.2 Expanded Baseband

The expanded baseband, channels I through 19 plus channel H, was evaluated with PAM on channel H. The detailed conditions are:

Sample rate: 2100 sps

Test channel: 165 kc ±15%

LPOF: 4950 cps constant-delay 18 db/octave type

Discriminator FBW output: 20v, peak-to-peak

IF S/N ratio: 39 db

Figure II-3. 7-4a shows a photograph of the system input and output with no vertical scale expansion. Figure II-3. 7-4b shows the discriminator output using the Tektronix type Z plug-in. The photographs present similar data described in Section 3. 7. 1. 3. 1 for the IRIG baseband. Figure II-3. 7-5 shows the performance for 40% and 70% duty-cycle PAM.

# 3.7.2 PDM/FM/FM System Test

### 3.7.2.1 General

The PDM/FM/FM test was made to determine the system accuracy for pulse duration modulation (PDM). For each proportional-bandwidth baseband, the wideband channel was modulated with PDM at 900 sps rate for the IRIG baseband and 2100 sps for the expanded baseband. The zero- and full-scale pulse lengths are standard at 100 and 700 microseconds, respectively, for the expanded baseband. The discriminator low-pass output filter used was a constant delay, 18 db/octave type with the cutoff frequency equal to five times the repetition rate. The cutoff frequency was selected to be as narrow as possible without affecting the zero-scale pulse duration.

In all cases, photographs were taken of the oscilloscope display to show the variation in pulse duration. In addition to the pulse duration measurements, the adjacent channel in each baseband was checked for an increase in intermodulation (crosstalk) noise due to the PDM. The block diagram for the test is identical to the PAM test setup shown in Figure II-3.7-1.

## 3.7.2.2 Detailed Procedure

- a. Calibrate all VCOs.
- b. Deviate all channels with the exception of the test channel full bandwidth at the maximum modulating frequency for a deviation ratio of 5.
  - c. Set the receiver AGC to its normal operating condition.
  - d. The IF signal-to-noise ratio should be greater than 20 db.
- e. Deviate the test channel full bandwidth at the appropriate pulse rate with the output of the PAM/PDM simulator.
  - f. Set subcarrier discriminator full-scale output for 20v peak-to-peak.

- g. Observe and photograph the dual-trace oscilloscope display of the PDM input and discriminator output waveform.
- h. Repeat the intermodulation test (described in Section 3.3) on the adjacent channel for both 7.5% and 15% PDM deviation of the test channel.

### 3.7.2.3 Results

### 3.7.2.3.1 IRIG Baseband

The IRIG baseband, channels I through 16 plus channel E was evaluated with PDM on channel E. The detailed conditions were:

Repetition rate: 900 pulses per second

Test channel: 70 kc ±15%

LPOF: 4500 cps, constant-delay, 18 db/octave

Discriminator FBW output: 20v peak-to-peak

IF S/N ratio: 39 db

Zero-scale pulse: 100 microseconds

Full-scale pulse: 700 microseconds

Figure II-3.7-6 shows a photograph of the system input and output for 0, 25, 50, 75, and 100% full scale (FS) PDM. The time delay through the system is contained in this photograph. Figure II-3.7-7 shows the system input and output for a 0 and 100% FS PDM modulation with double exposure used to remove the relative system delay and simplify comparison of pulse duration.

The effect of PDM of the 70 kc  $\pm 15\%$  channel on the intermodulation level in the 40 kc  $\pm 7.5\%$  channel is shown in Figure II-3.7-8. The worst-case intermodulation was found to occur with all channels of the PDM input at 100% FS; therefore, intermodulation was measured with this PDM. Figure II-3.7-8a shows the intermodulation effect for full  $\pm 15\%$  PDM deviation of the 70 kc  $\pm 15\%$  channel while Figure II-3.7-8b shows the same effect for  $\pm 7.5\%$  deviation. No differences in pulse duration were found between  $\pm 7.5\%$  or  $\pm 15\%$  deviation.

### 3.7.2.3.2 Expanded Baseband

The expanded baseband, channels I through 19 plus channel H was evaluated with PDM on channel H. The detailed conditions were:

Repetition rate: 2100 pulses per second

Test channel: 165 kc ±15%

LPOF: 10500 cps, constant-delay, 18 db/octave

Discriminator FBW output: 20v peak-to-peak

IF S/N ratio: 39 db

Zero-scale pulse: 50 microseconds

Full-scale pulse: 300 microseconds

Figure II-3.7-9 shows a photograph of the system input and output with 0, 25, 50, 75, and 100% FS PDM. For ease of comparison, the system time delay has been removed through use of a double exposure. Figure II-3.9-10 shows the system input and output for 0 and 100% FS PDM with the system delay removed.

The effect of PDM of the 165 kc  $\pm$ 15% channel on the intermodulation level in the 93  $\pm$ 7.5% channel is shown in Figure II-3.7-11. The worst-case intermodulation was found to occur with all channels of the PDM input at 0% FS; therefore, the intermodulation was measured with this modulation. Figure II-3.7-11a shows the intermodulation effect for full  $\pm$ 15% PDM deviation and Figure II-3.7-11b shows the intermodulation for  $\pm$ 7.5% deviation. No differences in pulse duration were found between  $\pm$ 7.5% and  $\pm$ 15% deviation.

### 3.7.3 PCM/FM/FM Systems Test

### 3.7.3.1 General

The PCM/FM/FM test was made to determine the bit-error probability for pulse-code modulation as a function of carrier-to-noise ratio. For the proportional-bandwidth basebands, the wideband channel is modulated with PCM at 21,000 bits per second for the IRIG baseband and 49,500 bits per second for the expanded baseband. In each case, the bit rate is equal to the bandwidth of the channel and the channel was deviated at 70% of full bandwidth. This modulation condition has been shown to be optimum for PCM/FM.

<sup>(1)</sup> Experimental Determination of Signal-to-Noise Relationships in PCM/FM and PCM/PM Transmission, Interim Report for NASA, GSFC, Contract NAS 5-505, Electro-Mechanical Research, Inc., Sarasota, Florida, October 20, 1961.

<sup>(2)</sup> Telemetry System Study, Final Report, Volume II of III, Experimental Evaluation Program, U.S. Army Signal Research and Development Laboratories, Contract No. DA-36-039SC-73182, Aeronutric, Newport Beach, California, December 18, 1959

An EMR Model 219 PCM Signal Conditioner is used to reconstruct the PCM output of the wideband subcarrier discriminator. The discriminator low-pass output filter (LPOF) was bypassed and the PCM output signal fed directly into the signal conditioner. (Normally the LPOF should be operated several times the bit rate; however, one was not immediately available.) The signal conditioner is operated in the filter sample mode, i.e., a constant-delay input filter followed by an instantaneous sampling detector is used. The reconstructed PCM wave form from the signal conditioner and the input PCM wave train are then compared in the bit-error detector. The bit errors are accumulated in an electronic counter for a fixed interval of time, thus enabling the bit-error probability to be calculated. The block diagram for the PCM system test is shown in Figure II-3.7-12.

### 3.7.3.2 Detailed Procedure

- a. Calibrate all VCOs.
- b. Deviate all channels with the exception of the test channel full bandwidth at  $f_m$  where  $f_m$  is the maximum modulation frequency for deviation ratio of 5.
  - c. Hold the receiver AGC voltage at -4 volts dc.
  - d. Set the subcarrier discriminator output for 20 volts, peak-to-peak.
- e. Deviate the test channel 70% full bandwidth at the appropriate PCM rate with the output of the PCM random bit generator.
  - f. Set the IF carrier-to-noise ratio to greater than 20 db.
- g. Operate the EMR Model 219 Signal Conditioner at the appropriate rate and in the filter-sample mode.
- h. Adjust the delay in the bit-error detector to align the input PCM waveform and the reconstructed waveform. Under this condition, there should be no errors occurring at the output of the bit-error detector.
- i. Invert the output of the PCM signal conditioner and count the errors that occur at the output of the bit-error detector. The number of errors should equal the bit rate. Set the signal conditioner to normal output.
- j. Select appropriate carrier-to-noise ratios and determine the error count at each carrier-to-noise ratio.
- k. The bit-error probability can be calculated from the number of errors that occur in the total interval measured divided by the total number of bits occuring in that same interval.

1. Repeat the intermodulation test described in Section 3, 3, on the adjacent lower channel.

### 3.7.3.3 Results

### 3.7.3.3.1 IRIG Baseband

The IRIG baseband, channels I through 16 plus channel E was evaluated with PCM on channel E. The detailed conditions were:

Repetition rate: 21,000 bits per second

Test channel: 70 kc ±15%

LPOF: None (bypassed)

Discriminator full-bandwidth output: 20 volts, peak-to-peak

Table II-3.7-13 shows the bit-error rates measured with the various carrier-to-noise ratios. The effect of the random bit PCM modulation of the 70 kc  $\pm 15\%$  channel on the intermodulation (crosstalk) level in the 40 kc  $\pm 7.5\%$  channel is shown in Figure II-3.7-14a. The effect of intermodulation for an alternate ONE/ZERO bit pattern is shown in Figure II-3.7-15a.

## 3.7.3.3.2 Expanded Baseband

The expanded baseband channels I through 19 plus channel H, was evaluated with PCM modulation on Channel H. The detailed conditions were:

Bit rate: 49,500 bits per second

Test channel:  $165 \text{ kc} \pm 15\%$ 

LPOF: None (bypassed)

Discriminator full-bandwidth output: 20 volts, peak-to-peak

Table II-3. 7-13 shows the bit-error rate for PCM operation of the expanded baseband. The effect of the random-bit PCM modulation of the 165 kc ±15% channel on the intermodulation level in the 93 kc ±7.5% channel is shown in Figure II-3. 7-14b. The intermodulation for an alternate ONE/ZERO bit pattern is shown in Figure II-3. 7-15b.

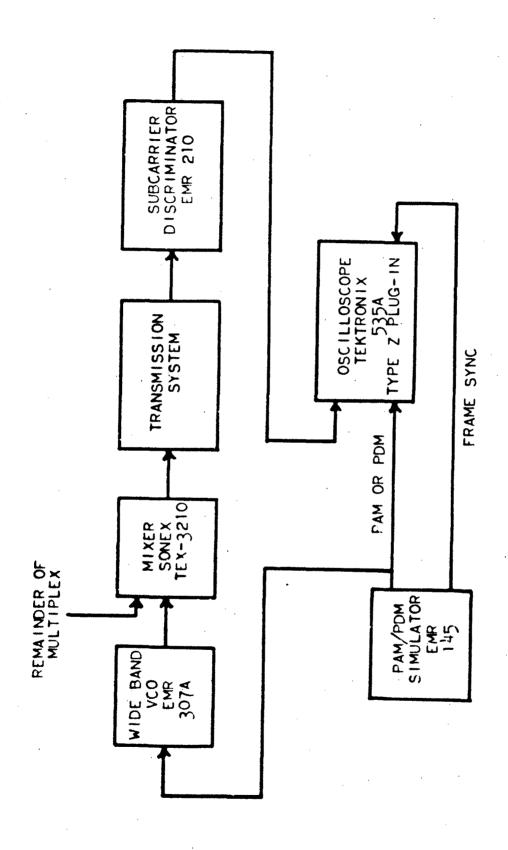
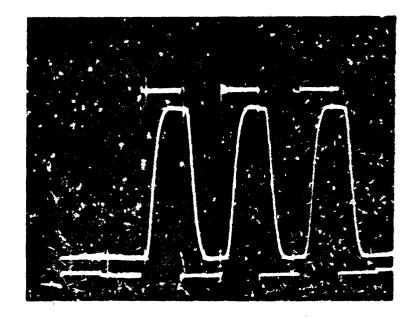


FIGURE II-3, 7-1 PAM/PDM BLOCK DIAGRAM

Discriminator Output Vertical Scale: 5V/cm (25% FBW/cm)

PAM Input Vertical Scale: 1V/cm (20% FBW/cm)

orizontal Scale:



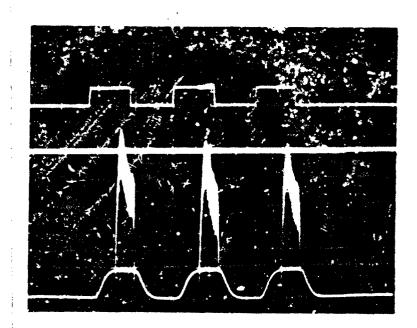
PAM INPUT AND OUTPUT - NO SCALE EXPANSION

PAM Input Vertical Scale: 10V/cm

Full Scale Level Vertical Scale: 0.05V/cm (0.25% FBW/cm)

Discriminator Output Vertical Scale: 0.05V/cm (0.25% FBW/cm)

Discriminator Cutput Vertical Scale: 25V/cm



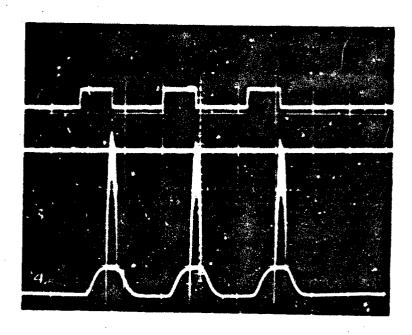
rizontal Scale: 1 ms/cm

EXPANDED SCALE PAM OUTPUT - 50% DUTY CYCLE

FIGURE II-3. 7-2 50% PAM ON 70 kc ±15% CHANNEL

- 1. PAM Input
  Vertical Scale:
  10V/cm
- 2. Full Scale LevelVertical Scale:0.05V/cm(0.25% FBW/cm)
- 3. Discriminator Output
  Vertical Scale:
  0.05V/cm
  (0.25% FBW/cm)
- 4. Discriminator Output
  Vertical Scale:
  25V/cm

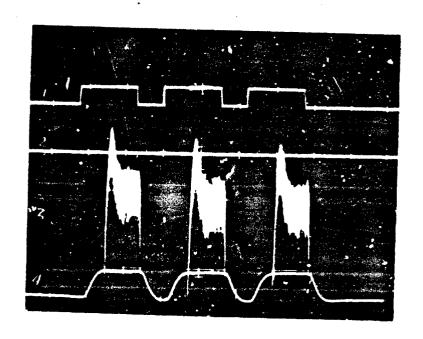
Horizontal Scale: 0.1 ms/cm



a. 40% PAM

- 1. PAM Input
  Vertical Scale:
  10V/cm
- 2. Full Scale LevelVertical Scale:0.05V/cm(0.25% FBW/cm)
- 3. Discriminator OutputVertical Scale:0.05V/cm(0.25% FBW/cm)
- 4. Discriminator Output
  Vertical Scale:
  25V/cm

Horizontal Scale: 0.1 ms/cm

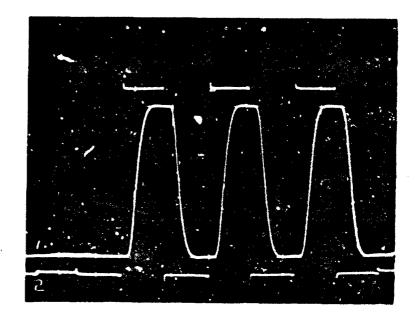


b. 70% PAM

FIGURE II-3. 7-3 40% AND 70% PAM ON 70 kc ±15% CHANNEL

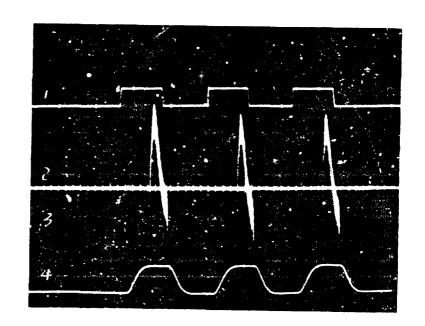
- Discriminator Output Vertical Scale: 5V/cm (25% FBW/cm)
- 2. PAM Input
  Vertical Scale:
  1V/cm
  (20% FBW/cm)

Horizontal Scale: 0, 2 ms/cm



. PAM INPUT AND OUTPUT - NO SCALE EXPANSION

- Vertical Scale: 10V/cm
- Vertical Scale:
  0.05V/cm
  (0.25% FBW/cm)
- Discriminator Output
  Vertical Scale:
  0.05V/cm
  (0.25% FBW/cm)
- Discriminator OutputVertical Scale:25V/cm



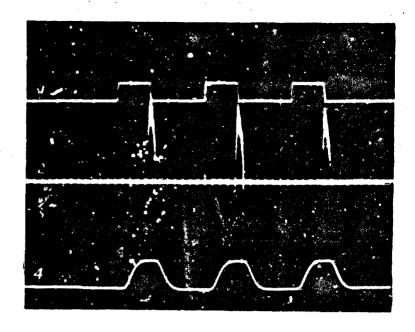
# Iorizontal Scale:

- .2 ms/cm
- . EXPANDED SCALE PAM OUTPUT 50% DUTY CYCLE

FIGURE II-3.7-4 50% PAM ON 165 kc ±15% CHANNEL

- 1. PAM Input
  Vertical Scale:
  10V/cm
- 2. Full Scale LevelVertical Scale:0.05V/cm(0.25% FBW/cm)
- 3. Discriminator Output
  Vertical Scale:
  0. ^5V/cm
  (0. 25% FBW/cm)
- 4. Discriminator Output Vertical Scale: 25V/cm

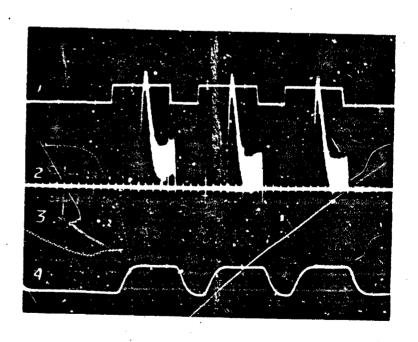
Horizontal Scale: 0.2 ms/cm



a. 40% PAM

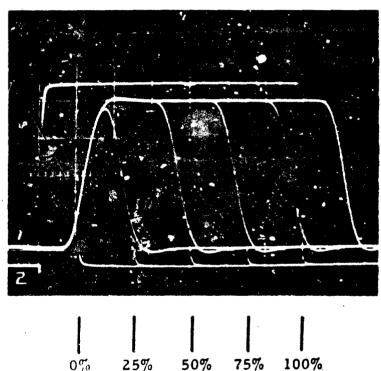
- 1. PAM Input
  Vertical Scale:
  10V/cm
- 2. Full Scale LevelVertical Scale:0.05V/cm(0.25% FBW/cm)
- 3. Discriminator Output
  Vertical Scale:
  0.05V/cm
  (0.25% FBW/cm)
- 4. Discriminator Output Vertical Scale: 25V/cm

Horizontal Scale: 0.2 ms/cm



b. 70% PAM

FIGURE II-3. 7-5 40% AND 70% PAM ON 165 kc ±15% CHANNEL



PDM Input Fulse Duration In Percent Full Scale

Trace 1. Discriminator Output
Vertical Scale: 5v/cm (25% FBW/cm)

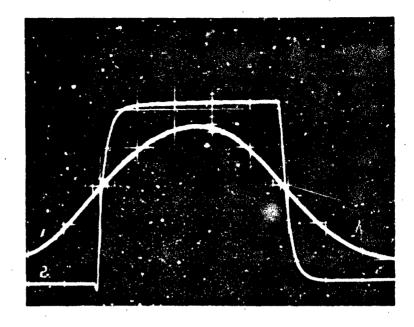
Trace 2. PAM Input
Vertical Scale: lv/cm (20% FBW/cm)

Horizontal Scale: 100 microseconds/cm

FIGURE II-3. 7-6 PDM ON 70 kc ±15% CHANNEL

- Discriminator Output Vertical Scale: 5v/cm
- 2. PAM Input
  Vertical Scale:
  lv/cm

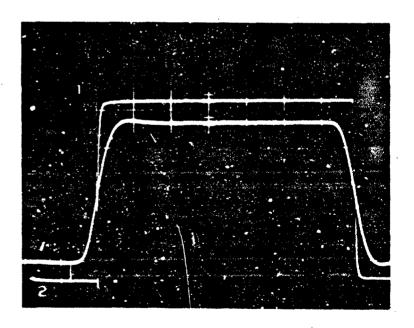
Horizontal Scale: 20 microseconds



a. 0% FS PDM Input and Output

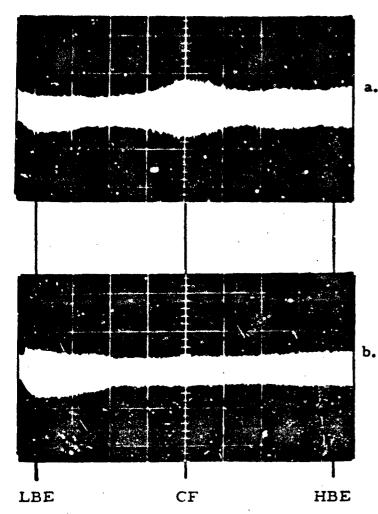
- Discriminator Output
   Vertical Scale:
   5v/cm
- 2. PAM Input
  Vertical Scale:
  lv/cm

Horizontal Scale: 100 microseconds/cm



b. 100% FS PDM Input and Output

FIGURE II-3. 7-7 0% AND 100% PDM ON 70 kc ±15% CHANNEL

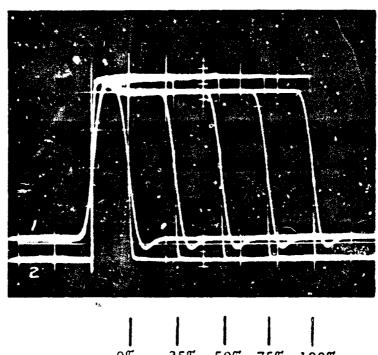


±15% PDM Deviation
Vertical: 0.5% FBW/cm
RMS Level: 27 mv max.

±7.5% PDM Deviation Vertical: 0.5% FBW/cm RMS Level: 24 mv max.

100% FS PDM Modulation on the 70 kc ±15% Channel Search Channel: 40 kc ±7.5%

FIGURE-3.7-8
EFFECT OF PDM MODULATION ON ADJACENT
CHANNEL INTERMODULATION - IRIG BASEBAND



000 25% 50% 75% 100%

PDM Input Pulse Duration In Percent Full Scale

Trace 1. Discriminator Output Vertical Scale: 5v/cm (25% FBW/cm)

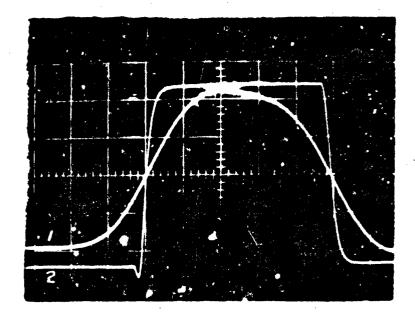
Trace 2. PAM Input Vertical Scale: lv/cm (20% FBW/cm)

Horizontal Scale: 50 microseconds/cm

FIGURE II-3. 7-9 PDM ON 165 kc ±15% CHANNEL

- 1. Discriminator Output Vertical Scale: 5V/cm
- 2. PAM Input
  Vertical Scale:
  1V/cm

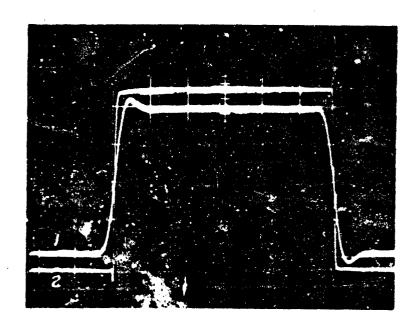
Horizontal Scale: 10 microseconds/cm



a. 0% FS PDM Input and Output

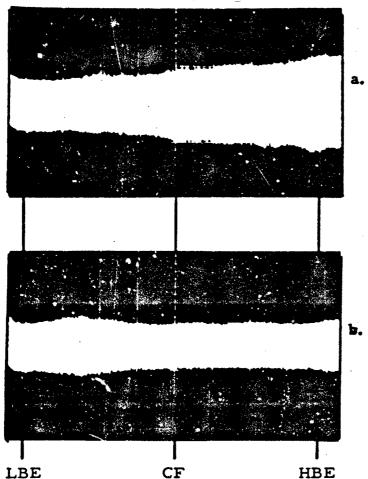
- 1. Discriminator Output Vertical Scale: 5V/cm
- 2. PAM Input
  Vertical Scale:
  1V/cm

Horizontal Scale: 50 microseconds/cm



b. 100% FS PDM Input and Output

FIGURE II-3. 7-10 0% AND 100% PDM ON 155 kc ±15% CHANNEL



a. ±15% PDM Deviation Vertical: 0.5% FBW/cm RMS Level: 49 mv max.

b. ±7.5% PDM Deviation
Vertical: 0.5% FBW/cm
RMS Level: 21 mv max.

100% FS PDM Modulation on the 165 kc ±15% Channel Search Channel: 93 kc ±7.5%

FIGURE II-3.7-11
EFFECT OF PDM MODULATION ON ADJACENT CHANNEL
INTERMODULATION - EXPANDED PROPORTIONAL BANDWIDTH BASEBAND

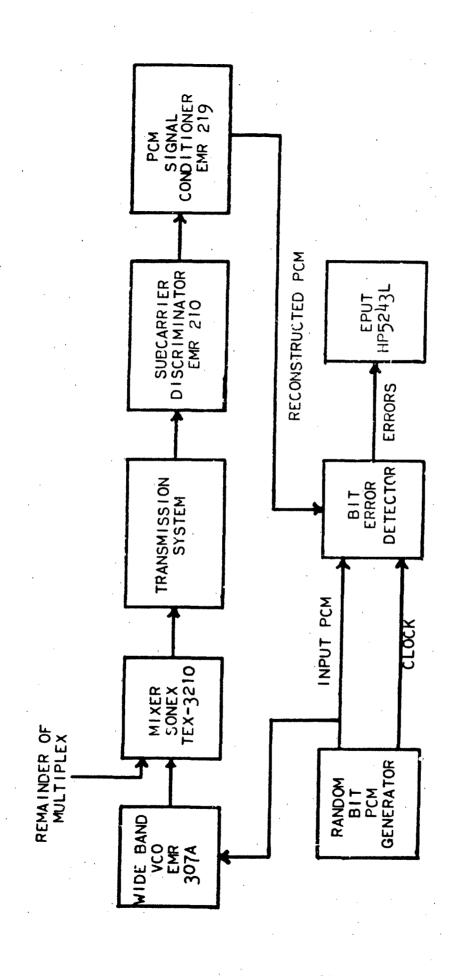
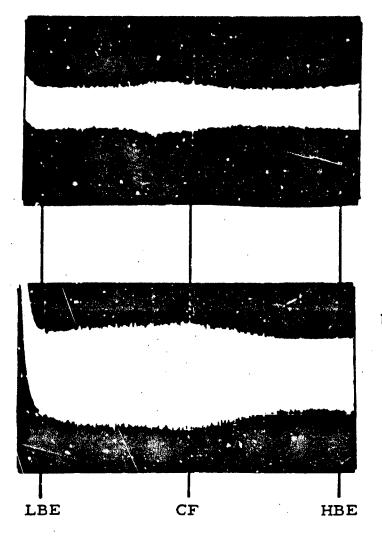


FIGURE II-3, 7-12 PCM BLOCK DIAGRAM

# TABLE II-3. 7-13 PCM BIT ERROR DATE

•	IRIG Baseba	and Expan	Expanded Baseband								
AGC Level:	-4.0 vd	<u>-</u>	-4.0 vdc								
Mult. Level:	1.0 YM	<u> </u>	630 MYTHS								
Bit Rate:	21,000 6/	<u> </u>	19,500 4/5								
Channel:	70KC \$ 157		165KC±1570								
Deviation:	0.7FBW		0.7FBW								
(S/N) c (db)	Bit Errors	Time Interval (Sec.)	Bit Error Probability								
IRIG Baseband											
8	27	600	2.14 × 10-6								
7	41	60	3.25×10-5								
6	472	60	3.75× 10-4								
5	6,442	60	5.1/x10-3								
4	21,865	60	1.74 ×10-2								
2	108, 328	60	8.60×10-2								
No Signal	622,362	. 60	4.94×10-1								
Expanded Baseband											
18	147	180	1.65 × 10-6								
17	73	60	2.46 × 10-5								
16	856	60	2.88×10-4								
14	3,415	60	1.15 × 10-3								
13	12,932	60	4.35×10-3								
12	39,313	60	1.32×10-2								
10	175,222	60	5.89 × 10-2								
9	279,747	60	9.42×10-2								

Name W Bishop Date 2/16/65

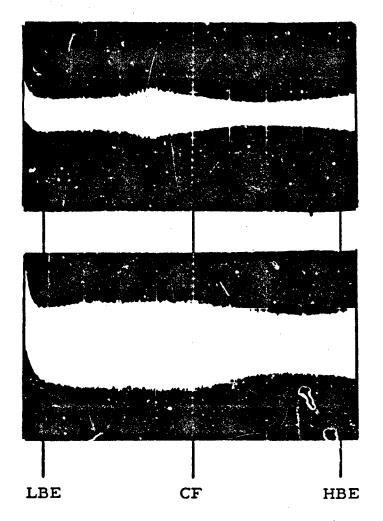


Search Channel: 40 kc ±7.5% PCM Channel: 70 kc ±15% Vertical: 0.5% FBW/cm RMS Level: 25 mv max.

b. Expanded Baseband
Search Channel: 93 kc ±7.5%
PCM Channel: 165 kc ±15%
Vertical: 0.5% FBW/cm
RMS Level: 60 my max.

All other channels in baseband modulated FBW at 0.1  $f_m$  where  $f_m$  is the maximum rate for a deviation ratio of 5.

FIGURE II-3. 7-14
EFFECT OF PCM MODULATION ON
ADJACENT CHANNEL INTERMODULATION



a. IRIG Baseband
Search Channel: 40 kc±7.5%
PCM Channel: 70 kc±15%
Vertical: 0.5% FBW/cm
RMS Level: 15 mv max.

b. Expanded Baseband
Search Channel: 93 kc ±7.5%
PCM Channel: 165 kc ±15%
Vertical: 0.5% FBW/cm
RMS Level: 54 mv max.

All other channels in baseband are turned off.

FIGURE II-3. 7-15
EFFECT OF PCM MODULATION ON ADJACENT
CHANNEL INTERMODULATION - TWO CHANNEL MULTIPLEX